

### REPORT OF GEOTECHNICAL EXPLORATION

# I-75 Interchange Modification at I-24 (Phase 2) (Design Build) (IA)

PIN 114174.01 Chattanooga, Tennessee

#### Prepared For:

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May 6, 2022



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Subject: Report of Geotechnical Exploration

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Dear Mr. Blevins:

Neel-Schaffer, Inc., is pleased to submit this report which details the results of our geotechnical exploration for the referenced project.

The project described includes the design of the reconstruction of the Interchange of Interstate 75 (I-75) and Interstate 24 (I-24) and approaches.

The project has been divided into two phases, and this report presents the general geologic conditions at the site of the bridge replacements and retaining walls proposed as part of Phase II. Information from the 2018 K.S. Ware and Associates (KSWA) report, and existing bridge foundation data was also utilized. In addition, a series of pavement cores and field dynamic cone penetrometer tests were performed to investigate the subgrade conditions along a section of I-24.

The attached report describes the site and subsurface conditions encountered. This report contains information for use by designers and is not intended for use as a design report conforming to the TDOT Geotechnical Manual. The Appendices contain figures and drawings, and field and laboratory test results from the most recent drilling as well as information that applies to Phase II from the KSWA report submitted in May of 2018.

We appreciate this opportunity to be of service to you on this project. Please contact us if you have any questions regarding this report.

Respectfully submitted,

David Barker

Neel-Schaffer, Inc.

David Barker, P.E.

Senior Geotechnical Engineer

Enclosures: Report of Geotechnical Exploration

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#### 1.0 INTRODUCTION

#### 1.1 PROJECT INFORMATION

The Tennessee Department of Transportation (TDOT) is currently building a new interchange at the junction of Interstate 75 and Interstate 24 in Chattanooga, Tennessee. A Site Location Plan is included as Figure 1 in Appendix A. The new interchange will include construction of new ramps and bridges within the interchange to reconfigure the traffic pattern in the interchange. Additional improvements to add traffic lanes will extend south on I-75 to about Exit 1 (Ringgold Road), north of I-75 to approximately Exit 4 (East Brainerd Road) and west on I-24 to Germantown Road. The project has been divided in to two phases, the first phase started south of Ringgold Road and extended through the Interchange to about Station 443+00, or south of the I-75 bridge over the CSX Railroad. Phase II will continue to approximately the East Brainerd Road exit, and includes the bridge over the CSX Railroad. On I-24, Phase I included interchange ramps and extended to approximately Station 175+00, inclusive of the Spring Creek Road overpass. Phase II will begin from this point back to the start of the project on I-24 at about Station 75+00, including the McBrien Road and Moore Road overpasses. It should be noted that noise walls are shown on the functional cross sections left of centerline as far west as Station 56+00, and right of centerline as far west as Station 60+00.

To facilitate the widening of lanes on I-24, **retaining walls** (primarily cut walls) are proposed to maintain grade separation between the interstate, off and on ramps, and the existing frontage roads. Overhead signs, ITS Systems, noise barrier walls, and other features will also be included.

The preliminary plans developed by Neel-Schaffer proposes the following retaining walls at the approximate locations along I-24 in Phase II:

Wall No. 1, I-24 Station 96+50 to Station 113+00, left of centerline.

Wall No. 2, I-24 Station 139+75 to Station 140+75, left of centerline, includes Moore Rd. N. abutment.

Wall No. 3, I-24 Station 155+00 to Station 160+50, left of centerline, includes McBrien Rd. N. abutment.

Wall No. 4, I-24 Station 105+10 to Station 114+60, right of centerline.

Wall No. 5, I-24 Station 114+00 to Station 117+50, right of centerline, cut/fill wall for proposed off-ramp.

Wall No. 6, I-24 Station 131+50 to Station 144+50, right of centerline, includes Moore Rd. S. abutment.

Wall No. 7, I-24 Station 154+25 to Station 155+75, right of centerline, includes McBrien Rd. S. abutment.

The following retaining walls are proposed along I-75 in Phase II:

Wall No. 8, I-75 Station 443+50 to Station 447+00, left of centerline.

Wall No. 10, I-75 Station 454+50 to Station 456+00, right of centerline.

Wall No. 11, I-75 Station 460+50 to Station 463+00, right of centerline.

Phase II will also include replacing 3 existing **bridges**. The following list provides the location of the planned structures.

Bridge for I-75 SB and I-75 NB over CSX Railroad, to be replaced.

Bridge for McBrien Road over I-24 EB and WB, to be replaced.

Bridge for Moore Road over I-24 EB and WB, to be replaced.

A review of the cross sections included with the functional plans indicate that **noise barrier walls** are being considered as far west as I-24 Station 56+00. It should be noted that the surcharge load of noise walls (where required) must be considered in the design of the proposed retaining walls discussed in this report. The intervals where noise walls are required adjacent to retaining walls are noted in the discussion of the site conditions along each retaining wall. It is understood that the Design-Build (DB) team may alter the height and offset from centerline of a noise wall if it meets the Department's noise abatement criteria.

#### 1.2 PURPOSE AND SCOPE OF EXPLORATION

This report is being submitted as a supplement to the baseline report of the geotechnical conditions prepared by K. S. Ware and Associates, L.L.C. (KSWA), and submitted to Neel-Schaffer, Inc. in May of 2018. This preliminary data, in addition to the supplemental data collected by GeoEngineers for Neel-Schaffer in 2022, is used for evaluation and cost estimation for the preparation of the 30% Design Package being prepared by Neel-Schaffer. This report makes use of the drilling data performed for the KWSA report, particularly at the 3 bridge sites, as well as the additional borings performed in the vicinity of the 10 retaining walls listed above. Foundation data from the plans for the existing bridges, as well as from the recently constructed I -24 over Germantown Road bridge and the Belvoir Avenue over I-24 bridge has also been examined. The scope of services performed does not constitute all geotechnical exploration work necessary for design of the complete project. This report and portions of the earlier KSWA report are intended as information to assist prospective Design/Build teams in understanding the subsurface conditions present along the alignment. Additional geotechnical work will need to be performed to provide design studies compliant with TDOT's geotechnical manual for each structure and road alignment.

Exploratory test borings were previously drilled at the bridges as part of the KSWA report, and these will be referenced in this report. Additional borings have been documented by GeoEngineers for Neel-Schaffer along the walls proposed along I-24 and I-75 for the widened interstate or new ramps.

It should be noted that drilling access for this preliminary report was restricted to areas that did not require the removal of trees, the construction of dozer roads, and the installation of erosion prevention and sediment control (EPSC) measures. Due to those restrictions, the borings were offset from the proposed wall face, and is it expected that the Design-Build team will be able to locate borings along the final wall locations.

Figure 2 in Appendix A shows the approximate location of each of the exploratory borings.

The following table from the KSWA report summarizes the exploration previously performed for Phase II.

**Table 1 Summary of KSWA Test Borings** 

LOCATION	QUANTITY	BORING PREFIX	COMMENTS		
LOCATION					
		Phase I and Phase II			
Alignment Borings	21	A	Terminated at 15 ft or Refusal		
			Designated as L for travel lane or S for		
Pavement Coring	13	В	shoulder, two coreholes at each		
			location		
		Phase II			
CSX Railroad	3	CSX	Borings drilled from interstate		
COA Ramoad	3	CSA	shoulder		
MaRrian Pond Bridge	2	McB	McB-1 and MCB-2 drilled from		
McBrien Road Bridge	2	IVICD	McBrien Road		
M D 1D:1	0		M-1 drilled from Moore Road, M-2		
Moore Road Bridge	2	M	drilled from shoulder of I-24 EB		

It should be noted that 6 of the 21 borings with the boring prefix A are located in Phase II. Borings A-01 and A-02 were performed north of the CSX Railroad bridge, immediately south of the East Brainerd Road exit. Borings A-08, A-09, A-10, and A-11 were performed between I-24 Station 130+00 and the Spring Creek Road bridge. The logs for these borings have been attached to this report.

Field sampling and test procedures are described in Appendix B. The Test Boring Logs which detail the subsurface conditions encountered at each test boring location are included in Appendix B. The field testing procedures used for drilling and sampling are also included in Appendix B.

#### 2.0 GEOLOGIC CONDITIONS

#### 2.1 SITE GEOLOGY

As outlined in the KSWA report, the site is located in Chattanooga, Tennessee within the Valley and Ridge Physiographic Province. The Valley and Ridge is characterized by folded sedimentary rock composed of limestone, dolomite, sandstone, shale, and siltstone. Folding of the units formed as systems of anticlines and synclines developed. The forces causing the folding also resulted in the formation of a series of faults throughout the Valley and Ridge. In the Chattanooga area, many of the faults are low-angle, shallow, thrust faults. This type of faulting in conjunction with the folding resulted in many nonconformable contacts between geologic units.

The majority of the total project area is underlain by Ordovician-aged carbonate rock collectively called the Chickamauga Supergroup. The Supergroup is composed of the equivalent units of the Chickamauga Group (Reedsville Shale, an unnamed limestone unit, Moccasin Formation, Bays Formation, Ottosee Shale, Holston Formation (red limestone), Lenoir Limestone, Athens Shale, and Sevier Shale) and the Nashville Group (Hermitage Formation and Bigby-Cannon Limestone, Leipers-Catheys Limestone). Locally, the Chickamauga Group consists of mostly limestone units with some minor shale.

At the northern end of the project area, the site is underlain by the Knox Group. The geologic map in Appendix A of the KSWA report also indicates the Knox Group beneath the western end of the project, west of approximate Station 130+00, with the geologic contact mapped along Wando Drive south of I-24, and along Parkdale Avenue (Amhurst Avenue on the map) north of I-24. The Knox Group is an undifferentiated grouping of siliceous limestone and dolomites (Newala Formation, Mascot Dolomite, Kingsport Formation, Longview Dolomite, Chepultepec Dolomite, and Copper Ridge Dolomite). Zones of sandstone shale and quartzite are also contained in the group.

Geologic maps indicate that a thrust fault zone is present at the contact between the Chickamauga and the Knox in the northern portion of the site, approximately following the CSX Railroad crossing of the project site. The change can be observed in the area topography, where the ground at lower elevations with minor topographic undulations generally indicate areas underlain by the Chickamauga Super-Group, while the area of the site where the hillier areas are located generally indicate areas underlain by the Knox. A generalized geologic map from the public domain is provided as Appendix A, Figure 4.

#### 2.2 GEOLOGIC HAZARDS

Many of the faults in the area are considered incapable or inactive. However, earthquakes are known to occur within the region. Past events generally point to lower magnitude events located at relatively short distances to the epicenter, or greater magnitudes at greater distances to the epicenter. The higher magnitude events potentially impacting the area include the New Madrid Fault Zone and fault system located near Charleston, South Carolina. It is assumed that the seismic hazard, specifically the acceleration spectrum (peak ground acceleration coefficient, and the short- and long-term spectral acceleration coefficients) will analyzed using the General Procedure outlined in Section 3.10.2.1 of the AASHTO LRFD Bridge Design Specifications, Ninth Edition, 2020.

The site is located in an area underlain by carbonate bedrock. Limestone and dolomite, to a lesser extent, are subject to chemical solution weathering, especially along predisposed planes of weakness, such as faults, joints and bedding planes. Such weathering often results in the formation of irregular rock surfaces, including: pinnacles, slots, sloping surfaces, clay filled seams and open cavities. Water moving through the subsurface system can create erosion channels, which over time may increase in size. These channels can lead to the formation of underground voids and ultimately sinkholes.

It should be noted that no active sinkholes were observed while reconnoitering the area to be impacted by Phase II of the subject project. However, because of the geologic conditions, the risk of sinkholes is present within the project area.

#### 3.0 SITE CONDITIONS

#### 3.1 I-75 STATION 440+00 TO STATION 476+00

The KSWA report noted that Interstate 75 near Exit 4 begins in rolling terrain and slopes down to lowerlying areas with less topographic relief. The roadways through this area are primarily constructed on fill embankments to maintain grades and elevate the roadway above adjoining flood prone areas. The borings performed in this interval as part of the KSWA investigation were logged as CSX-1, CSX-1A, CSX-2, CSX-3 near the beginning of this interval, and A-01 and A-02 at the end of this interval near exit 4. The

Neel-Schaffer borings in this interval are logged as RW8-1, RW10-1, RW10-2, RW11-1, RW11-1A, and RW11-2.

#### 3.2 I-24 STATION 56+00 TO STATION 95+50

Interstate 24 beginning west of Germantown Road is generally constructed on natural ground as I-24 approaches Belvoir Avenue. Parallel frontage roads are located on either side of the interstate east of Germantown Road, and also are generally constructed on natural ground, although not at the same elevation as the interstate. West of Germantown Road, dense vegetation has become established outside of the shoulder, which may create an obstacle to drilling access for the proposed noise barrier walls.

#### 3.3 I-24 STATION 95+50 TO STATION 175+00

Interstate 24 beginning between Germantown Road and Belvoir Avenue is generally constructed on natural ground or relatively thin fill sections as I-24 approaches the Spring Creek Road overpass. Parallel frontage roads located on either side of the interstate are generally at higher elevations than the interstate traffic lanes. In many areas along this interval, dense vegetation has become established, which may create an obstacle to drilling access for the final design plans, particularly for the proposed retaining walls.

#### 4.0 SUBSURFACE CONDITIONS

#### **4.1 PAVEMENT CORING**

The existing pavement conditions in Phase II were explored by KSWA with 8 pavement cores, numbered B-10 through B-13 (BL stands for core hole in lane, BS stands for core hole in shoulder). TDOT crews surveyed the general boring locations. KSWA located the pavement cores at each location, although documentation of the survey data is not included in the KSWA report. It is assumed that the borings with the BL prefix were located in the outside lane, and the borings with the BS prefix were located on the adjacent shoulder. The approximate location of the KWSA coring locations were shown in Figure 2 of Appendix A of the KSWA report, and snapshots of the Figure showing the Phase II locations are shown below:

Figure 1: Excerpt of KSWA Pavement Coring Location Plan





The pavement thicknesses encountered by KSWA within Phase II are listed below in Table 2.

Table 2: Summary of Pavement Thicknesses from KSWA Coring

		TRAVEL LA	NE		SHOULDER						
Boring No.	Pavement type	Pavement Thickness	Base Material Thickness	<u>Total</u> <u>Thickness</u>	Boring No.	Pavement type	Pavement Thickness	Base Material Thickness	<u>Total</u> <u>Thickness</u>		
		<u>(in.)</u>	<u>(in.)</u>	<u>(in.)</u>			<u>(in.)</u>	<u>(in.)</u>	<u>(in.)</u>		
BL-10	Concrete	11 3/4	8	19 3/4	BS-10	Asphalt	8 3/4	19 1/4	28		
BL-11	Concrete	12 1/4	9 1/4	21 1/2	BS-11	Asphalt	5	17 1/4	22 1/4		
BL-12	Concrete	12 1/2	25 1/2	38	BG-12	Concrete	10	24	34		
BL-13	Concrete	10 1/2	10 1/2	21	BS-13	Asphalt	10	13	23		

Note that core sites B-10 and B-11 are located on I-75, with B-12 and B-13 are located between Belvoir Avenue and Moore Road on I-24.

Additional pavement coring and in-situ subgrade testing was performed beneath each lane of I-24 between Stations 140+00 and 164+40, and those coring locations are shown on the Neel-Schaffer boring location sheets in Appendix A, with the prefix EB or WB. The pavement thicknesses encountered by GeoEngineers/Neel-Schaffer are listed below in Table 3:

Table 3: Summary of Pavement Thicknesses from GeoEngineers/Neel-Schaffer Coring

Boring No.	Station	<u>Lane</u>	Pavement Type	Pavement Thickness (in.)	Base Material Thickness (in.)	Total Thickness (in.)
EB-1	140+00	Outside EBL	Concrete	12	7	19
WB-3	145+00	Inside WBL	Concrete	12	4.5	16.5
EB-2	150+00	Middle EBL	Concrete	12	7	19
WB-2	155+00	Middle WBL	Concrete	12	7	19
EB-3	160+00	Inside EBL	Concrete	12	6	18
WB-1	164+40	Outside WBL	Concrete	12	8	20

**Dynamic Cone Penetrometer (DCP) Tests** - To evaluate the consistency and pavement support characteristics in the underlying soil, DCP tests were performed at some locations. The DCP values were used to estimate the California Bearing Ratio (CBR) of the subgrade material.

From the DCP test results, the following CBR Values were estimated. Below is the result of the DCP test performed by KSWA within the limits of Phase II. Note that the location is estimated from examining the coring location layout sheet.

**Table 4: Estimated CBR Values from KSWA Testing** 

Boring No.	Station	<u>Lane</u>	Estimated CBR Value
B-13	120+00 <u>+</u>	Outside WBL	11

The estimated CBR values from the in-situ testing by Neel-Schaffer are shown in the table below:

Table 5: Estimated CBR Values from GeoEngineers/Neel-Schaffer Testing

Boring No.	<u>Station</u>	Station Lane			
EB-1	140+00	Outside EBL	31		
WB-3	145+00	Inside WBL	13		
EB-2	150+00	Middle EBL	24		
WB-2	155+00	Middle WBL	37		
EB-3	160+00	Inside EBL	31		
WB-1	164+40	Outside WBL	45		

Of particular interest to the Department was the section of I-24 between approximate Stations 140+00 and 164+50. GeoEngineers performed a series of continuous DCP tests at each location listed above, from the top of soil subgrade/bottom of base stone to a depth of 500 mm (19.7 inches) below the top of subgrade. The tests at 5 of the 6 locations encountered a subgrade with a CBR value reflective of a compacted clay that has remained at optimum moisture content. However, the CBR values at WB-3, located in the left inside lane at Station 145+00, are indicative of perched/trapped water. Note that the relatively high CBR at the end of the test interval increases the average CBR value in this series of tests. It also indicates reduced moisture content with depth. The results at WB-3 are shown below:

Table 6: CBR Estimates based on DCP at WB-3

Boring ID: WB-3

Doning ib.							
Number of Blows	Cumulative Pentration (mm)	Penetration Between Readings (mm)	Penetration per Blow (mm)	Hammer Factor <sup>1</sup>	DCP Index (mm/blow)	USCS Classifcation	Estimated CBR (%)
3	50	50	17	2	33	CL	6
4	100	50	13	2	25	CL	8
5	150	50	10	2	20	CL	10
3	200	50	17	2	33	CL	6
3	250	50	17	2	33	CL	6
5	300	50	10	2	20	CL	10
7	350	50	7	2	14	CL	15
18	400	50	3	2	6	CL	43

Average CBR (%) = 13

Compare the values above to those at EB-1, which is typical of the other 5 test sites:

Table 7: CBR Estimates based on DCP at EB-1

Boring ID: EB-1

Number of Blows	Cumulative Pentration (mm)	Penetration Between Readings (mm)	Penetration per Blow (mm)	Hammer Factor <sup>1</sup>	DCP Index (mm/blow)	USCS Classifcation	Estimated CBR (%)
9	50	50	6	2	11	CL	20
11	100	50	5	2	9	CL	25
15	150	50	3	2	7	CL	35
18	200	50	3	2	6	CL	43
10	250	50	5	2	10	CL	22
16	300	50	3	2	6	CL	37
14	350	50	4	2	7	CL	32

Average CBR (%) = 31

All of the DCP test results are in Appendix B.

It should be noted that TDOT typically performs CBR lab tests on samples that are compacted to optimum density and then submerged in order to account for the possibility of water accumulation. It is therefore likely that a relatively low CBR value was utilized in the design of the existing pavement structure, and the other areas tested could be considered to be over-designed.

#### 4.1.1 SUBGRADE RECOMMENDATIONS

It is recommended that pavement design within this interval be based on subgrade with a CBR of 6, with good drainage being provided through the use of drainage layers of stone or underdrains in poorly drained areas. Improvements to the subgrade may be needed in some areas of the lane widening to improve the conditions below existing shoulders and grassed areas alongside the interstate. Imported fill used to construct embankments should be of sufficient quality to produce a CBR value of at least 6.

#### 4.2 SOIL AND BEDROCK CONDITIONS

Soil encountered by the borings varied along the alignment. On the I-75, or north portion, it generally encountered existing fill soil underlain in some cases by alluvial soil, followed by residual soil before encountering auger refusal. Two of the alignment borings performed by KSWA, located near I-75 exit 4, planned for a depth of 15 feet below the ground surface, reached the termination depth without encountering auger refusal or reaching the bottom of the existing fill interval. On the I-24, or west portion of Phase II, existing fill soils and residual soils were encountered along the frontage roads, and the existing interstate was underlain by residual soil of widely varying depth.

The bedrock encountered in most of the borings where rock was cored consisted of hard, gray, argillaceous, limestone with seams of dark gray shale. Based on the elevations where auger refusal was encountered, weathering of the limestone appears to have created an undulating surface, with areas of localized weathering where the bedrock surface has near vertical weathering features creating slots of deeper soil cover. In these areas, locally steep sloping rock is present. This was noted in several locations where the steep surface caused drilling tools to wander, following the angle of the rock surface. In some of these cases, the condition was severe enough to cause the boring to be abandoned as noted on the

logs. Rock quality was generally good to excellent after penetrating the upper 1 to 5 feet of bedrock. Lower-quality rock was encountered in some locations at greater depth, but appeared to be a more aberrant condition in this formation.

The following sections describe the conditions in more detail, focusing on differences or highlights to the descriptions given above. Additional information can be found on the boring logs, including natural moisture and Atterberg limit data. Laboratory test results not shown on the borings logs are provided in Appendix B of this report.

#### 4.3 I-75 STATION 440+00 TO STATION 450+00

The KSWA report noted that alluvial soils, consisting of silty clay, clayey silt and intervals of brown sand were encountered along the northern side of the embankment fill for the recently completed Phase I construction. Similar soils were encountered below the embankment by borings performed from the right shoulder of I-75. North of the CSX railroad, the embankment was underlain by residual soil.

#### 4.3.1 RETAINING WALL 8, STATION 443+00 TO STATION 447+00, LEFT OF CENTERLINE

KSWA boring CSX-3 was drilled from the left shoulder near approximate Station 447+00, encountering 22 feet of medium stiff to stiff clay fill underlain by 25 feet of very moist to moist stiff residual clay. Neel-Schaffer boring RW8-1 was performed along the left shoulder at Station 443+62, indicating 35 feet of fill over 13 feet of silty clay. Below is an excerpt from the GeoEngineers/Neel-Schaffer boring summary table showing the additional boring performed for Wall 8:

Table 8: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 8

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments
RW8-1	443+62.2	77.9' Lt.	703.6	48	X	655.6	Upper 35' medium stiff to stiff fill, over medium stiff to stiff residuum

See the attached KSWA log CSX-3 and GeoEngineers log RW8-1 for detailed descriptions of the boring profiles, including SPT blow counts.

#### 4.3.2 I-75 OVER CSX RAILROAD

The portion of Table 4 of the KSWA report that applies to I-75 over CSX Railroad is shown below:

Table 9: Summary of KSWA drilling at I-75 over CSX Railroad

Boring No.	Surface Elevation	Soil Drill Depth (ft)	Auger Refusal?	Depth Cored (ft)	Total Depth	Existing Fill Thicknes s (ft)	Elev GW (ft)	Approximate Top of Rock Elevation	Base of Signficant Weathering Elevation	Comments			
	Bridge over CSX Railroad												
CSX-1	720.9	86.9	YES	7.4	94.3	28.5	X	634	X	Irregular rock surface, hard abrasive rock, no recovery FAULT ZONE			
CSX-1A	720.9	72.5	YES	7.8	80.3	1.5	X	648.4	X	Irregular rock surface, hard abrasive rock, no recovery FAULT ZONE			
CSX-2	715.5	55	YES	14	69	18.5	X	660.5	656				
CSX-3	716.0*	57.9	YES	14.8	72.7	22	X	658.1	656	Hard rock, siliceous, low grade metamorphism, brecciated dolomite			

The rock compressive strength varied widely at the railroad bridge. The wide range of rock compressive strengths between the samples taken from near the same elevation but opposite sides of I-75 is notable. However, this difference will likely not affect the end bearing piles expected to achieve refusal on the rock surface near elevation 650 along most of the bridge site.

Table 10: Summary of KSWA Compressive Strength Testing from CSX Railroad over I-24

Test Boring Number	Depth of Sample <sup>2</sup> (feet)	Compress (psi) <sup>1</sup>	ive Strength (ksf) <sup>1</sup>
CSX-2	58.4-58.8	14,253	2,050
CSX-2	64.1-64.5	27,594	3,970
CSX-3	64.0-64.4	6,785	970

Below is a snip of the boring table included in the original bridge plans:

Table 11: Ground and Rock Elevation Data from Original I-24 over CSX RR Bridge Plans

	BORINGS											
Hole	Hole Station Offset Ground El. Rock El. Hole Station Offset Ground El. Rock El.											
/	75+96	64'Lt.	700.0	651.0	9	76+50	24 Rt.	710.9.	650.9			
2	76+20	24'1+	707.6	653.6	10	76+57	70'Rt.	720.4	650.4			
7	77+15	64 Lt.	709 3	647.3	/5	77+7/	24'Rt.	716.4	652.4			
8	77+38	24'Lt.	711. 2	647.2	16	78 +05	64'Rt.	7/7.5	647.5			

Boring locations are referenced to & 1-502

The table above indicates a relatively uniform rock surface between elevations 647.2 and 653.6. It should be noted that KSWA borings CSX-1 and CSX-1A, located on the left shoulder of I-24 immediately east of the existing bridge abutment, indicated the possibility of deeper refusal depths along the proposed 2<sup>nd</sup> abutment due to the presence of the thrust fault noted above. It is assumed that the abutments and bent foundations of the replacement bridge will be placed on end-bearing piles.

#### 4.4 I-75 STATION 450+00 TO STATION 476+00

The KSWA report stated that borings drilled from the shoulder in this area encountered relatively thick intervals of existing fill, about 20 to 30 feet, before residual soil was encountered, and the additional Neel-Schaffer borings have indicated similar conditions. The fill and the underlying residual soil was generally composed of reddish-brown, yellowish-brown and light brown silty clay containing chert fragments and some sand. Sand in this soil was typically seen as remnants of weathered chert. These soils are typical of the type of soil encountered in areas underlain by the Knox Group. It should be noted that chert fragments can inflate SPT blow counts.

The KSWA report also noted that bedrock encountered by the borings CSX-1 through CSX-3 was composed of hard, gray, siliceous dolomite. Calcite healed fractures were common in the recovered core. Drilling operations reported slow penetration rates and above normal wear on drilling tools. At CSX-1 and the offset boring drilled after CSX-1 was abandoned, floating brecciated rock above the steeply sloping surface was noted. Both attempts as CSX-1 were unsuccessful in recovering measurable rock core. As noted previously, it is believed this location is within or near a thrust fault zone.

#### 4.4.1 RETAINING WALL 10, STATION 454+50 TO STATION 456+00, RIGHT OF CENTERLINE

Neel-Schaffer borings RW10-1 and RW10-2 were performed along the right shoulder of I-24 NB at Stations 455+03 and 456+04, respectively, indicating 20 to 23 feet of fill over medium stiff silty clay. Each boring was terminated at a depth of 50 feet without encountering in-place rock. Below is an excerpt from the Neel-Schaffer boring summary table listing the additional borings performed for this wall:

Table 12: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 10

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)		Approximate Top-of-Rock Elevation	Comments
RW10-1	455+02.8	62.6' Rt.	727.26	50	X	X	Upper 20' medium stiff to stiff fill, over medium stiff to stiff residuum
RW10-2	456+04.6	62.3' Rt.	727.8	50	X	X	Upper 23' medium stiff to stiff fill, over residuum with chert

See the attached logs for Retaining Wall 10 for detailed descriptions of the boring profiles, including SPT blow counts.

#### 4.4.2 RETAINING WALL 11, STATION 460+50 TO STATION 463+00, RIGHT OF CENTERLINE

Neel-Schaffer borings RW11-1, RW11-1A, and RW11-2 were performed along the right shoulder near Stations 461+00 and 463+00, respectively. Relatively high N-values were indicated at the 2 borings located right of Station 460+50 before auger refusal, possibly on heavy chert or rock fill. The boring located right of Station 463+00 was advanced through approximately 15 feet of clay fill before being terminated in residual clay at a depth of 50 feet.

Table 13: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 11

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments
RW11-1A	460+92.6	62.6' Rt.	732.2	17	X	715.2	Clay fill with moderately heavy chert, possible refusal on rock fill
RW11-1	460+99.5	62.8' Rt.	732.3	7.5	X	724.8	Clay fill with moderately heavy chert, possible refusal on rock fill
RW11-2	463+04.4	61.5	733.3	50	X	X	Upper 15' clay fill with chert, over residuum with chert.

See the attached logs for a detailed description of the boring profile, including SPT blow counts.

#### 4.5 I-24 STATION 56+00 TO STATION 99+00

The foundation data sheet from the plans for the recently completed I-24 over Germantown Road bridge replacement lists 12 borings that encountered irregularly weathered rock at depths of between 127.9 and 199.8 feet. It is estimated that the borings for the bridge are located between approximate I-24 Stations 73+00 and 74+00. It should be noted that the stationing used in the plans for the recently completed bridge replacements do not match the stationing for the interchange project.

At the time of this writing, no additional drilling has been performed between Station 56+00 and Germantown Road, and between Germantown Road and Belvoir Avenue. It should be noted that the rock surface was encountered at such depths at both bridges that it is not likely to be a factor in the design of any retaining walls or noise barrier walls proposed between Germantown Road and Belvoir Avenue.

A review of the cross sections indicates that roadway and embankment widening is proposed immediately east of Germantown Road, or near Station 75+00. Based on the drilling information obtained for the replacement of the I-24 over Germantown Road bridge, this interval is likely to be underlain by deep residual soils.

#### 4.6 I-24 STATION 96+50 TO STATION 117+50

The foundation data sheet from the plans for the recently completed Belvoir Avenue over I-24 bridge replacement lists 8 borings that encountered irregularly weathered rock at depths of between 44.3 and 76.3 feet. According to the preliminary plans, the borings for the bridge are located between Stations 99+75 and 101+00. With the exception of the 2 holes located left of Station 103+00, which refused near 12 feet, the Neel-Schaffer borings performed along the proposed wall sites in this interval (Walls 1, 4, and 5) obtained auger refusals at depths as shallow as 26.6 feet, while the majority were terminated at 50 feet without encountering rock. See Table 17 for a summary of the wall borings. The bedrock that was cored by KSWA at the one bridge in this section was very highly weathered with thick clay-filled zones encountered below the auger refusal/top-of-rock elevation.

#### 4.6.1 RETAINING WALL 1, I-24 STATION 96+50 TO STATION 113+00, LEFT OF CENTERLINE

Prior to the drilling performed for this report, 3 borings were performed between approximate Stations 109+75 and 101+50 by KSWA for the Belvoir Avenue over I-24 bridge replacement, as shown below:

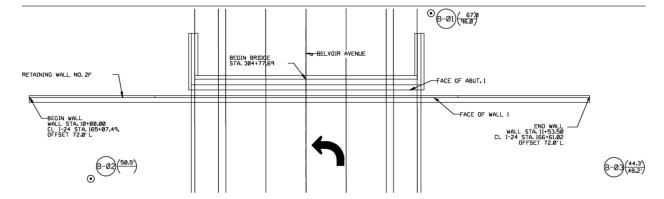


Figure 2: Excerpt of KSWA Retaining Wall Boring Location Plan

Two borings were located along the interstate shoulder, and one was located near the intersection of North Terrace Road and Belvoir Avenue. These borings indicated deep, medium stiff to stiff clay soils along this area. Note that the centerline of the bridge crosses I-24 near Station 100+50, and the I-24 stationing shown on the drawing snip does not apply. It should also be noted that an MSE wall has been constructed in this area, and Wall 1 has been designed to tie-in to this wall, particularly east of Belvoir Avenue.

Seven additional borings were performed by Neel-Schaffer along the proposed cut wall site, which begins approximately 100 feet west of the recently completed Belvoir Avenue over I-24 bridge replacement. With the exceptions of Borings RW1-1 and RW1-1A, which achieved auger refusals at approximately 12 feet, the borings indicated a relatively deep (25 to over 50 feet) irregularly weathered rock surface. Standard Penetration Tests (SPTs) performed on the overburden produced N-values that were typically between 7 and 15, reflective of medium stiff to stiff clays. Please refer to the boring logs

Offset 38' north of wall, soft 13'-20', boring terminated at 50'

Offset 100' east of end of wall, boring terminated at 50'

for additional information. The preliminary wall concept drawings are based on the assumption that depending on the wall height, anchored and unanchored pile and lagging walls will be the preferred wall type. Below is a summary table of the additional borings performed along Wall 1:

Approximate Boring Offset Surface Soil Drill Elev. GW I-24 Station Top-of-Rock Comments From C/L Elevation Depth (ft) (ft) No. Elevation I-24 Walls Retaining Wall 1 RW1-1A 102+76.25 130.2' Rt. 752.9 11.8 741.1 Offset 12' west of RW1-1 to confirm shallow refusal RW1-1 102+88.65 129.7' Lt. 12 741.3 Offset 53 ' north of wall, shallow refusal 753.3 X RW1-2 104+51.44 127.8' Lt. 757.35 44.7 712.65 Offset 49' north of wall, medium stiff to stiff clay RW1-3 106+01.91 130.8' Lt. 757.9 50 728.4 Offset 36' north of wall, boring terminated at 50' X RW1-4 | 107+50.12 | 128.9' Lt. 753.7 26.6 X 727.1 Offset 39' north of wall, medium stiff to stiff clay

Table 14: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 1

See the attached logs for a detailed description of the boring profiles, including SPT blow counts.

X

X

727.2

678

50

The retaining wall built for the north abutment of the recently completed Belvoir Avenue bridge replacement extends between approximate stations 99+75 and 101+25. This MSE wall was constructed with the use of soil nail excavation support, and a review of the contractor records included verification and proof test data performed on the soil nails. It was noted that a design bond strength of 750 psf was used in determining the loading schedule of the verification test nail, which was located at the north abutment. The verification test load of 2 times the design load, or 1,500 psf, was held for 10 minutes before the nail was loaded to 2.76 times the design load without pullout failure.

#### **North Terrace Road**

RW1-5

RW1-6

108+95.9

113+95

127.6' Lt.

86.1' It.

745.2

While drilling along the shoulder of North Terrace Road, it was observed that the asphalt curb along the frontage road had been displaced between approximate Stations 105+00 and 109+50, and it was noted that the pavement of the shoulder and left lane was cracked and broken in a pattern indicative of long-term slow movement of the cut slope above I-24. Proposed Wall 1 should help stabilize the toe of the slope above I-24, but not necessarily the entire slope. It is assumed that the scope of work for the final design will specify stabilizing the upper part of the slope. It is likely that this will affect the loading and possibly the height of Wall 1 within the interval that the Design-Build (DB) team determines is unstable or marginally stable.

#### Noise Wall Proposed Between Wall and North Terrace Road

Another factor in the design of some segments of Wall 1 will be the surcharge load from the noise wall proposed/required between Wall 1 and North Terrace Road. Inspection of the Functional Plans cross sections indicate that a noise wall will be required between the retaining wall and North Terrace Road from the beginning of the wall to Station 100+00, and from approximate Station 106+00 to the end of the wall. As mentioned in Section 1.1, it is understood that the Design-Build team may alter the height and offset from centerline of a noise wall if it meets the Department's noise abatement criteria.

#### 4.6.2 RETAINING WALL 4, I-24 STATION 105+10 to STATION 115+60, RIGHT OF CENTERLINE

Four offset borings were performed along the proposed cut wall site, which begins approximately 400 feet east of the recently completed Belvoir Avenue over I-24 bridge replacement. Borings RW4-1 through RW4-4 indicated from 28.5 to over 50 feet of clay over an irregularly weathered rock surface. Standard Penetration Tests (SPTs) performed on the overburden produced N-values that were typically between 10 and 16, reflective of medium stiff to very stiff clays. The Neel-Schaffer borings for Wall 4 that are listed in Table 17 are shown below:

				•			
Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments
RW4-1	105+12	117.3' Rt.	736.4	50	699.4	X	Offset 36' south of wall, medium stiff to stiff clay, wet at 33.5'
RW4-2	107+94.3	115.4' Rt.	738	50	706	X	Offset 31' south of wall, medium stiff to stiff clay, wet at 34'
RW4-3	111+02.5	114.8' Rt.	734.2	28.5	X	705.7	Offset 25' south of wall, medium stiff to stiff clay
RW4-4	113+88.8	119.8' Rt.	719.4	45	X	674.4	Offset 15' south of wall face, medium stiff to stiff clay

Table 15: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 4

See the attached logs for a detailed description of the boring profiles, including SPT blow counts.

#### Noise Wall Proposed Between Retaining Wall and South Terrace Road

Another factor in the design of some segments of Wall 4 will be the surcharge load from the noise wall required between the proposed retaining wall and South Terrace Road. Inspection of the Functional Plans cross sections indicate that a noise wall will be required between the retaining wall and south Terrace Road from Station 110+00 to approximate Station 113+15. As mentioned in Section 1.1, it is understood that the Design-Build team may alter the height and offset from centerline of a noise wall if it meets the Department's noise abatement criteria.

#### 4.6.3 RETAINING WALL 5, I-24 STATION 114+00 TO STATION 117+50, RIGHT OF CENTERLINE

Two borings were performed near the site of the proposed wall. Inspection of the Functional Plans cross sections indicates that the wall begins as a small cut wall and ends as a small fill wall, maintaining grade separation between I-24 eastbound and proposed Ramp K. Borings RW5-1 and RW5-2 indicated deep residual soils, with both borings terminated in clay at depth of 50 feet. Standard Penetration Tests (SPTs) performed in the upper 30 feet of soil produced N-values that were typically between 8 and 18, indicative of medium stiff to very stiff clays. Please refer to the boring logs for additional information. The GeoEngineers/Neel-Schaffer borings for Wall 5 that are listed in Table 33 are shown below:

Approximate Offset Surface Soil Drill Elev. GW Boring I-24 Station Top-of-Rock Comments From C/L Elevation Depth (ft) No. (ft) Elevation RW5-1 115+76.1 119.6' Rt. 710.8 50 X Offset 20' south of wall, stiff clay to 20', medium stiff below 20' X 117+90.1 70.3' Rt. 648.7 Offset east of end of wall, medium stiff to stiff clay

Table 16: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 5

#### 4.7 I-24 STATION 117+50 TO STATION 175+00

The KSWA report noted that except where fill soil was encountered, the residual soil profile in this area is relatively thin, less than about 15 feet, and in some cases less than 10 feet. Residual soils were found

to be composed of stiff to very stiff, brown and gray, silty clay. A layer of black to brown sand was encountered between about 1 and 3 feet below the surface in KSWA boring A-8, located within the median on the western side of Spring Creek Road.

The bedrock encountered at the two bridges in this section, Moore Road and McBrien Road overpasses, was different. At M-1 and M-2 (Moore Road), pink to dark red limestone and gray, brown and green calcareous shale was recovered. The rock quality varied from fair to good, but the recovery percentages were good to excellent. Fractured zones within the rock were common. Most of the fractures appeared to be closed but some weathering was encountered on open fractures. The higher degree of fracturing is believed to be related to a thrust fault zone located west of the project area. Bedrock encountered at McB-1 and McB-2 (McBrien Road) returned to the hard, gray, argillaceous limestone. The upper 5 feet of coring at McB-1 encountered significant weathering and mud seams. The remainder of the rock quality was good to excellent.

#### 4.7.1 RETAINING WALL 2, I-24 STATION 139+75 TO STATION 140+75, LEFT OF CENTERLINE

One additional boring was performed for this cut wall, which will support the north abutment of the Moore Road bridge over I-24. This boring was offset west of the beginning of the wall to Station 138+00, along the shoulder of the existing interstate. Boring RW2-1 obtained auger refusal at a depth of 10.3 feet, near elevation 669. As is shown in the discussion of the site conditions at the proposed bridge on the following page, KSWA boring M-1 is located north of Abutment 2, left of approximate I-24 Station 140+50. The upper 12 feet of soil at hole M-1 was logged as fill, and is a firm clay with an average N-value of 8. The lower soils are stiff to very stiff residual clays with an average N-value of 16. Prior to the construction of the existing bridge, eight rock soundings were performed across the site of the north abutment of the Moore Road bridge, which is also discussed in the following section. The surface of the underlying limestone along the wall site is expected to be encountered near elevation 670. Below is a summary table of the Neel-Schaffer boring performed along Wall 2:

Table 17: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 2

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	100,000,000,000,000	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments
RW2-1	139+08.6	76.2' Lt.	679.3	10.25	Х	668.75	Offset 75' west of beginning of wall, medium stiff to stiff clay

Please refer to KSWA boring log M-1 and Neel-Schaffer log RW2-1 for additional information.

#### 4.7.2 MOORE ROAD OVER I-24

The portion of Table 4 of the KSWA report that applies to Moore Road over I-24 is shown below:

Table 18: Summary of KSWA drilling at I-75 over Moore Road

Boring No.	Surface Elevation	Soil Drill Depth (ft)	Auger Refusal?	Depth Cored (ft)	Total Depth	Existing Fill Thicknes s (ft)	Elev GW (ft)	Approximate Top of Rock Elevation	Base of Signficant Weathering Elevation	Comments
								Moore Ro	ad Bridge	
M-1	699.7	30.1	YES	9.8	39.9	12	X	669.6	666	9.6 feet offset from stake
M-2	680.7	8.1	YES	26.2	34.3	1.6	X	672.6	657	

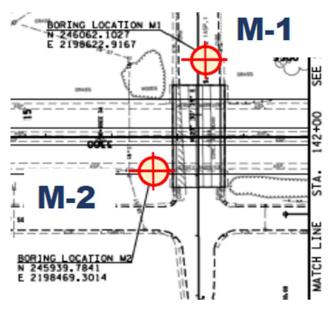
The rock compressive strength varied somewhat at this bridge. It should be noted that sample M-1 was taken from approximate elevation 768, which is near the rock surface, and the M-2 sample is from approximate elevation 753, or 19 feet below the rock surface. This difference in compressive strengths will likely not be a factor in the end bearing piles achieving refusal on the rock surface near elevation 670 along most of the bridge site. However, the compressive strength of the rock at depth would be an important factor in modeling the capacity of drilled shafts, if used at the center bent.

Table 19: Summary of KSWA Compressive Strength Testing from Moore Road over I-24

Test Boring Number	Depth of Sample <sup>2</sup> (feet)	Compress: (psi) <sup>1</sup>	ive Strength (ksf) <sup>1</sup>
M-1	32.1-33.2	2,614	370
M-2	27.3-27.7	6,230	890

Below is a snip from the KSWA report showing the approximate locations of borings M-1 and M-2:

Figure 3: Excerpt from Figure 3J in Appendix 1 of KSWA Report showing Moore Road Boring Locations



Note that boring M-1 was advanced through the entire fill thickness, while boring M-2 was located south of the interstate near the existing ditchline.

The preliminary layout for the replacement bridge indicates that Abutment 1 is south of I-24, and Abutment 2 is north of I-24. Sounding points 27 through 34 for the existing bridge were performed at the existing south abutment, or proposed **Abutment 1**:

Table 20: Ground and Rock Elevation Data from Original Bridge Plans, Abutment 1

Hole No.	Ground Elev.	Rock Elev.
27	682.2	671.2
28	*	*
29	682.7	671. 7
30	682.9	669. 9
31	682.7	669. 7
32	682.6	671.6
33	681.0	668.0
34	681.1	667.1

Based on the information provided in the 2018 KSWA report and the original bridge plans, it is assumed that end-bearing piles will be used at the south abutment, with an average pile tip refusal elevation of 670 expected.

Soundings 15 through 20 were located along the site of the **center bent**:

Table 21: Ground and Rock Elevation Data from Original Bridge Plans, Center Bent

Hole No.	Ground Elev.	Rock Elev.
15	678.5	667. 5
16	680.5	667.5
17	680.5	667.5
18	680.2	669.2
19	679.6	666.6
20	678. <b>4</b>	668.4

The plans for the existing bridge dated 1958 indicate that a bottom of footing elevation of 776.7 was proposed for both end columns. In the absence of as-built plans, and based on the existing drilling information, it is likely that some of the driven piles for this bent have slightly less than 10 feet of soil embedment. If a 10-foot minimum H-pile length is required at the center bent, it is anticipated that the rock will be pre-drilled as much as 3 feet prior to inserting the pile and backfilling the space around the pile with concrete.

It is assumed that core borings similar to those performed during the KSWA investigation will be needed to characterize the in-place rock at depth if the designer of the final bridge plans proposes to use spread footings or drilled shaft foundations.

Sounding points 1 through 8 were performed at the existing north abutment, or proposed **Abutment 2**:

Table 22: Ground and Rock Elevation Data from Original Bridge Plans, Abutment 2

Hole No.	Ground Elev.	Rock Elev.
/	679.4	668. 4
2	679.3	668. 3
3	679.5	666.5
4	679.5	667.5
5	679. 3	667. 3
6	679.3	669.3
7	677.9	670.9
8	677.9	669. 9

Based on the information provided in the KSWA report and the original bridge plans, it is assumed that end-bearing piles will be used at the north abutment, with an average pile tip refusal elevation of 668 expected.

#### 4.7.3 RETAINING WALL 6, I-24 STATION 131+50 TO STATION 144+50, RIGHT OF CENTERLINE

Six additional borings were performed for this cut wall, a section of which will support the south abutment of the Moore Road bridge over I-24. As shown in the discussion of the site conditions at the proposed bridge in the previous section, KSWA boring M-2 was located near the existing ditchline, and the Neel-Schaffer borings were located upslope of the proposed wall face, primarily along the shoulder of South Terrace Road. The additional borings obtained auger refusal at depths from 4.75 feet to 24.5 feet, as shown in the table below. The surface of the underlying limestone is expected to be encountered between elevations 665 and 685. Please refer to the boring logs for additional information. Below is a summary table of the additional borings performed along Wall 6:

Approximate Boring Offset Surface Soil Drill Elev. GW -24 Station Top-of-Rock Comments From C/L Elevation Depth (ft) (ft) No. **Flevation** 131+99.6 130.9' Rt. 689.8 679.8 RW6-1 10 X Offset 23' south of wall, medium stiff clay RW6-2 135+03.5 108.4' Rt. 688.8 4.75 Х 684.05 Offset 22' south of wall, medium stiff to stiff clay RW6-3 137+99 4 114.1 'Rt. 694.1 19 X 675.1 Offset 24' south of wall, medium stiff to stiff clay 24.5 RW6-4 139+50.4 114.4' Rt. 698 X 673.5 Offset 24' south of wall, medium stiff to stiff clay. Upper 5' fill. RW6-5 142+00 115.7' Rt. 695.4 22 673.4 Offset 28' south of wall, medium stiff to stiff clay. Upper 10' fill. RW6-6 143+75.8 98.0' Rt. 687.9 18.5 669.4 Offset 6' south of wall, medium stiff to stiff clay. Upper 5' fill.

Table 23: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 6

#### Noise Wall Proposed Between Retaining Wall and South Terrace Road

Another factor in the design of one of Wall 6 will be the surcharge load from the noise wall required between the proposed wall and South Terrace Road. Inspection of the Functional Plans cross sections indicate that a noise wall will be required between the retaining wall and South Terrace Road from approximate Station 133+50 to approximate Station 134+70. Unlike at other wall locations, it does not appear that the Design-Build team will have much room to alter the height and offset from centerline of a noise wall.

#### 4.7.4 MCBRIEN ROAD OVER I-24

The portion of Table 4 of the KSWA report that applies to McBrien Road over I-24 is shown below:

Base of Soil Drill Depth Approximate Boring Surface Auger Total Fill Elev GW Signficant Depth Cored Top of Rock Comments Elevatio Refusal Depth hicknes (ft) Weathering No. (ft) (ft) Elevation s (ft) Elevation McBrien Road Bridge Moved hole 12 feet NE, Elevation 0.5 foot lower than stake, Clay Seams in upper 5 MCB-1 697.2 27.2 YES 15.2 42.4 18.5 X 670 663 MCB-2 696.6 31.1 YES 11 42.1 16 665.5 661

Table 24: Summary of KSWA drilling at I-75 over Moore Road

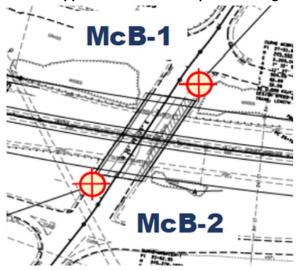
The compressive strength of the rock sample obtained near the rock surface at Boring MCB-2 is shown in the snip from Table 5 of the KSWA report.

Table 25: Summary of KSWA Compressive Strength Testing from McBrien Road over I-24

Test Boring	Depth of Sample <sup>2</sup>	Compressi	ve Strength
Number	(feet)	(psi)1	(ksf)1
MCB-2	31.7-32.1	3,801	550

Below is a snip from the KSWA report showing the approximate locations of borings MCB-1 and MCB-2:

Figure 4: Excerpt from Figure 3K in Appendix 1 of KSWA Report showing McBrien Rd. Boring Locations



The preliminary layout for the replacement bridge indicates that Abutment 1 is south of I-24, and Abutment 2 is north of I-24. Boring MCB-2 was performed near the existing south abutment, or proposed **Abutment 1**, indicating hard, argillaceous in-place limestone near elevation 665.5, at a depth of 31 feet.

Sounding points 27 through 34 for the existing bridge were performed at the south abutment, or proposed **Abutment 1**:

Table 26: Ground and Rock Elevation Data from Original Bridge Plans, Abutment 1

Hole No.	Ground Elev.	Rock Elev
27	672.8	664.8
28	672. <i>9</i>	664.9
29	673.0	666.0
<i>30</i>	674. /	665.1
3/	674.3	665.3
32	671.9	664.9
33	671.6	664.6
34	671.5	664.5

Based on the information provided in the 2018 KSWA report and the original bridge plans, it is assumed that end-bearing piles will be used at the south abutment, with an average pile tip refusal elevation of 665 expected.

Soundings 15 through 20 were located along the site of the **center bent**:

Table 27: Ground and Rock Elevation Data from Original Bridge Plans, Center Bent

Hole No.	Ground Elev.	Rock Elev.
15	672.8	666.8
16	673.1	666.1
17	674.4	665.4
18	674.5	665.5
19	673.5	664.5
20	673.6	665.6

The plans for the existing bridge indicate that a bottom-of-pile cap elevation of 773.3 was proposed for both end columns at the **center bent**. In the absence of as-built plans, and based on the existing drilling information, it is likely that some of the driven piles (if used) for this bent have slightly less than 10 feet of soil embedment. If a 10-foot minimum H-pile length is required at the center bent, it is anticipated that the rock will be pre-drilled as much as 3 feet prior to inserting the pile and backfilling the space around the pile with concrete.

It is assumed that core borings similar to those performed during the KSWA investigation will be needed to characterize the in-place rock at depth if the designer of the final bridge plans proposes to use spread footings or drilled shaft foundations.

KSWA boring MCB-1 was performed near the existing north abutment, or proposed **Abutment 2**, indicating weathered, argillaceous in-place limestone near elevation 670, at a depth of 27.2 feet. The boring indicates that the limestone becomes hard at a depth of 32.2 feet.

Sounding points 1 through 8 were performed at the existing north abutment, or proposed Abutment 2:

Table 28: Ground and Rock Elevation Data from Original Bridge Plans, Abutment 2

Hole No.	Ground Elev.	Rock Elev
/	<i>675.</i> /	668.1
2	674.5	667.5
3	<i>676.0</i>	668.0
4	676.5	666.5
5	676.7	667.7
6	676.9	666.9
7	677.0	669.0
8	677.5	668.5

Based on the information provided in the KSWA report and the original bridge plans, it is assumed that end-bearing piles will be used at the north abutment, with an average pile tip refusal elevation of 668 expected.

#### 4.7.5 RETAINING WALL 3, I-24 STATION 155+00 TO STATION 160+50, LEFT OF CENTERLINE

Three additional borings were advanced along this cut wall, part of which will also support the north abutment of the McBrien Road bridge over I-24. As shown in the discussion of the site conditions at the proposed bridge, boring McB-1 is located north of Abutment 2. Additional borings RW3-1, RW3-2, and

RW3-3 were offset left of the proposed wall face along the shoulder of North Terrace Road. The upper 10 to 20 feet of soil appears to be fill, and is a stiff clay with an average N-value of 10. The lower soils are stiff to very stiff residual clays with an average N-value of 18. Below is an excerpt from the summary table of the additional Neel-Schaffer borings listing the holes performed for Wall 3:

Table 29: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 3

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments	
RW3-1	155+14.8	167.9' Lt.	695.3	25	X	670.3	Offset 50' north of wall, medium stiff to stiff clay	
RW3-2	156+88.5	139.5' Lt.	694.4	23.5	X	670.9	Offset 49' north of wall face, stiff to very stiff clay. Predominantly fill.	
RW3-3	159+03.9	108.3' Lt.	687.9	25	X	663	Offset 18' north of wall face, medium stiff to stiff clay. Upper 15' fill.	

Please refer to KSWA boring log McB-1 and GeoEngineer/Neel-Schaffer logs RW3-1, RW3-2, and RW3-3 for additional information.

#### Noise Wall Proposed Between Wall 3 and North Terrace Road

Inspection of the Functional Plans cross sections indicate that a noise wall will be required between the retaining wall and North Terrace Road from east of McBrien Road near Station 157+00 to the end of the wall near Station 160+50. The surcharge load of the noise wall must be considered in the design of the proposed retaining wall, depending on its proximity to the retaining wall. As mentioned in Section 1.1, it is understood that the Design-Build team may alter the height and offset from centerline of a noise wall if it meets the Department's noise abatement criteria.

#### 4.7.6 RETAINING WALL 7, I-24 STATION 154+25 TO STATION 155+75, RIGHT OF CENTERLINE

Two additional borings were advanced along this cut wall, part of which will also support the south abutment of the McBrien Road bridge over I-24. As shown in the discussion of the site conditions at the proposed bridge, boring McB-2 is located south of Abutment 1. Additional borings RW7-1 and RW7-2, were located near Stations 154+50 and 155+50, respectively. The upper 16 feet of soil appears to be fill, and is a stiff clay, and the lower soils are stiff to very stiff residual clays. The surface of the underlying limestone is expected to be encountered near elevation 665.

Table 30: Summary of GeoEngineers/Neel-Schaffer drilling at Wall 7

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)		Approximate Top-of-Rock Elevation	Comments
RW7-1	154+60.2	110.9' Rt.	696	31	Х	665	Offset 20' south of wall, medium stiff to stiff clay
RW7-2	155+29.5	103.6' Rt.	697.2	34.5	Х	662.7	Offset 13' south of wall, medium stiff to stiff clay

Please refer to KSWA boring log McB-2 and GeoEngineer/Neel-Schaffer logs RW7-1 and RW7-2 for additional information.

#### **4.8 KSWA BORING SUMMARY**

The following table provides a summary of the KSWA borings, showing the surface elevations, thickness of fill encountered, auger refusal elevation, and estimated elevation of the start of good-to-excellent

quality rock. Additional information and comments about the conditions are also provided in the summary table. Conditions can vary from between locations, including significant variations even at close distances due to the nature of the weathering and variability in the surface of the bedrock. Please refer to the boring logs for additional information. Figures 5G, 5H, and 5I in Appendix A provides graphical summary diagrams for I-75 over CSX Railroad, Moore Road over I-24, and McBrien Road over I-24, respectively.

Base of Soil Drill Depth Approximate Boring Surface Auger Total Fill Elev GW Signficant Top of Rock Comments Depth Cored Weathering No. Elevation Refusal? Depth Thicknes (ft) (ft) Elevation s (ft) Elevation **Alignment Borings** 717.3 15 15 Cherty, silty, clay FILL A-02 718.7 15 NO X 15 15 X X X Cherty, silty, clay FILL A-08 673.9 14.7 YES X 14.7 3.5 659.2 Possible FOUNDRY SAND, could be RAP 673 YES 5.5 667.5 Shallow Refusal at 5.5 ft A-09 5.5 A-10 684.5 9.4 YES X 9.4 4.9 Х 675.1 A-11 680.5 YES 9.3 3.2 671.2 Moved hole to 4.9 offset Bridge over CSX Railroad CSX-1 720.9 86.9 YES 7.4 94.3 28.5 634 Irregular rock surface, hard abrasive rock, no recovery FAULT ZONE 720.9 648.4 Irregular rock surface, hard abrasive rock, no recovery FAULT ZONE CSX-2 715.5 55 YES 14 69 18.5 660.5 656 CSX-3 716.0\* 57.9 YES 14.8 72.7 22 658.1 656 Hard rock, siliceous, low grade metamorphism, brecciated dolomite Moore Road Bridge 9.6 feet offset from stake 30.1 M-2 680.7 8.1 YES 26.2 34.3 1.6 672.6 657 Moved hole 12 feet NE. Elevation 0.5 foot lower than stake. Clay Seams in upper 5 MCB-1 697.2 27.2 YES 15.2 42.4 18.5 X 670 663 MCB-2 696.6 31.1 YES 11 42.1 16 665.5 661

Table 31: Excerpt from Table 4 of KSWA Report

#### 4.9 GEOENGINEERS/NEEL-SCHAFFER BORING SUMMARY

RW3-3 159+03.9 108.3 Lt.

The following table provides a summary of the Retaining Wall borings logged by GeoEngineers for Neel-Schaffer, showing the ground surface elevations, auger refusal elevation, and estimated top-of-rock elevation. Additional information and comments about the conditions are also provided in the summary table. Conditions can vary from between locations, including significant variations even at close distances due to the nature of the weathering and variability in the surface of the bedrock. Please refer to the boring logs for additional information.

				•	_	-	•		
Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments		
	I-24 Walls								
	Retaining Wall 1								
RW1-1A	102+76.25	130.2' Rt.	752.9	11.8	X	741.1	Offset 12' west of RW1-1 to confirm shallow refusal		
RW1-1	102+88.65	129.7' Lt.	753.3	12	X	741.3	Offset 53 ' north of wall, shallow refusal		
RW1-2	104+51.44	127.8' Lt.	757.35	44.7	X	712.65	Offset 49' north of wall, medium stiff to stiff clay		
RW1-3	106+01.91	130.8' Lt.	757.9	50	728.4	X	Offset 36' north of wall, boring terminated at 50'		
RW1-4	107+50.12	128.9' Lt.	753.7	26.6	X	727.1	Offset 39' north of wall, medium stiff to stiff clay		
RW1-5	108+95.9	127.6' Lt.	745.2	50	727.2	X	Offset 38' north of wall, soft 13'-20', boring terminated at 50'		
RW1-6	113+95	86.1' Lt.	706	50	678	X	Offset 100' east of end of wall, boring terminated at 50'		
	Retaining Wall 2								
RW2-1	139+08.6	76.2' Lt.	679.3	10.25	X	668.75	Offset 75' west of beginning of wall, medium stiff to stiff clay		
	Retaining Wall 3								
RW3-1	155+14.8	167.9' Lt.	695.3	25	X	670.3	Offset 50' north of wall, medium stiff to stiff clay		
RW3-2	156+88.5	139.5' Lt.	694.4	23.5	X	670.9	Offset 49' north of wall face, stiff to very stiff clay. Predominantly fill.		

Table 32: Summary of GeoEngineers/Neel-Schaffer Retaining Wall Boring Data

663

Offset 18' north of wall face, medium stiff to stiff clay. Upper 15' fill.

Table 33: Summary of GeoEngineers/Neel-Schaffer Retaining Wall Boring Data (Continued)

Boring No.	I-24 Station	Offset From C/L	Surface Elevation	Soil Drill Depth (ft)	Elev. GW (ft)	Approximate Top-of-Rock Elevation	Comments			
I-24 Walls										
Retaining Wall 4										
RW4-1	105+12	117.3' Rt.	736.4	50	699.4	X	Offset 36' south of wall, medium stiff to stiff clay, wet at 33.5'			
RW4-2	107+94.3	115.4' Rt.	738	50	706	X	Offset 31' south of wall, medium stiff to stiff clay, wet at 34'			
RW4-3	111+02.5	114.8' Rt.	734.2	28.5	X	705.7	Offset 25' south of wall, medium stiff to stiff clay			
RW4-4	113+88.8	119.8' Rt.	719.4	45	X	674.4	Offset 15' south of wall face, medium stiff to stiff clay			
					Retaini	ng Wall 5				
RW5-1	115+76.1	119.6' Rt.	710.8	50	X	X	Offset 20' south of wall, stiff clay to 20', medium stiff below 20'			
RW5-2	117+90.1	70.3' Rt.	695.7	50	648.7	X	Offset east of end of wall, medium stiff to stiff clay			
					Retainir	ng Wall 6				
RW6-1	131+99.6	130.9' Rt.	689.8	10	X	679.8	Offset 23' south of wall , medium stiff clay			
RW6-2	135+03.5	108.4' Rt.	688.8	4.75	X	684.05	Offset 22' south of wall, medium stiff to stiff clay			
RW6-3	137+99.4	114.1 'Rt.	694.1	19	X	675.1	Offset 24' south of wall, medium stiff to stiff clay			
RW6-4	139+50.4	114.4' Rt.	698	24.5	X	673.5	Offset 24' south of wall, medium stiff to stiff clay. Upper 5' fill.			
RW6-5	142+00	115.7' Rt.	695.4	22	X	673.4	Offset 28' south of wall, medium stiff to stiff clay. Upper 10' fill.			
RW6-6	143+75.8	98.0' Rt.	687.9	18.5	X	669.4	Offset 6' south of wall, medium stiff to stiff clay. Upper 5' fill.			
					Retainir	ng Wall 7				
RW7-1	154+60.2	110.9' Rt.	696	31	X	665	Offset 20' south of wall, medium stiff to stiff clay			
RW7-2	155+29.5	103.6' Rt.	697.2	34.5	X	662.7	Offset 13' south of wall, medium stiff to stiff clay			
					I-75 W	alls				
Retaining Wall 8										
RW8-1	443+62.2	77.9' Lt.	703.6	48	X	655.6	Upper 35' medium stiff to stiff fill, over medium stiff to stiff residuum			
					Retaining V	Vall 10				
RW10-1	455+02.8	62.6' Rt.	727.26	50	X	X	Upper 20' medium stiff to stiff fill, over medium stiff to stiff residuum			
RW10-2	456+04.6	62.3' Rt.	727.8	50	X	X	Upper 23' medium stiff to stiff fill, over residuum with chert			
					Retaining V	Vall 11	·			
RW11-1A	460+92.6	62.6' Rt.	732.2	17	X	715.2	Clay fill with moderately heavy chert, possible refusal on rock fill			
RW11-1	460+99.5	62.8' Rt.	732.3	7.5	X	724.8	Clay fill with moderately heavy chert, possible refusal on rock fill			
RW11-2	463+04.4	61.5	733.3	50	X	X	Upper 15' clay fill with chert, over residuum with chert.			

#### 4.10 GROUNDWATER CONDITIONS

The KSWA report noted that groundwater was observed in some of the borings within the soil profile during drilling. Borings encountering water were generally those drilled within the interchange and/or near Spring Creek (located in Phase I) and those near South Chickamauga Creek (SCC and RW). In most cases, groundwater was found to occur in sand layers present in the alluvial soil in the lower-lying areas and trapped in loose fill materials in low-lying areas (especially in the interchange medians).

An examination of the moisture content tests performed by Geotechnics on samples obtained by GeoEngineers/Neel-Schaffer indicates soils with moisture contents above 30 percent below a depth of 32 feet, particularly along Retaining Walls 4 and 5. Although some isolated lenses of soils with relatively high moisture contents were indicated at other boring locations, an extensive, near-surface water table does not appear to be present along the I-24 retaining wall locations. It should be noted that groundwater levels will vary depending on the time of year, climatic conditions and the degree of construction activities.

#### **4.11 LABORATORY TEST RESULTS**

KSWA and Neel-Schaffer/Geotechnics performed the laboratory testing on split spoon and rock core samples in general accordance with ASTM and AASHTO procedures with results presented on the boring logs or in Appendix B where results require additional space for reporting. The laboratory testing included:

- Natural Moisture Content (AASHTO T 265 and ASTM D 2216-19)
- Atterberg Limit Determination (AASHTO T 89, T 90, and ASTM D 4318-17)
- Grain Size Analysis (AASHTO T 27 and ASTM D 422-63 (2007), AASHTO T88)
- Unconfined Compressive Test- Rock

Unconfined compressive strength of selected samples of rock by KSWA were determined by generally using applicable ASTM methods. Samples of weathered to moderately weathered rock and relatively unweathered rock samples were selected for testing to permit comparison. The results of the rock core compressive strength testing from the I-75 over South Chickamauga Creek, I-75 over CSX railroad, Moore Road over I-24, and McBrien Road over I-24 I are presented in this excerpt from Table 5 of the KSWA report.

**Table 34: Summary of KSWA Rock Core Compressive Strength Data** 

Test Boring Number	Depth of Sample <sup>2</sup> (feet)	Compressi (psi) <sup>1</sup>	ive Strength (ksf) <sup>1</sup>
CSX-2	58.4-58.8	14,253	2,050
CSX-2	64.1-64.5	27,594	3,970
CSX-3	64.0-64.4	6,785	970
M-1	32.1-33.2	2,614	370
M-2	27.3-27.7	6,230	890
MCB-2	31.7-32.1	3,801	550
SCC-1	20.9-21.1	3,194	460

Pounds per square inch (psi); Kips per square foot (ksf).

<sup>2</sup> All sample depths are approximate.

#### **5.0 QUALIFICATIONS OF RECOMMENDATIONS**

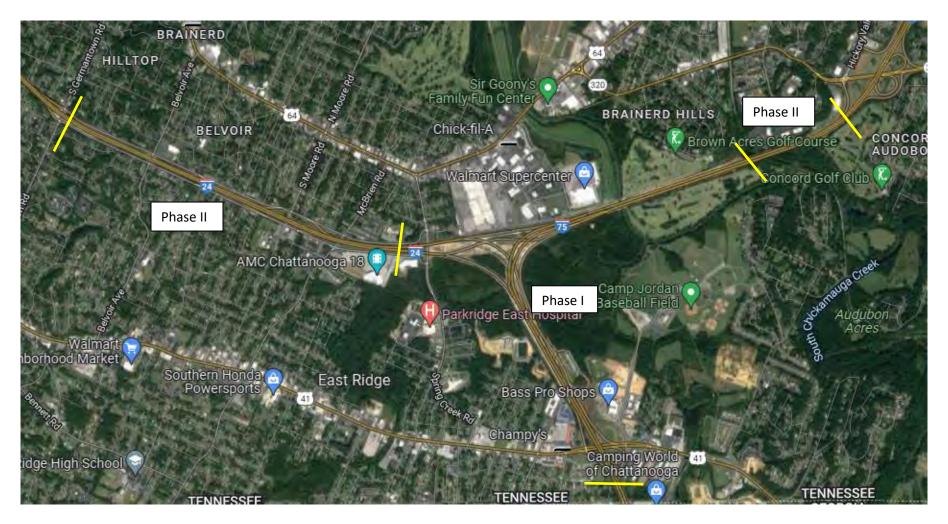
The conditions described in this report were interpreted from our observations at the site and using the information obtained from the test borings that were advanced at the site. Test borings only depict the soil and rock conditions at the specific location and time at which they were made. The soil and rock conditions at other locations on the sites may differ from those occurring at the boring locations.

The conclusions and recommendations for the design of pavements in this report were based on the available subsurface information, the project information provided, and the assumptions previously stated.

The scope of our geotechnical services did not include assessment or investigation for the presence or absence of hazardous or toxic materials in the soil, groundwater or surface water within or beyond the site studied.

Our professional services were limited to developing a geotechnical conditions baseline report and was not intended to act as a design geotechnical study for this project. Additional exploration and evaluation will be need to conform to the requirements of the TDOT Geotechnical Manual for each of the structures. Neel-Schaffer is not responsible for the conclusions, opinions, or recommendations made by others based upon the data included herein.

# APPENDIX A FIGURES

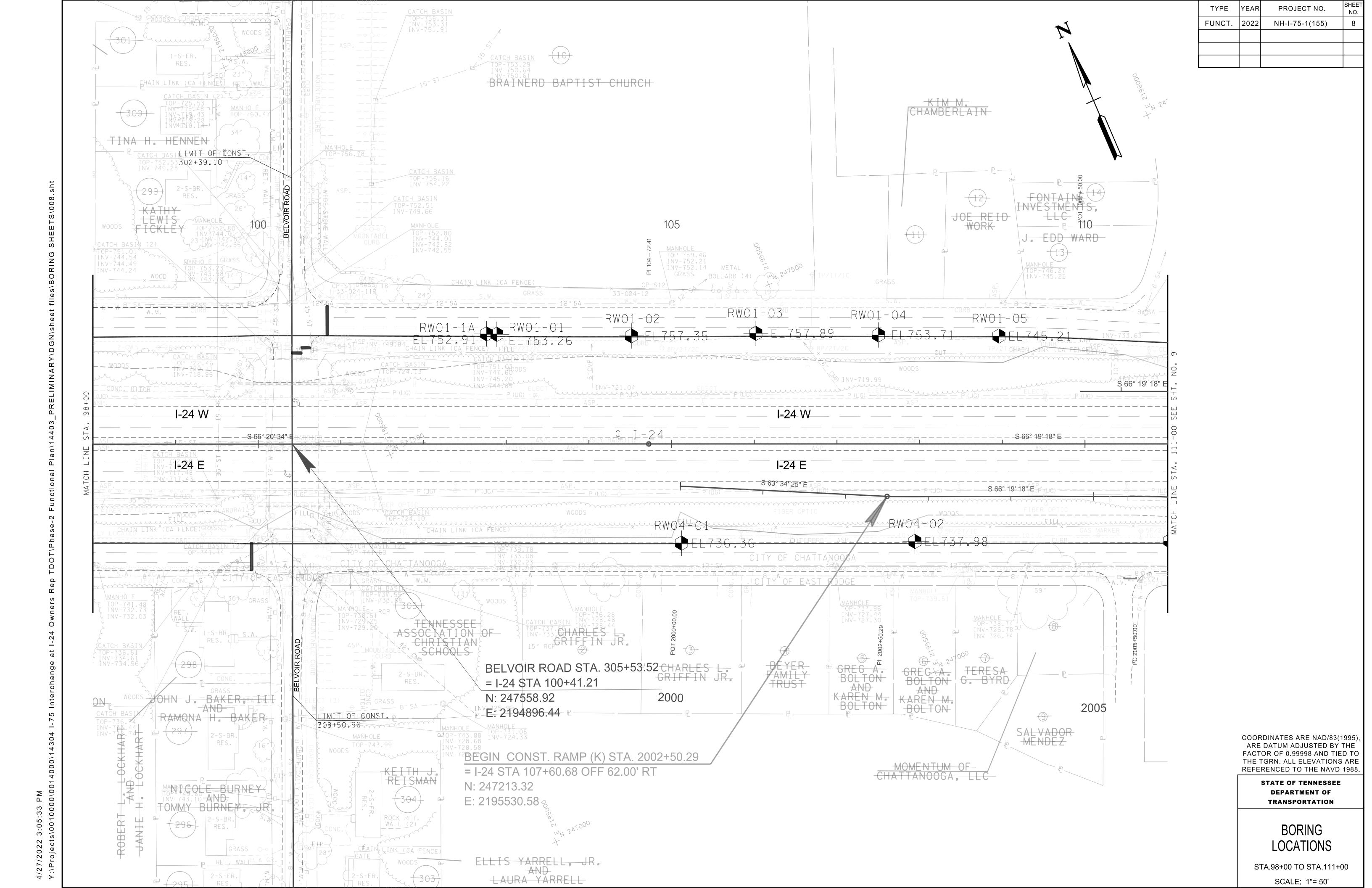


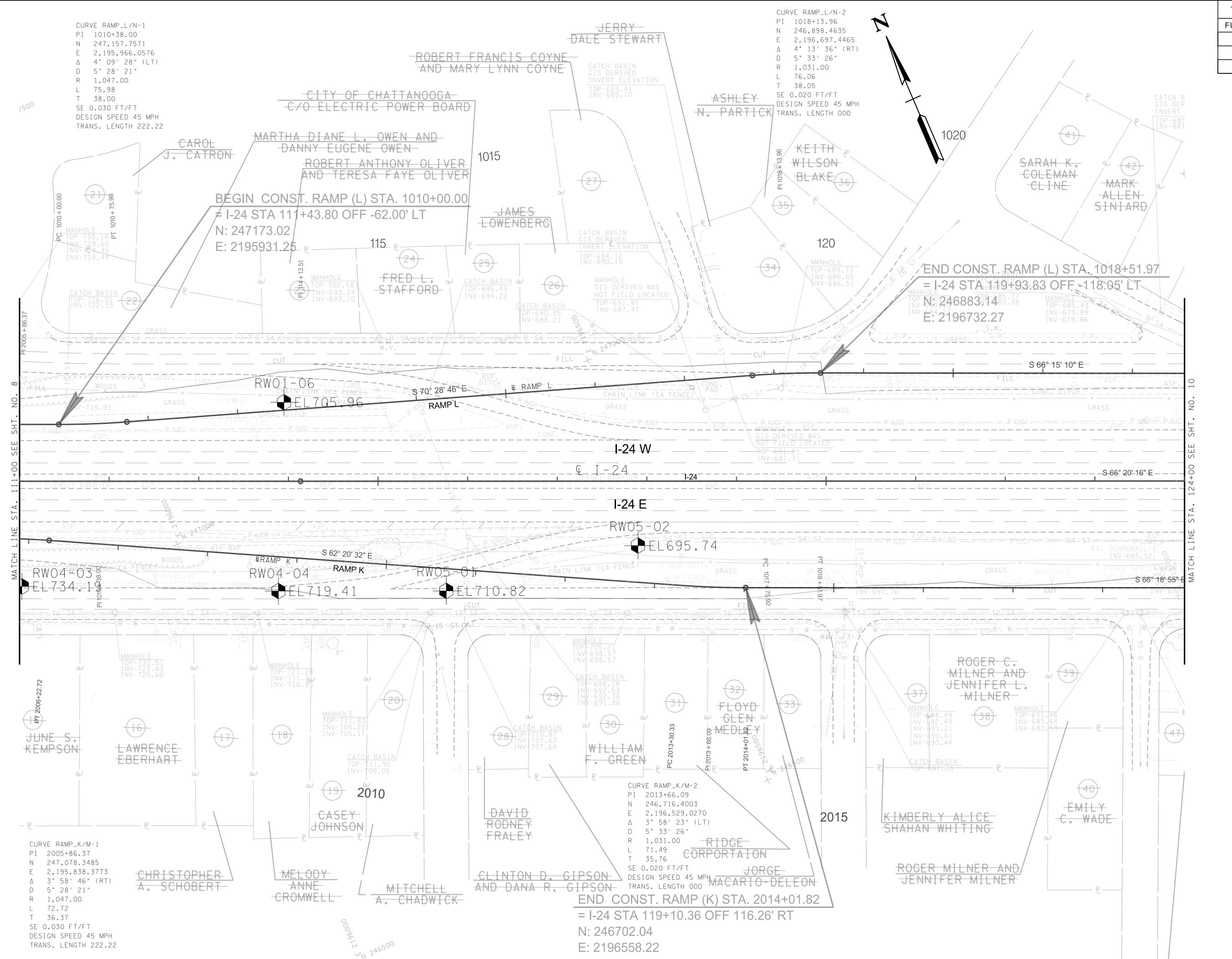
# Site Location Plan

I-75 Interchange Modification at I-24 (Phase 2)
PIN 114174.01
Chattanooga, Tennessee

Figure 1

# Figure 2 GeoEngineers/Neel-Schaffer Boring Location Sheets





SHEETS/009

PRELIMINARY\DGN\sheet files\BORING

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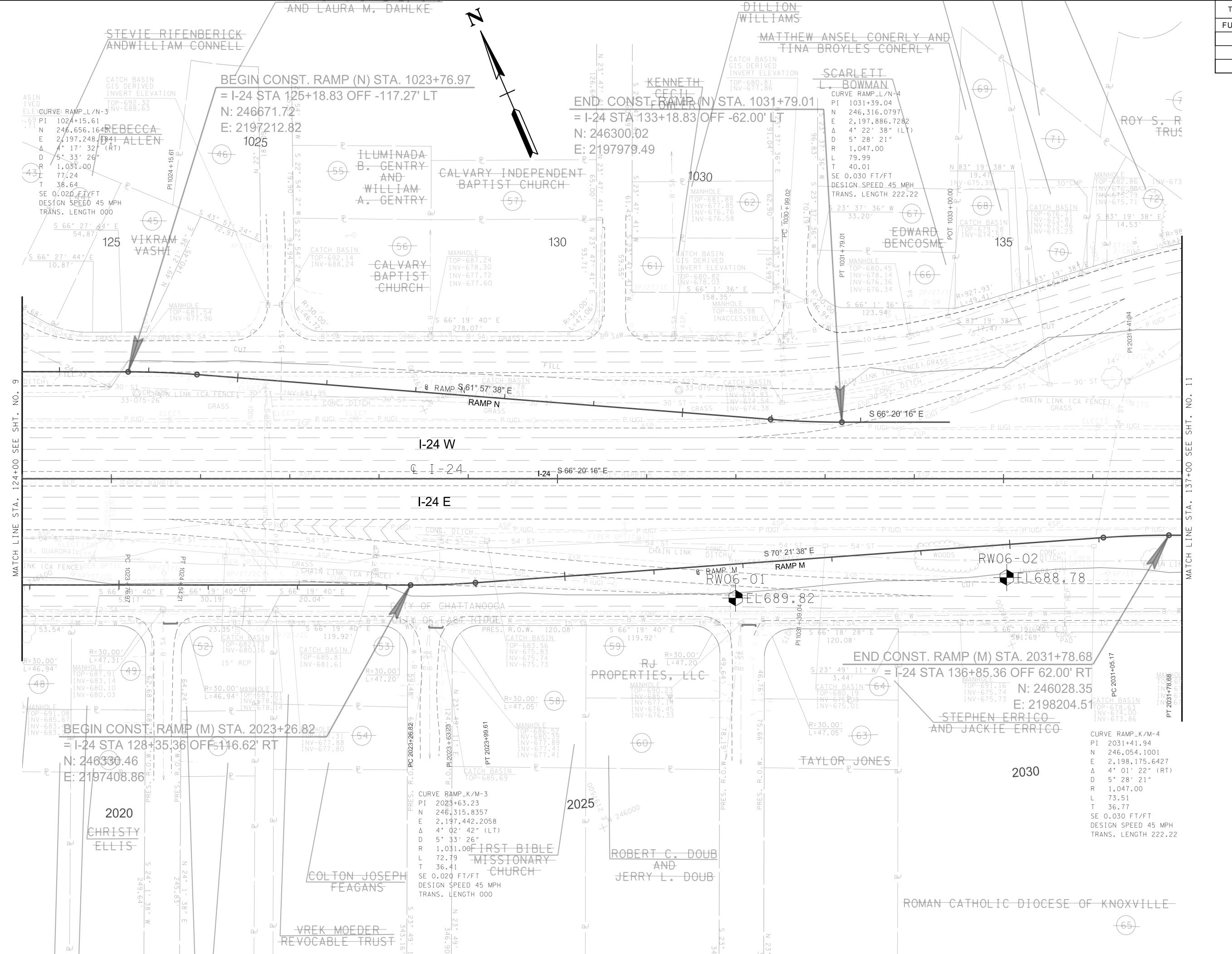
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COORDINATES ARE NAD/83(1995), ARE DATUM ADJUSTED BY THE FACTOR OF 0.99998 AND TIED TO THE TGRN. ALL ELEVATIONS ARE REFERENCED TO THE NAVD 1988.

STATE OF TENNESSEE
DEPARTMENT OF
TRANSPORTATION

BORING LOCATIONS

STA.111+00 TO STA.124+00 SCALE: 1"= 50'



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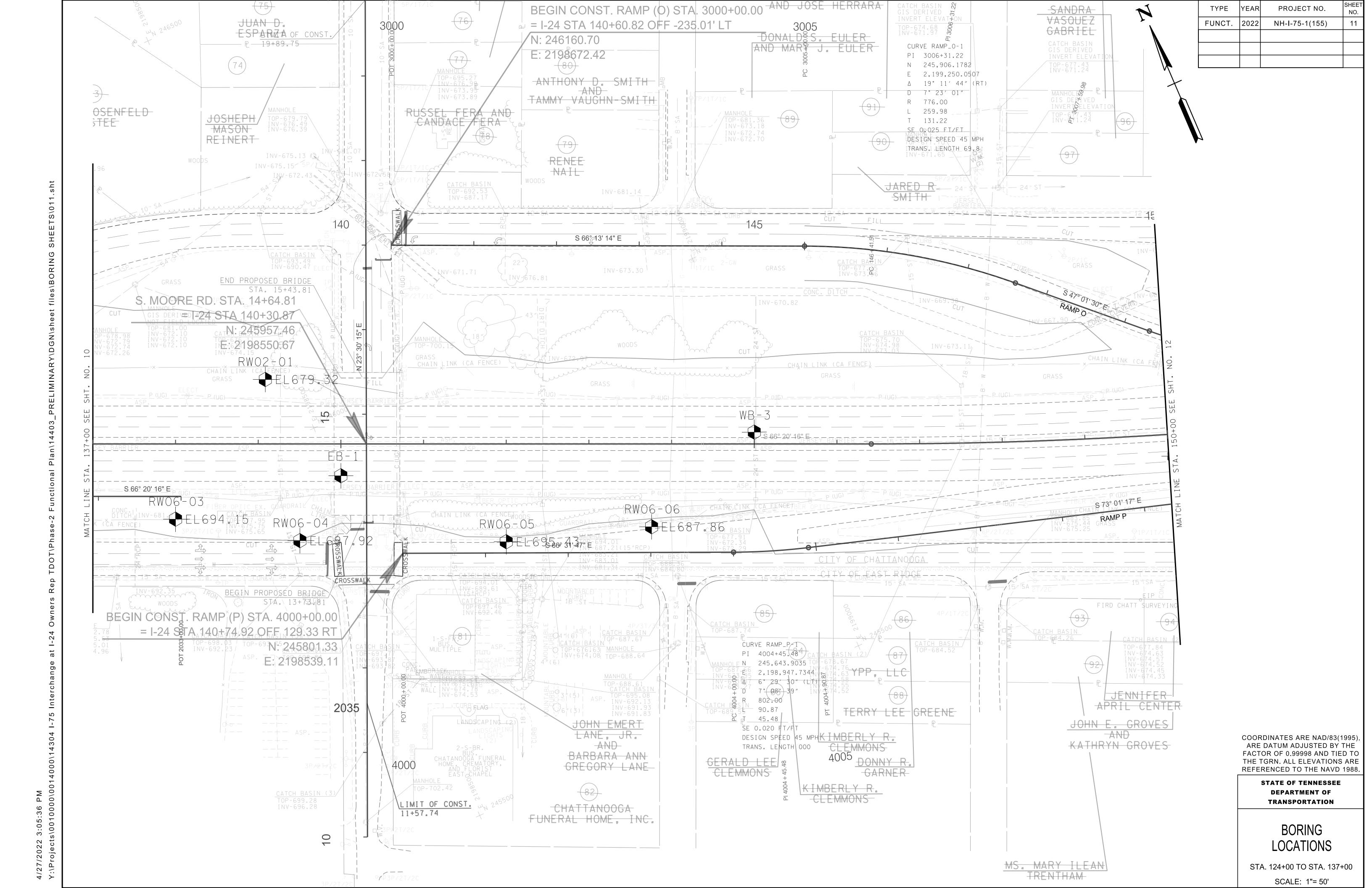
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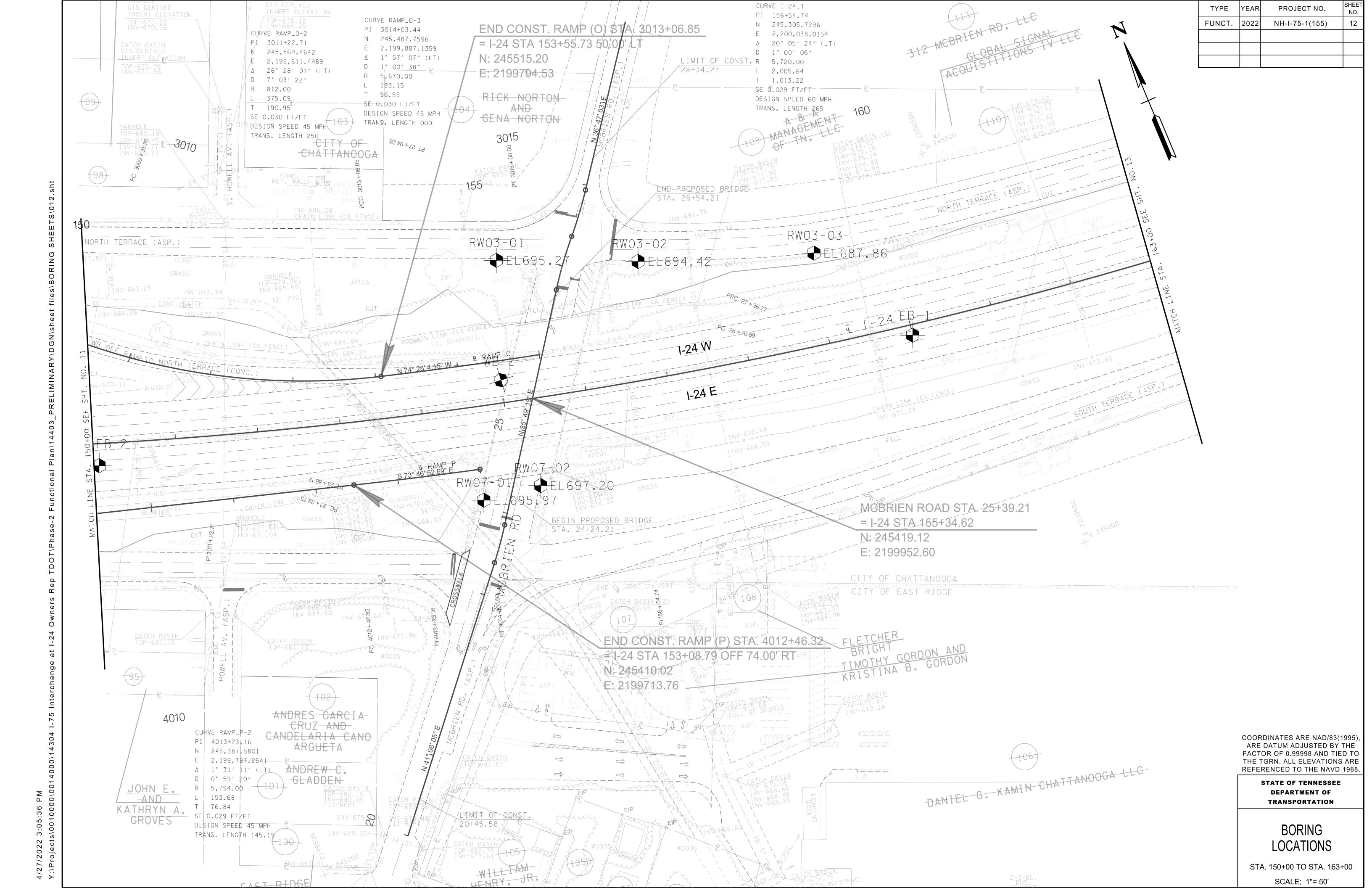
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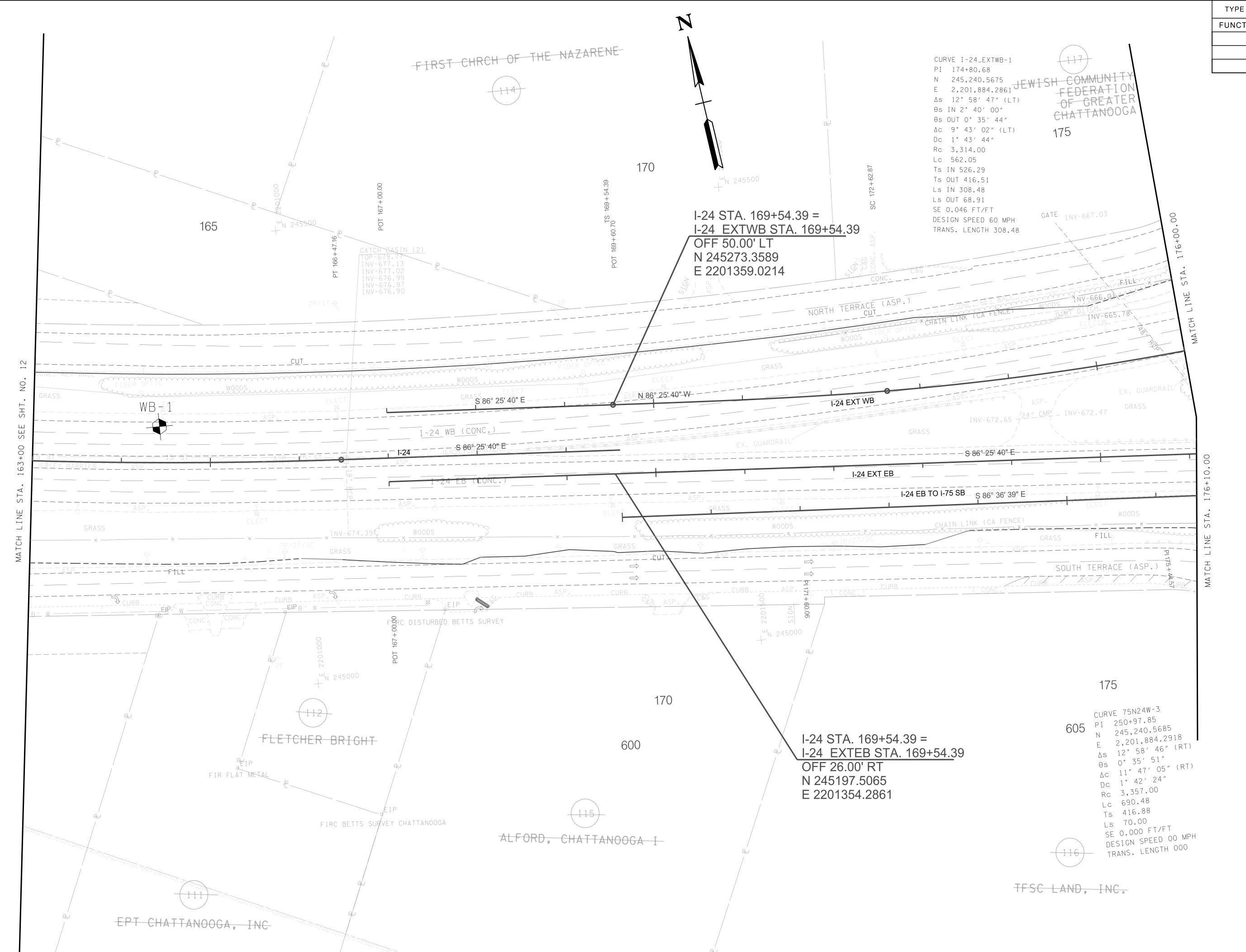
STATE OF TENNESSEE
DEPARTMENT OF
TRANSPORTATION

BORING LOCATIONS

STA.124+00 TO STA.137+00 SCALE: 1"= 50'







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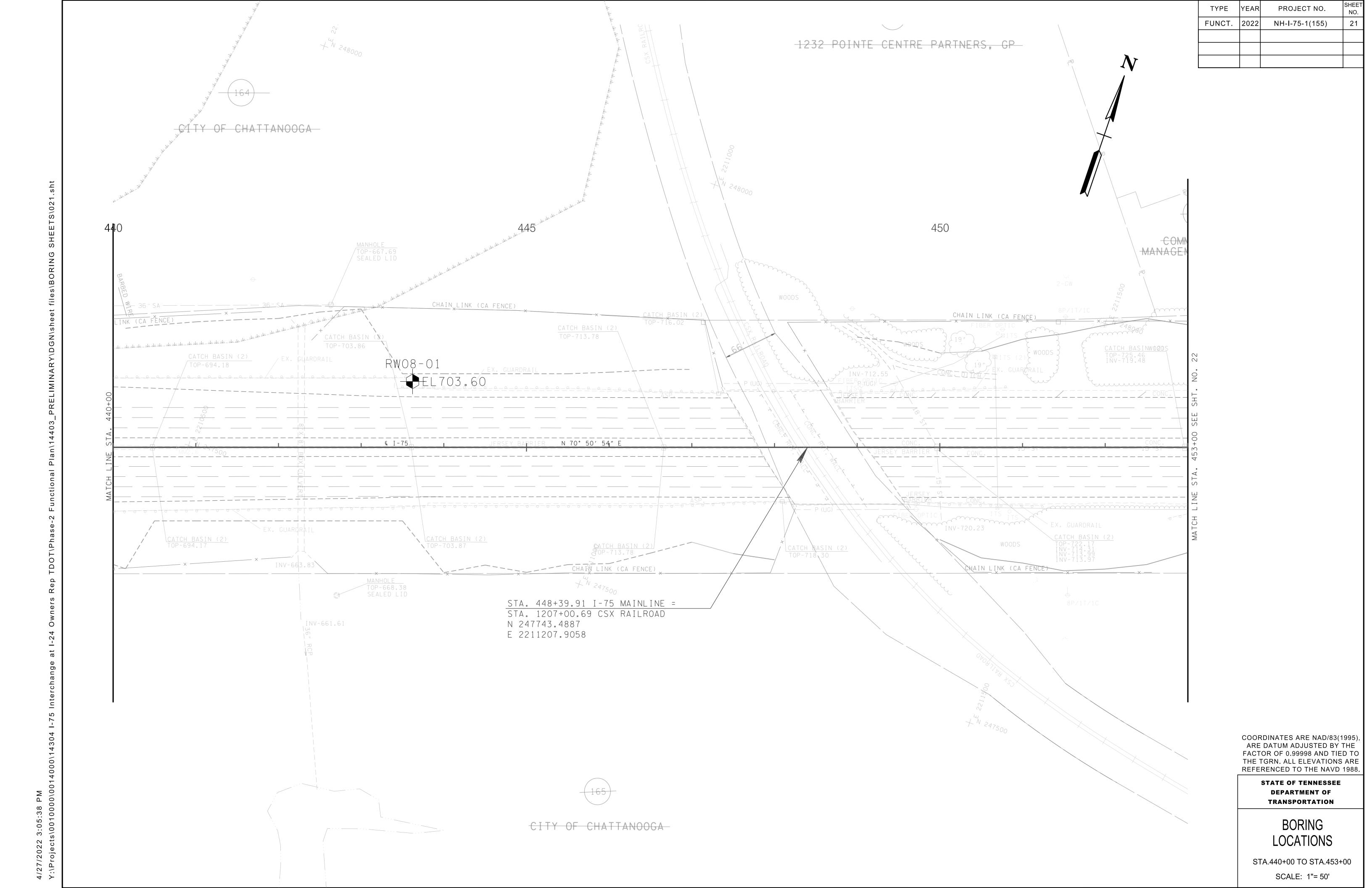
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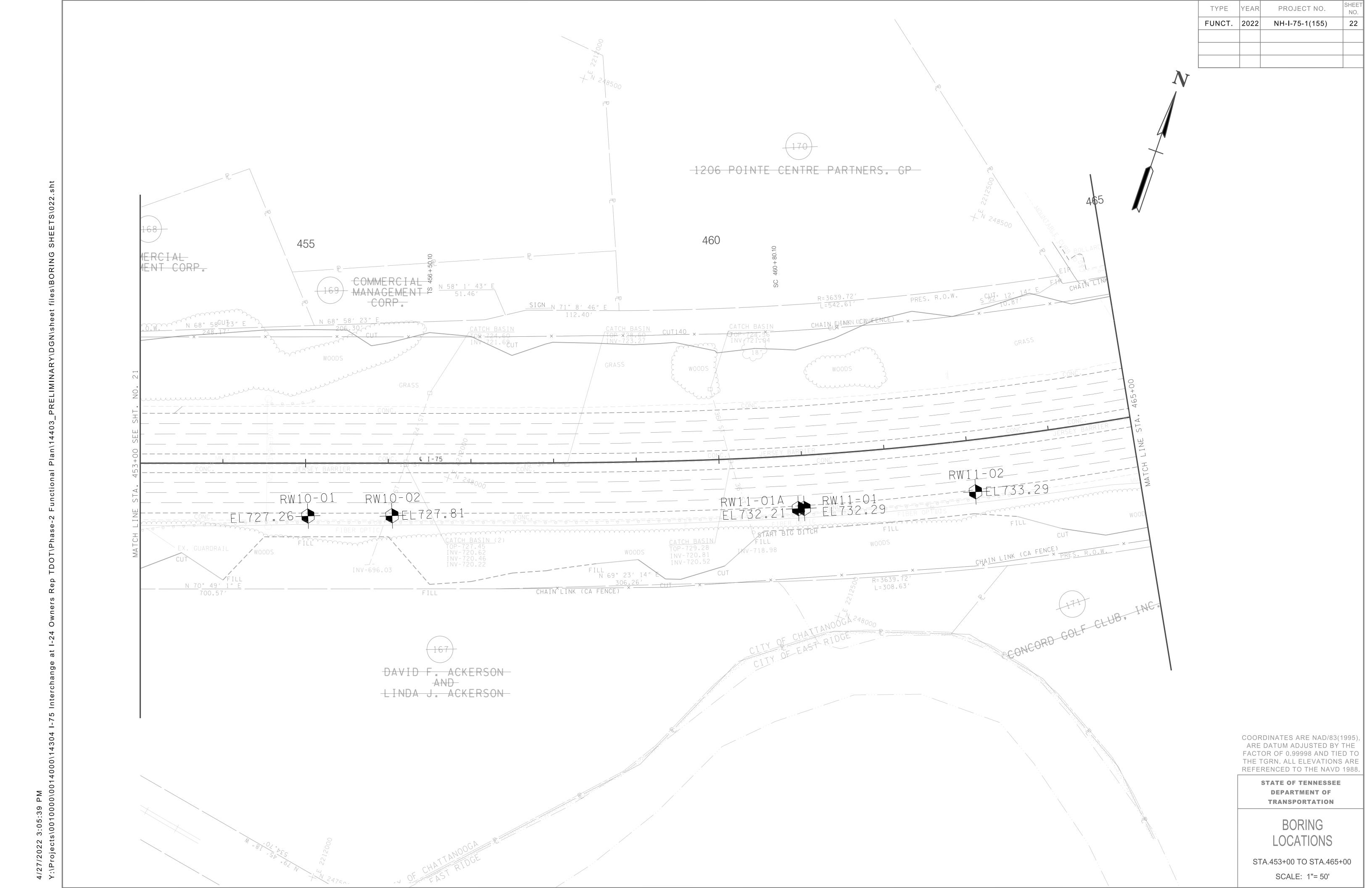
COORDINATES ARE NAD/83(1995), ARE DATUM ADJUSTED BY THE FACTOR OF 0.99998 AND TIED TO THE TGRN. ALL ELEVATIONS ARE REFERENCED TO THE NAVD 1988.

> STATE OF TENNESSEE DEPARTMENT OF TRANSPORTATION

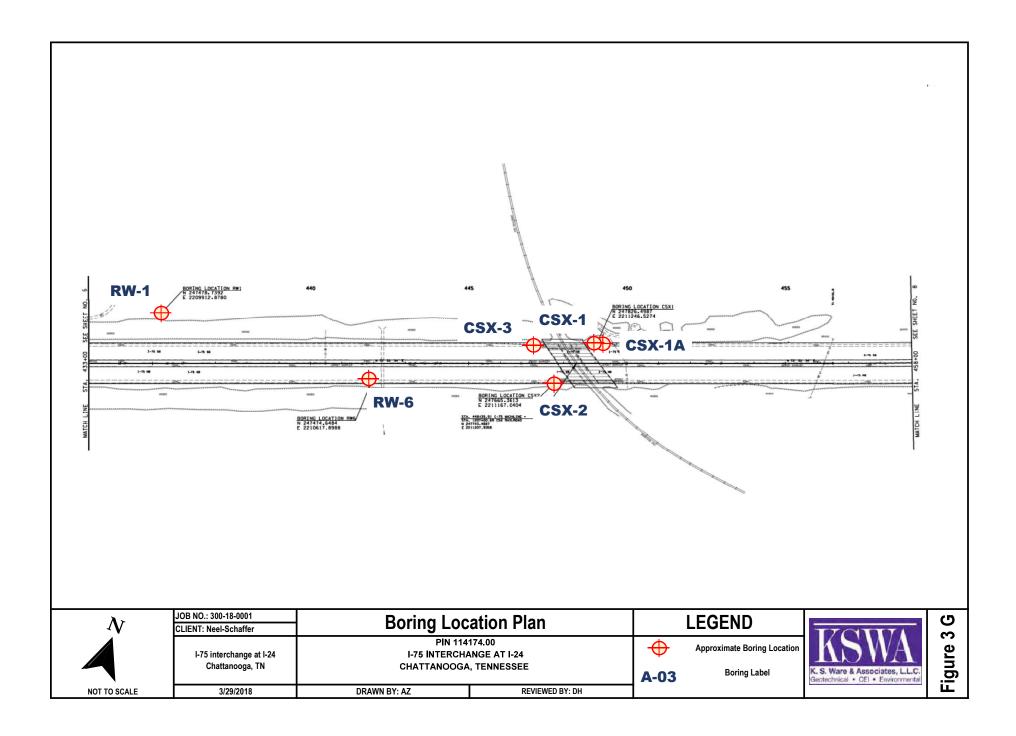
BORING LOCATIONS

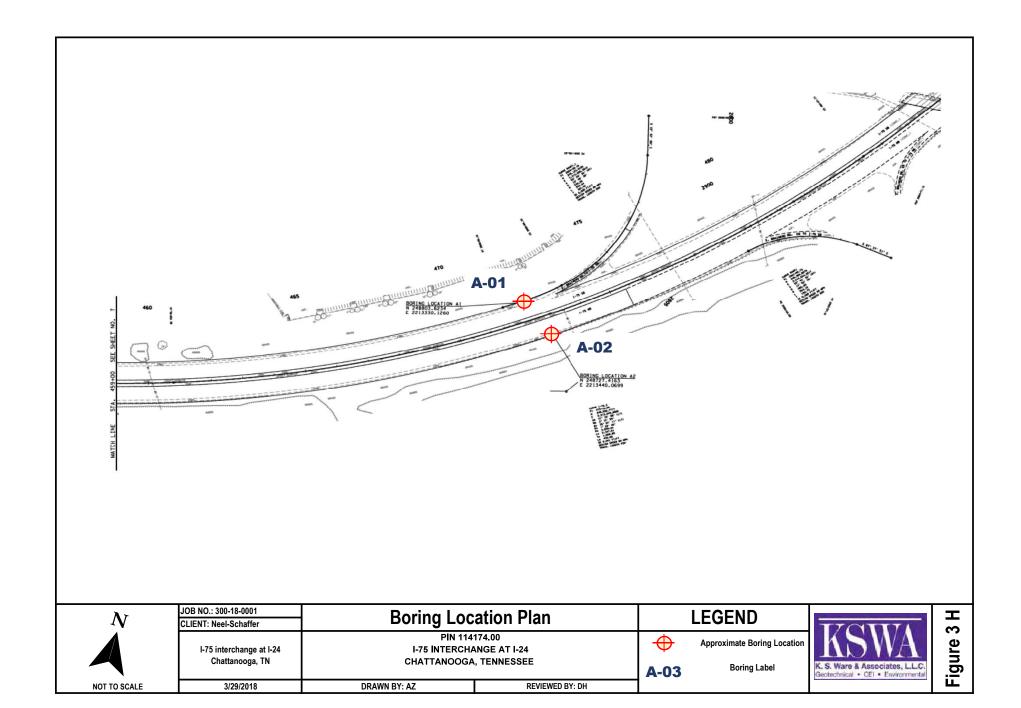
STA. 163+00 TO STA.176+00 SCALE: 1"= 50'

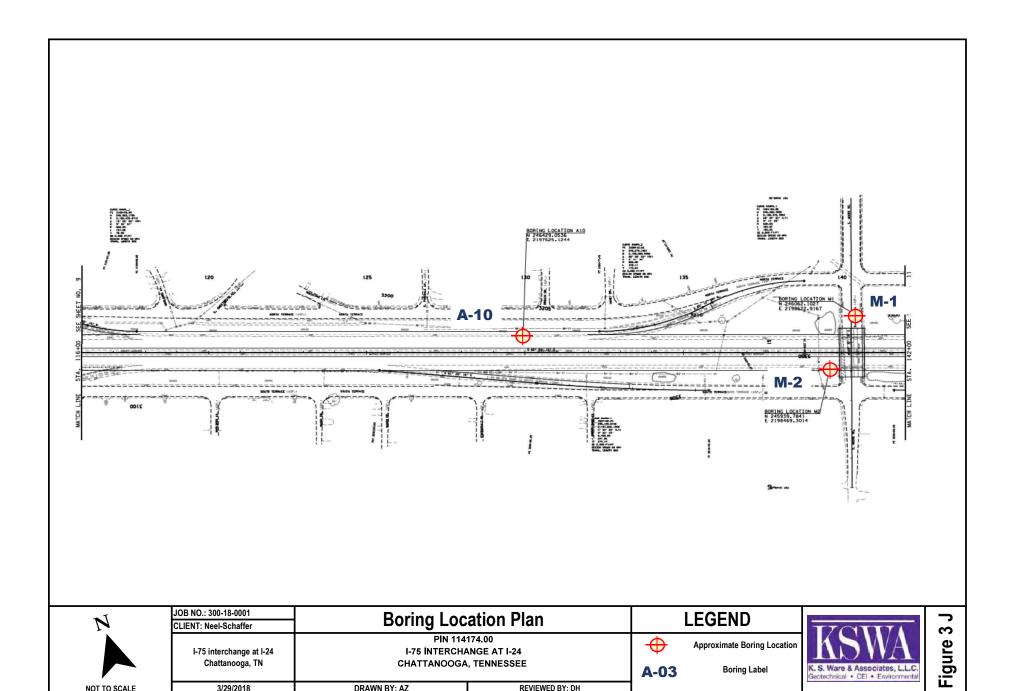




## Figure 3 K.S. Ware & Associates Boring Location Sheets





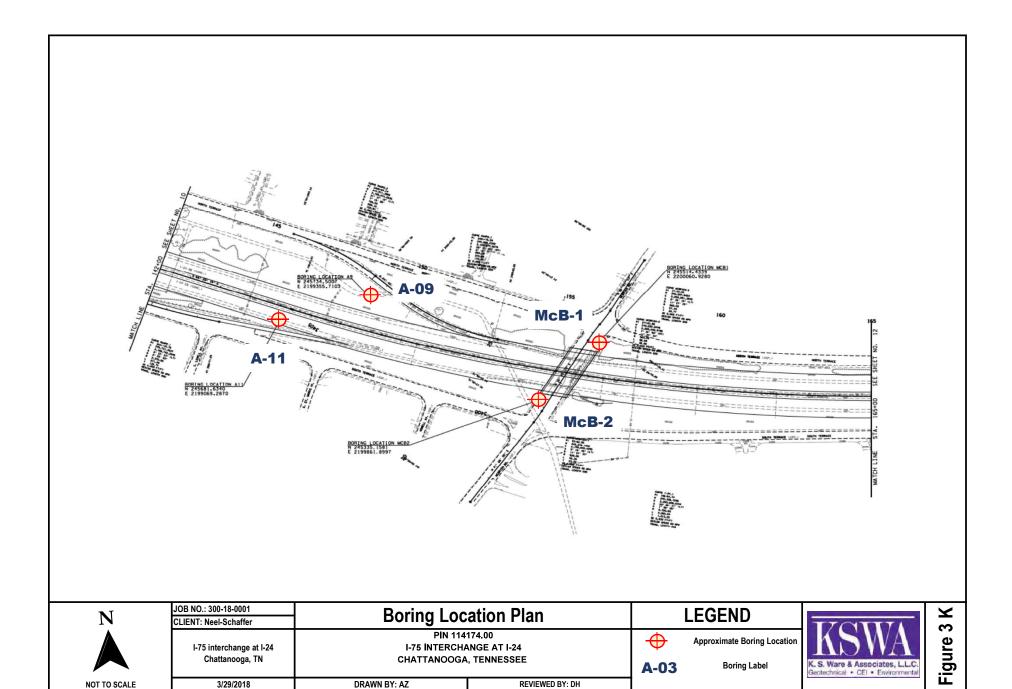


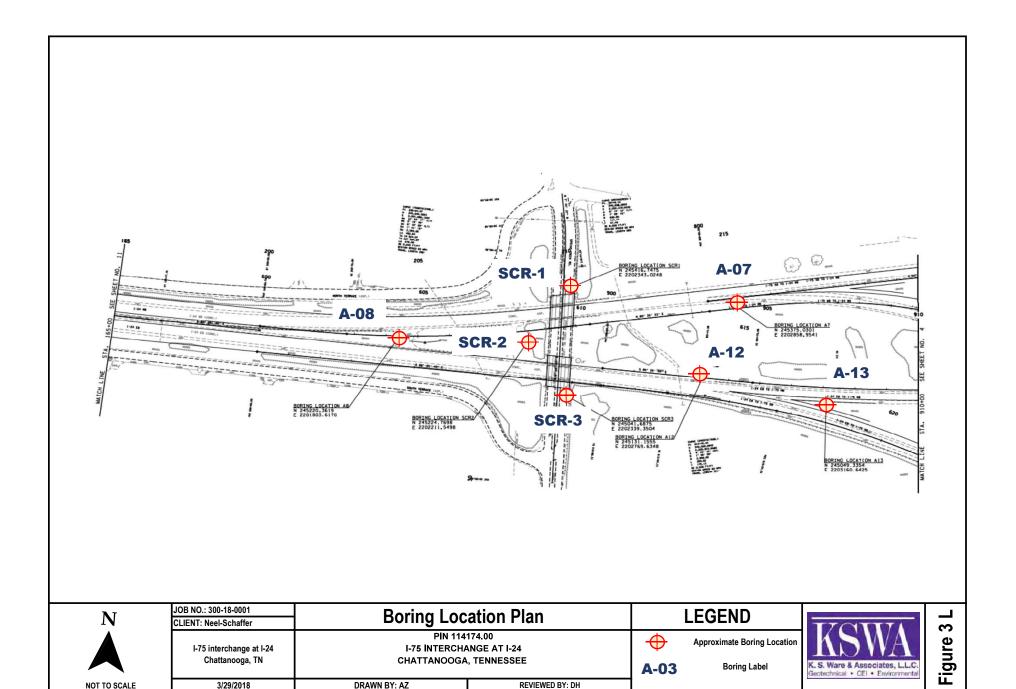
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3/29/2018

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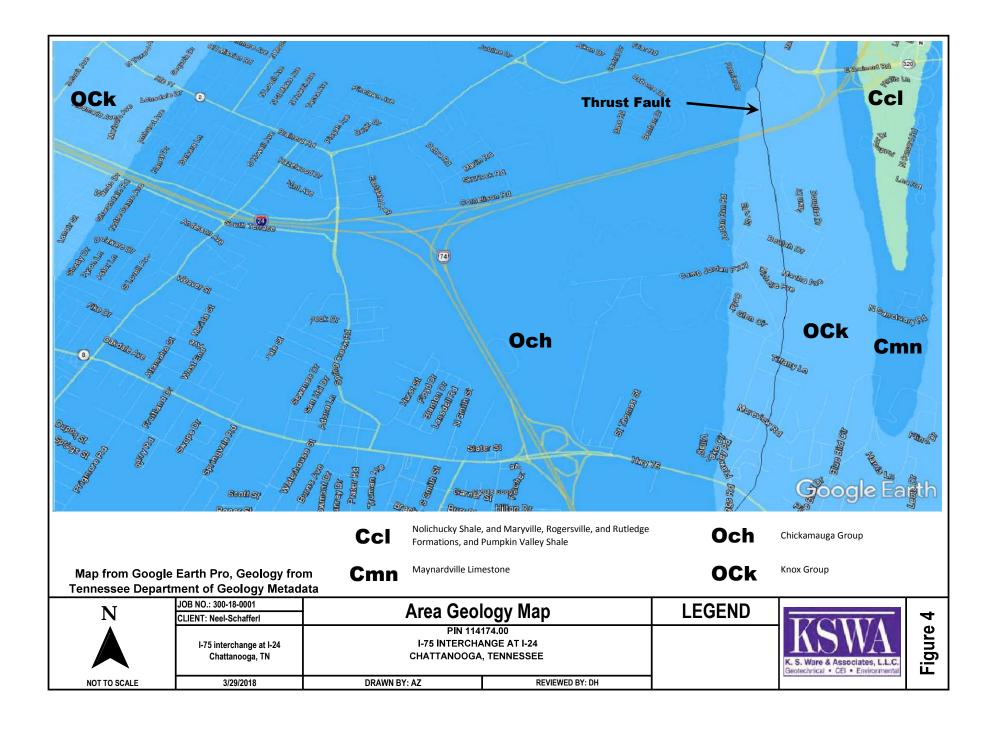


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3/29/2018

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### Figure 5 KSWA Bridge Subsurface Diagrams



CLIENT Neel-Schaffer

### SUBSURFACE DIAGRAM CSX RAILROAD BRIDGE FIGURE # 5G

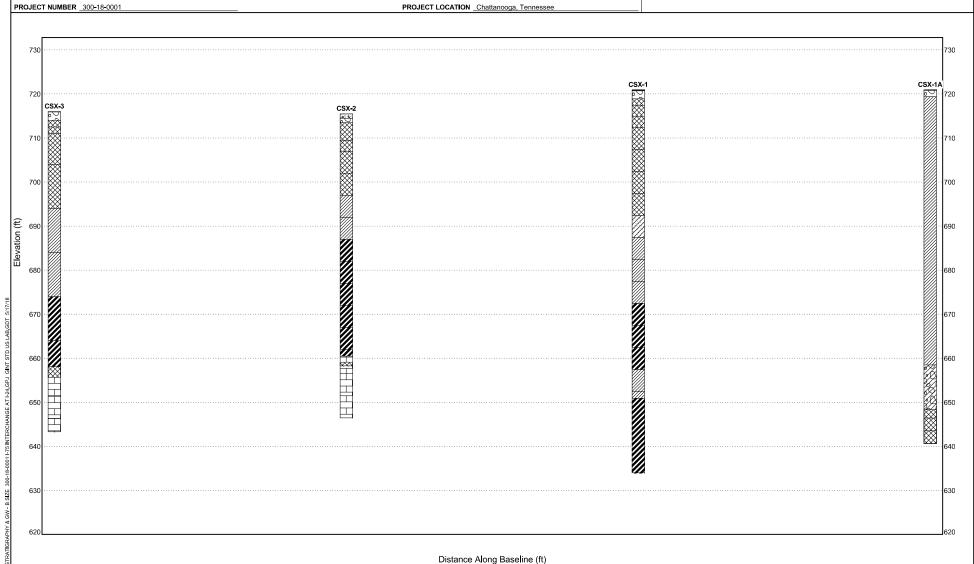
USCS Clayey Sand

USCS Poorly-graded Gravel USCS Low Plasticity Clay

Fill (made ground) USCS High Plasticity Clay Concrete

PROJECT NAME TDOT I-75 Interchange

PROJECT LOCATION Chattanooga, Tennessee





### SUBSURFACE DIAGRAM MOORE ROAD BRIDGE FIGURE # 5H

Asphalt USCS Poorly-graded Gravel
USCS Low Plasticity Clay Limestone

Fill (made ground)



Distance Along Baseline (ft)



### SUBSURFACE DIAGRAM MCBRIEN ROAD BRIDGE FIGURE # 51

Asphalt USCS Poorly-graded Gravel
USCS Low Plasticity Clay Limestone

Fill (made ground)

USCS High Plasticity Clay

CLIENT Neel-Schaffer PROJECT NAME TDOT I-75 Interchange PROJECT NUMBER 300-18-0001 PROJECT LOCATION Chattanooga, Tennessee 700 700 MCB-1 MCB-2 695 695 690 685 Elevation (ft) 680 670 665 665 660 655 655 650 240

Distance Along Baseline (ft)

# APPENDIX B KSWA Boring Logs GeoEngineers Boring Logs Geotechnics Lab Test Results GeoEngineers Subgrade Test Results



### **TEST BORING NO. A-01**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 1 of 1

		Geotechnical • CEI • Environmental	PROJECT NO	.: 30	00-18	-0001	l				Sheet	1 of	1
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): Location: N 248803.6234 E 221	3330.1260	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
	,,,	ASPHALT (4 inches)	0.3×							>			┝
c	°V°	BASESTONE (15.6 inches)											
	××××	_ A-1	1.6_										
	XXX	LEAN CLAY (CL), with chert, reddish I A-7-5	orown, stiff, (F <b>I</b> LL)										
- 🚽	XXX	A-1-3	3.5	IXI			5 <b>-</b> 5 <b>-</b> 6			18.1			
		LEAN CLAY (CL), with chert, very silty		$\langle \cdot \rangle$									
4 7	XXX	stiff, (FILL)	,	IXI			3-4-5			20.8	41	21	
}	XXX	A-7-5		$\vdash$									
	XXX		<u>6.0_</u>										
}	XXX	LEAN CLAY (CL), very silty, dark redd A-7-5	ish brown, (FILL)	$ \mathcal{N} $			3-4-5			22.0			
	XXX			$\angle \Delta$									
- 8 –	XXX		8.5										
_ 🕸		LEAN CLAY (CL), silty, dark reddish b	rown, (FILL)							00.7			
8	XX	A-7-5		$ \Lambda $			3-3-4			20.7			
	XX												
{	XX												
12-	XX												
- 8	XXX												
	XXX		13.5_										
· -{	XX	FAT CLAY (CH), very silty, dark reddis A-7-6	sh brown, (FILL)	$ \mathcal{N} $			3-3-5			27.0			
. 🕸	XXX		15.0	$\angle $									
40		BORING TERMINATED AT 15.0 FBG	S										
16-													
. 4													
7													
-20-													
- 4													
7													
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24-													
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-28-													
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		1											
			narks: <b>Groundwa</b> t	er w	as N	OT e	ncounte	red d	luring	g or a	fter		
Date S		d: 4/11/18 dri	lling activities.  Bo mpleted with a tru	ring ck-∾	was	back	tilled Wi rillria El	ith Cl	านเมอ	ys. Bo	oring	was	
Drilled		TSD / Richardson by	Neel-Schaffer.	∪N-11	Juli	.cu u	ı ıııı ıy. El	<del>c v</del> al(	7112 V	4616 F	JI UVI	u <del>c</del> u	
	ed By:	W.S. Anderson											



### **TEST BORING NO. A-02**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 1 of 1

	Geotechnical • CEI • Environmental	PROJECT NO	50	<i>7</i> 0-10	-000					Sheet	1 01	ı
Depth, feet Graphic Log	Approx. Surface El. (feet, MSL): 7 Location: N 248727.4136 E 221344	10.0699	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
(0)	BASESTONE (19.2 inches)	0.3⁄										
	LEAN CLAY (CL), silty, some chert, reddis	h brown, stiff,										
	(FILL) A-7-5	4.0	X			3-4-6			18.7			
- 4	LEAN CLAY (CL), silty, occaisional sandy, reddish brown, with gravel, (FILL) A-7-5		X			4-5-6			18.0			
	LEAN CLAY (CL), silty, sandy, with lots of zones, (FILL) A-7-5	6.0_ sandy chert	X			4-5-6			13.8			
8 -	LEAN CLAY (CL), very silty, reddish brown A-7-5	, (FILL)8.5	X			3-2-3			18.4			
-12-		13.5										
	LEAN CLAY (CL), silty, reddish brown, (FIL A-7-5	_L) 15.0	X			4-6-8			15.3			
-16-	BORING TERMINATED AT 15.0 FBGS											
-20-												
-24-												
- 28-												
Completi Date Sta Date Cor Drilled By Logged E	npleted: 4/10/18 completed: TSD / Richardson by Nee	s: Groundwat g activities. Bo eted with a trud el-Schaffer.	ring	was	back	filled wi	th cu	ıtting	js. Bo	ring	was ded	



### **TEST BORING NO. A-08**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 1 of 1

	Geotechnical • CEI • Environmental	PROJECT NO	st	JU-10	-000	! 				Sneet	1 01	
Depth, feet Graphic Log	Approx. Surface El. (feet, MSL): Location: N 245220.3619 E 22018	803.6170	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	Copal Aticitoria
	POORLY-GRADED SAND (SP) A-3a POORLY-GRADED SAND (SP), black, d (FILL) Possible Foundry Sand A-30a	·	X	93		16-22-25			3.7			
- 4 -	LEAN CLAY (CL), brown, stiff, moist A-7-5	3.5_	X	67		7-4-6			18.2			
	LEAN CLAY (CL), brown, stiff, moist A-7-5	6.0	X	13		7-6-4			15.2			
- 8 -	LEAN CLAY (CL) with traces of sand, bro A-7-5	<u>8.5</u> own, stiff, moist	X	87		4-5-6			17.9	48	20	:
- 12- - 12-		13.5_										
- 16-	FAT CLAY (CH), brown, stiff, moist A-7-6 Severely weathered Limestone AUGER REFUSAL AT 14.7 FBGS BORING TERMINATED AT 14.7 FBGS	14.1 14.7	X	100		11-15- 50/2			13.5			
-20-												
-28-												
Completion  Date Stare  Date Con  Drilled By  Logged B	npleted: 4/12/18 N93E : MW / Mike Borin	rks: Groundwat ng activities. Off . Ground surfac ng was backfille .Schaffer.	set l e at	nole ' hole	15' fr is at	om stake out 2.7'	alor	ng a Ì er tha	bearii an sta	ng of ake.		



### **TEST BORING NO. A-09**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 1 of 1

			CEI • Environmental	PROJE	CT NO	.: 30	00-18	3-0001				;	Sheet	1 of	1
Depth, feet	Graphic Log	Approx. Location	Surface El. (feet, No. 18 No.	E 2199356.2500		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		LEAN C	IL (12 inches) LAY (CL), reddish brow black mineral staing		<u>1.0</u>	X	67		3-5-8			19.0			
4 -		LEAN C fragmen	LAY (CL), brown mottle ts, black mineral stainir	d gray, stiff, rock	_3 <u>.</u> 5_	X	89		4 <b>-</b> 7 <b>-</b> 6			13.3			
_			REFUSAL AT 5.5 FBG TERMINATED AT 5.5		5.5										
8 –															
-															
12-															
-															
16- -															
_															
20 – –															
-															
24 <i>-</i> -															
_															
28-															
Date Date Drille	Starte	leted:	5.5 4/16/18 4/16/18 Geotech / Patrick A. Zeb	Remarks: Groudrilling activities completed with provided by No.	es. Bo h CME	ring -550	was , HS/	back	ncounte filled wit 4 inch I.	th cu	tting	s. Boı	ring v	was	



### **TEST BORING NO. A-10**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PRO IECT NO - 300-18-0001

	i i	K. S. Ware & Associates, L.L.C. Geotechnical • CEI • Environmental	PROJECT	NO.: 3	300-1	8-000	1				Sheet	1 of	1
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL) Location: N 246429.0536 E 2	197625.1244	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		ASPHALT (4.8 inches) BASESTONE (54 inches) A-1		).4,-						>			
4				1.9	50		3-10-7						
		FAT CLAY (CH), brown mottled gray fragments A-7-6	r, firm, dense, chert		100		3-4-4						
8 –		AUGER REFUSAL AT 9.4 FBGS	9	0.4	93		6-50/5-						
		BORING TERMINATED AT 9.4 FBG	ss										
- 16 —													
-20-													
-24													
-28-													
Comple Date S			emarks: <b>Ground</b> vrilling activities.	water v	was N	NOT e	ncounte	red c	luring ttings	g or a	ifter	was	
Date C Drilled Logged	Ву:	leted: 4/30/18 TSD / Richardson	ompleted with Di rovided by Neel-	iedricł	า D-50	), HS/	<b>A</b> 2-1/4 ir	nch I.	D. ĔĬ	evato	ns w	ere	



### **TEST BORING NO. A-11**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PRO IECT NO : 300-18-0001 Shoot 1 of 1

		K. S. Ware & Associates, L.L.C.  Geotechnical • CEI • Environmental	PROJECT N	O.: 30	00-18	-0001	l			;	Sheet	1 of	1
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): Location: N 245681.6340 E 219	99069.2870	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )
		ASPHALT (9.8 inches)  POORLY GRADED SAND (SP), gray dense, (FILL) A-2			67		22-8-6			4.4			
4 -		FAT CLAY (CH), Residual soil, brown firm to very stiff, mottled A-7-5	3.2 and gray, moist,		100		8-3-6			25.3	61	27	3
- - - 8 –					100		6-9-15			22.1			
		AUGER REFUSAL AT 9.3 FBGS BORING TERMINATED AT 9.3 FBGS	9.:	3	100		50/4			24.5			
- 12-													
-16-													
-20-													
- 24 -													
- 28-													
Date Date Drille	Starte	d: 4/15/18 dri bleted: 4/15/18 ba MW / Bill Woods tru	marks: Groundw Iling activities. E ckfilled with cutt ck-mounted drill	Boring ings. I	was Borin	mov ig wa	ed 4.9' o s compl	ffset eted	. Bor with	ing w a	as	ffer.	



### **TEST BORING NO. CSX-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001

Sheet 1 of 3

	Geotechnical • CEI • Environmental	FROJECTIVE				- 	st)	ω	_		1 01	
Depth, feet Granhic Lod	Approx. Surface El. (feet, MSL): Location: N 247841.8209 E 2211		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Nater Content (%)	Liquid Limit	Plastic Limit	
	MATERIAL DESCRIPTI	ON				0)	Ъс	Δ.	Watı			
00		0.2										
	A-1											
- 🔛	LEAN CLAY (CL), very silty, sandy, grav	2 <u>.0</u> /e <b>l</b> , light brown,										
💥	(FILL) A-2-7	3.5	X			10 <b>-</b> 8-5			11.3			
4 –	LEAN CLAY (CL), silty, sandy, reddish b	prown, (FILL)										
	A-2-7					3-3-4			23.7			
		6.0										
	LEAN CLAY (CL), very silty, brown to re											
· -	FILL) A-7-5					5 <b>-</b> 6-7			14.9			
8 – 💥												
	LEAN CLAY (CL), silty, reddish brown, (	<u></u>										
	A-7-5					10-12-13			19.4			
12-												
		40.5										
	LEAN CLAY (CL), silty, yellowish to redo	<u> 13.5</u> dish brown,										
	(FILL) A-7-5					9-10-13			25.7			
16-												
💥												
- 💥		10.5										
	LEAN CLAY, sandy with chert fragments	<u>18.</u> 5 s, si <b>l</b> ty, light										
🔉	reddish brown, (FILL) A-2-7					4 <b>-</b> 6-7			14.8			
20-												
		22.5										
24-	LEAN CLAY (CL), sandy, silty, light redo	23.5 dish brown to										
<sup></sup> 🛞	light brown, (FILL) A-2-7					14 <b>-</b> 16- 50/4			23.0			
-												
	$\otimes$											
-28-		20.5										
	SAND (SC), very clayey, light reddish br											
	A-2-7		X			15-19-14			14.5			
Complet	on Depth (ft.): <b>94.3</b> Rema	arks: <b>Groundwa</b>	iter w	as N	OT e	ncounte	red d	uring	g or a	fter		_
Date Sta	rted: 4/11/18 drilli	ng activities. Bo	oring	was	back	filled wit	h cut	tting	s. Boı	ring v		
Date Co Drilled B	TSD / Richardson prov	pleted with Died rided by Neel-So			, нъ	4 ∠-1/4 in	cn I.I	U. EK	evato	ns W	ere	
Logged I	sy: W.S. Anderson											



### **TEST BORING NO. CSX-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 2 of 3

vel and sand streaks,	33.5 38.5	Recovery (%)	RQD (%)	SPT Values 8-8-50/5	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit
vel and sand streaks,		7		8-8-50/5					
vel and sand streaks,				8-8-50/5			23.3		
vel and sand streaks,		7		8-8-50/5			23.3		
vel and sand streaks,		7		8-8-50/5			23.3		
vel and sand streaks,		7		8-8-50/5			23.3		
vel and sand streaks,				8-8-50/5			23.3		
	38.5			8-8-50/5			23.3		' I
	38.5	<u> </u>		0-0-30/3					
	38.5						20.0		
	38.5			<b>I</b>					
	38.5								
	38.5								
	38 <u>.</u> 5								
	38.5	1 1							
vel and sand streaks,	\ /	,							
	$\perp$			5-5-7			29.3		
				3-3-7			23.5		
		1							
	43.5	]							
ddish brown, chert				466			29.7		
				4-6-6			29.7		
	<u> </u>								
	48.5	,							
brown				222			36.0		
				2-3-3			30.9		
	53.5	,							
vet				2-2-4			36.4		
		]		227			""		
		1							
	<u>58.5</u>	,							
eauish drown, wet	$  \vee  $			4-4-6			30.7		
	/\								
Remarks: Ground	dwater w	vas N	OT e	ncounte	ed d	uring	or a	fter	
									was
completed with I	Diedrich	D-50,							
provided by Nee			, ⊓ა⊬	\ <del>_</del>	CII I.L	J. EK	evato	ns w	ere
_^	vet  Remarks: Groun drilling activities completed with	vet  53.5  eddish brown, wet  Remarks: Groundwater with drilling activities. Boring completed with Diedrich	brown  53.5  vet  Seddish brown, wet  Remarks: Groundwater was N  drilling activities. Boring was	brown  53.5  vet  Seddish brown, wet  Remarks: Groundwater was NOT end of the drilling activities. Boring was back	vet 2-3-3  2-3-3  2-3-3  2-3-3  2-4  2-2-4  Remarks: Groundwater was NOT encounter drilling activities. Boring was backfilled wit	brown 2-3-3  2-3-3  2-3-4  2-2-4  Remarks: Groundwater was NOT encountered d	brown  2-3-3  2-3-3  2-3-3  2-2-4  2-2-4  Remarks: Groundwater was NOT encountered during drilling activities. Boring was backfilled with cuttings	Prown  2-3-3  36.9  36.9  2-2-4  36.4  36.4  30.7  Remarks: Groundwater was NOT encountered during or a drilling activities. Boring was backfilled with cuttings. Boring was backfilled with cuttings. Boring was backfilled with cuttings.	Prown  2-3-3  36.9  36.9  2-2-4  36.4  30.7  Remarks: Groundwater was NOT encountered during or after drilling activities. Boring was backfilled with cuttings. Boring was backfilled with cuttings. Boring was backfilled with cuttings.



### **TEST BORING NO. CSX-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 3 of 3

	Geotechnical • CEI • Environmental	PROJECT NO	).: 30	00-18	3 <b>-</b> 000	1			;	Sheet	3 of
Depth, feet Graphic Log	Approx. Surface El. (feet, MSL): Location: N 247841.8209 E 2211	283.5481	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit
64-	LEAN CLAY (CL) with chert and gravel, A-2-7	63.5				13-9-13			29.7		
-68-	LEAN CLAY (CL), some gravel, silty, sa A-2-7  FAT CLAY (CH), wet, very soft with sea (Drilling tods advanced under their own A-7-6					1-1-1			48.4		
 - 76-   - 80-	NO RECOVERY		<b>X</b>			50/0.2"			28.6		
84-	NO RECOVERY					7-8-50/1			18.0		
 88 - 	AUGER REFUSAL AT 86.9 FBGS BEGAN CORING AT 86.9 FBGS NO RECOVERY, CORE BARREL LEAL CORING TERMINATED AT 94.3 FBGS	86.9 DING OFF									
_	NO RECOVERY, CORE BARREL LEAD CORING TERMINATED AT 94.3 FBGS  on Depth (ft.): 94.3 Remarked: 4/11/18 drilling completed: 4/12/18 Comproversity (comproversity comproversity comproversity comproversity comproversity comproversity comproversity comproversity comproversity comproversity control of the comproversity control of the comproversity control of the control o	orks: Groundwa ing activities. Bo pleted with Died vided by Neel-Sc	ring Irich	was D-50	back	filled wit	h cu	tting	s. Bo	ring v	was ere



**TEST BORING NO. CSX-1A** 

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

	C	Geotechnical •	Associates, L.L.C. CEI • Environmental	PROJECT	NO.: 30	00-18	3-0001	l			;	Sheet	1 of	3
Depth, feet	Graphic Log		Surface El. (feet, M : Offset 20 feet E	of CSX-1	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
			MATERIAL DES	CRIPTION					$\Box$		Wa			
	مکر	N ASPHAL	T (1 inch)		0.1/									Ī
	$\langle O \rangle$	BASEST	ONE (16.8 inches)											
Ł	(4,6	_ A-1	,		1.5									
4		AUGER	ONLY											
Ł		LEAN CL	AY (CL), some chert, si	Ity, reddish brown										
-		A-4a	, ,	•										
4 –														
k														
7														
7														
_														
E														
8														
E														
4														
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28-														
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k	<u>////</u>		00.2	5 , 6						  a.ace#		EL -		
		Depth (ft.):	がU.J 4/4つ/40	Remarks: Ground	lwater w	as N	OI e	ncounte	rea d	uring	or a	rter M		
	Starte		4/12/18 4/13/18	drilling activities.	Boring	was	pack	rilled wi	ın cu	tting	s. U l	IVI		
	Comp d By:		TSD / Richardson	coordinates were	taken f	rom	GIS.							
	u ÞV:		W.S. Anderson	1										



**TEST BORING NO. CSX-1A** 

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 2 of 3

Depth, feet	Graphic Log	Approx. Location	Surface El. (feet, Manne:  Offset 20 feet E			Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
ם			MATERIAL DES	CRIPTION			ď		S	_ g	۵	Nate			
						Ь									1
						$\mathbf{I}$									
						9									
-32-									<b></b>						
- 4															
-36-															
-40-															
						H									
-44-															
_															
- 4															
-															
-48-															
_															
- 1															
-52-															
_ 4															
-56-						1									
						7									
	<b>/////</b>														
-60-				I		1									
Comp	pletion	Depth (ft.):	80.3	Remarks: Grou	undwate	er w	as N	OT eı	ncounte	red d	uring	g or a	fter		
Date	Starte	d:	4/12/18	drilling activiti	es. Bori	ing	was	back	filled wit	h cu	ttings	s. UT	M		
	Comp	leted:	4/13/18 TSD / Richardson	coordinates w	ere take	n fi	om (	GIS.							
urille	ed By:		W.S. Anderson	i											



### **TEST BORING NO. CSX-1A**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 3 of 3

Approx. Surface EI. (feet, MSL): 720.9 Location: Offset 20 feet E of CSX-1  MATERIAL DESCRIPTION  62.4  CLAYEY GRAVEL (GC) Casing advanced with tri-cone roller bit through dense chert zone A-2-7  72.6	Plastic Limit
CLAYEY GRAVEL (GC) Casing advanced with tri-cone roller bit through dense chert zone A-2-7	
CLAYEY GRAVEL (GC) Casing advanced with tri-cone roller bit through dense chert zone A-2-7	
CLAYEY GRAVEL (GC) Casing advanced with tri-cone roller bit through dense chert zone A-2-7	
CLAYEY GRAVEL (GC) Casing advanced with tri-cone roller bit through dense chert zone A-2-7	
Casing advanced with tri-cone roller bit through dense chert zone A-2-7	
-64 - Chert zone A-2-7	
73.6	
-72-	
-72- <del> </del>	
1/-0//	
RUN 1	
Weathered rock from 72.6' - 74.5'	
74.5	
RUN 2 LIMESTONE, brecciated and quartzitic	
77.4_	
RUN 3 NO RECOVERY	
80.3	
CORING TERMINATED AT 80.3 FBGS	
CORE BARREL RUPTURED, LOST IN THE HOLE	
BORING ABONDONED	
-84-	
-88-	
Completion Depth (ft.): 80.3 Remarks: Groundwater was NOT encountered during or after	
Date Started: 4/12/18 drilling activities. Boring was backfilled with cuttings. UTM	
Date Completed: 4/13/18 coordinates were taken from GIS.	
Drilled By: TSD / Richardson Logged By: W.S. Anderson	



### **TEST BORING NO. CSX-2**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 1 of 3

Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): 715.5 Location: N 247665.3613 E 2211167.040	<b>04</b> 88	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		CONCRETE (1 foot)  BASESTONE (12 inches) A-1 LEAN CLAY (CL), sandy, brown, stiff, moist, (FIL A-2-7	1.0 2.0	8.	7	22-17-16			7.6			
- 4 -			6,0	7:	3	11-5-6			7.4			
- 8		LEAN CLAY (CL), sandy with gravel, brown, hard (FILL) A-2-7		10	0	12-22-24			18.8			
		CLAYEY SAND (SC), gravel, brown, very stiff, m (FILL) A-2-7	13.5	10	00	5-11-15			17.9			
16-		LEAN CLAY (CL), sandy, brown, very stiff, moist A-2-7	, (FILL)	10	00	7-10-15			27.0			
· 20-		LEAN CLAY (CL), with traces of fine sand, browr very moist A-7-5		10	00	4-3-3						
-24 -   - 28 -		LEAN CLAY (CL), very stiff, moist, mottled A-7-5		10	00	8-9-12			27.1			
		FAT CLAY (CH), stiff, moist, mottled A-7-5	28.5	8.	7	6-6-8			29.0			
Date Date Drille	pletion Starte Comp d By: ed By:	A-7-5  Depth (ft.): 69.0 d: 4/9/18 Deted: 4/10/18 MW / Mike  Remarks: G drilling acti backfilled v truck-mour	roundwater vities. Borin vith cuttings ited drillrig.	was g wa	NOT is mo	encounte ved to 10. /as compl	8' off eted	set. i with	g or a Borin a	g wa		



### **TEST BORING NO. CSX-2**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 2 of 3

	Geotechnical • CEI • Environmental	PROJECT NO	).: 30	00-18	-000	1			;	Sheet	2 of	3
Depth, feet Graphic Log	Approx. Surface El. (feet, MSL): Location: N 247665.3613 E 221		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
- 32-    - 36-	FAT CLAY (CH), with traces of gravel a very stiff, moist A-7-6	<u>33.5</u> and chert, brown,	X	100		7-7-9			36.8			
	FAT CLAY (CH), with traces of gravel a very stiff, moist A-7-6	<u>38.5</u> and chert, brown,		100		6-10-7			41.8			
	FAT CLAY (CH), with traces of gravel a very stiff, moist A-7-6	and chert, brown,	X	60		5-6-9			33.9			
	FAT CLAY (CH), with traces of gravel a very stiff, moist A-7-6	48.5 and chert, brown,	X			6-11-7			30.7			
-52-	FAT CLAY (CH), with traces of gravel avery stiff, moist A-7-6 AUGER REFUSAL AT 55 FBGS BEGAN CORING AT 55 FBGS RUN 1	53.5 and chert, brown, 55.0 55.2		100		9 <b>-</b> 50/5-			15.9			
60 Completion Date Starte	Stained core (55.2') Zone of angled fractures from 56.5' - 5  RUN 2 LIMESTONE, very hard, quartzitic, grant Depth (ft.): 69.0 Red: 4/9/18  Red dril	y with calcite parks: <b>Groundwa</b> <b>ling activities. Bo</b>	ring	was	move	ed to 10.	8' off	set l	Borin		s	
	ed: 4/9/18 dril bleted: 4/10/18 bac MW / Mike true		ring ngs.	was Borin	move ng wa	ed to 10. s compl	8' off eted	set I with	Borin a	g wa		



### **TEST BORING NO. CSX-2**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

	(	K. S. Ware & Associates, L.L.C. Geotechnical • CEI • Environmental	PROJECT N	10.: 3	00-18	-0001	l				Sheet	3 of	3
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): Location: N 247665.3613 E 221	1167.0404	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
-		MATERIAL DESCRIPT healed fractures	ION							>			
					100	100							
L													
	$\Box$		64.										
-64	Ħ	RUN 3		<u> </u>									
- ‡	T	Non-jointed below 64 FBGS											
- ‡													
[					90	90							
-68	$\pm$												
	$\pm$	l Core loss left in hole	69.	0									
		CORING TERMINATED AT 69.0 FBGS											
-72-													
_													
_													
-76-													
- 4													
_													
-80-													
80													
- 1													
-84													
_													
-													
-88-													
- 4													
													L
Comp			arks: <b>Groundw</b> i <mark>ng activities. E</mark>									e	
Date (	Comp	bleted: 4/10/18 bac	kfilled with cut	tings.	Borir	ng wa	s compl	eted	with	а			
Drilloc	d By:	MW / Mike true	k-mounted dril	lria G	Elovoi				d by	Nool	Saha	ffor	



### **TEST BORING NO. CSX-3**

PROJECT NAME: TDOT I-75 Interchange LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001

Sheet 1 of 3

	Geotechnical • CEI • Environmental	PROJECT NO	5	JU-10	-000					Sheet	1 01	_
Depth, feet Graphic Log	MATERIAL DESCRIPTI		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
	ASPHALT (1.2 inches)  BASESTONE (22.8 inches)	0.1/										
000		2.0										
	LEAN CLAY (CL), with traces of gravel in brown to reddish brown, (FILL)	basestone, silty,	X	50		5-3-4			15.9			
- 4 –	A-7-5  LEAN CLAY (CL), with traces of basesto	one, slightly silty,		33		2.2.2			16.0			
- 💥	reddish brown, (FILL) A-7-5 A-7-5 A-7-5	5.0_	$\triangle$	33		2-2-2			10.0			
💥	LEAN CLAY (CL), silty to very silty, san- chert gravels, yellowish to reddish browi (FILL)	n, very soft,										
💥	A-2-7		X	80		1-2-2			21.5			
8 - 8												
💥			X	100		2-2-2			22.5			
💥												
💥		12,0										
12	LEAN CLAY (CL), silty to very silty, sand yellowish to reddish brown, firm to stiff,	dy to very sandy,										
	Å-2-7	,										
. 💥			$\triangle$	100		2-3-3			19.9			
-16-												
- 💥												
💥												
💥				100		5 <b>-</b> 7 <b>-</b> 6			22.8			
20-												
💥		20.0										
	LEAN CLAY (CL), silty to very silty, sand		-									
	A-2-7											
24-///			X	100		6-9-10			16.8			
-28-												
				100		9-9-12			26.9			
		. 0. 1								C4 -		
Date Star	ted: 4/18/18 drilli	arks: Groundwating activities. Bo	ring	was	back	filled wit	h cu				n	
Date Con Drilled By	: TSD / Richardson	UTM coordinates	s we	re tal	ken fi	rom GIS.	•					
Logged B	y: W.S. Anderson											_



### **TEST BORING NO. CSX-3**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 2 of 3

	Geotechnical • CEI • Environmental	PROJECT NO	).: 30	00-18	-000°	1			;	Sheet	2 of	
Depth, feet Graphic Log	Approx. Surface El. (feet, MSL): Location: 25 paces of W-SW of CSX bridge  MATERIAL DESCRIPT		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
- 32	LEAN CLAY (CL), silty to very silty, red brown, mottled A-7-5	32 <u>.</u> 0 Idish to yellowish		100		7-11-13			25.3			
-40				100		4-6-9			27.8			
	FAT CAY (CH), slightly silty, reddish to with black and white mottling A-7-6	yellowish brown,		100		6-7-9			36.5			
-48-		52.0	X	100		9-8-11			28.7			
-52   -56	FAT CLAY (CH), slightly silty, light brown mottled A-7-6			100		5-5-6			28.7			
- 60	AUGER REFUSAL AT 57.9 FBGS BEGAN CORING AT 57.9 FBGS RUN 1, Run 2 Weatherd Dolomite, stained core, mud		tor	50	0		rod d		2000	ftar		
Completion Date Starte Date Comp Drilled By: Logged By	ed: 4/18/18 dril bleted: 4/25/18 TSD / Richardson	arks: Groundwa ling activities. Bo I UTM coordinate	ring	was	back	filled wit	h cu				on	



### **TEST BORING NO. CSX-3**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PROJECT NO.: 300-18-0001 Sheet 3 of 3

		Geotechnical • CEI • Environmental	PROJECT NO	.: 30	00-18	3 <b>-</b> 0001	1				Sheet	3 of	•
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): 7 Location: 25 paces of W-SW of W CSX bridge  MATERIAL DESCRIPTIO	<i>l</i> corner of	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		N60.3'	60.3 60.3 gle fractures										
					100	100							
-64		RUN 4 BRECCIA, Dolomite, silicious, quartzitic w	64.7_										
 - 		healed fractures			100	100							
68-													
		Open, stained bedding plane (69.7') RUN 5 BRECCIA, Dolomite	69.7 69.7/		100	100							
72-		CORING TERMINATED AT 72.7 FBGS	72.7		100	100							
		CORING TERMINATED AT 72.7 FBGS											
76-													
· -													
80-													
· _													
84-													
. ]													
-88													
Date:	Starte Comp d By:	oleted: 4/25/18 TSD / Richardson and U	s: Groundwat g activities. Bo TM coordinates	ring	was	back	filled wi	th cu	  uring  tting	g or a	l lfter evatio	on .	



### **TEST BORING NO. M-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

	K. S. Ware & A Geotechnical • C	ssociates, L.L.C. CEI • Environmental	PROJECT	NO.: 30	00-18	-0001	I			;	Sheet	1 of	2
Depth, feet Graphic Log	Approx. S Location:	Surface El. (feet, MS N 246062.1027 E	2198622.9167	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
	ASPHALT	(9.6 inches)		2.0						>			
-0Q(		ONE (31.2 inches)		<u> 8.C</u>									
10 (V)	°	(3 3 3 3 7 )											
	<u> </u>												
- O			;	3.4									
4 –	LEAN CLA A-7-5	AY (CL), brown, dry, mo	pist and firm, (FILL)	-   X	72		2-3-6			20.4			
	A-7-5												
	×												
					72		3-3-3				50	23	
	$\otimes$				' -		0-0-0				50	20	
	8												
8 – 💥	$\hat{\otimes}$				1								
-	×			IX.	100		3-4-6			22.3			
	8												
	$\otimes$												
	<b>X</b>												
12			1	2 <u>.</u> 0									
	LEAN CLA A-7-5	AY (CL), Residual Soil,	brown, stiff to very stiff										
	A-7-3												
-////					100		6-7-9			28.1			
					100		0-7-9			20.1			
16-///													
					,								
-\///					100		3-5-7			16.8			
20-///							00.						
-\///													
<i>\\\\\</i>													
24-////				$  \times  $	94		7-10-11						
-¥///													
-\///													
28-////													
					400		7.0.50//						
<i>\\\\\</i>					100		7 <b>-</b> 8 <b>-</b> 50/4						
	<u></u>				<u> </u>								L
	on Depth (ft.): 3	89.9 1/20/18	Remarks: <b>Ground</b>	water w	as N	OT e	ncounte	red d	luring	g or a	tter		
Date Start Date Com		1/20/18 1/20/18	drilling activities. backfilled with cu	boring   boring	was Rorir	M W2	eu (O 9.6) Is compl	OTTS eted	et. B with	oring a	was		
rilled By:	· • • • • • • • • • • • • • • • • • • •	/IW / Bill Woods	truck-mounted dr	illria. E	levate	าษ wa ons w	vere prov	vided	l bv l	ع Neel-S	Scha	ffer.	
ogged B	v· E	Buehler											



### **TEST BORING NO. M-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

		K. S. Ware & Geotechnical	Associates, L.L.C. CEI • Environmental	PROJECT N	IO.: 3	800-18	3 <b>-</b> 000	1				Sheet	2 of	i
Depth, feet	Graphic Log	Approx. Location	Surface El. (feet, MSL) n: N 246062.1027 E 21		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
	,,,,,		MATERIAL DESCRIP						<u> </u>	_	⊗			1
	Щ		REFUSAL AT 30.1 FBGS CORING AT 30.1 FBGS	30.	1/ 📘 🗍									
		RUN 1			<b>'  </b>									
32-		LIMEST brown, h	ONE, argillaceous, pink and nard (Holstan Formation)	dark red to gray and		100								
-			,			100	88							
_		Open be	edding plane (33.6')	33.	o									
				34.	8									
_		∏ High and RUN 2	gle vertical fracture (34.8')	34.	9/									
36-		I KUNZ												
		]				100	92							
		]												
-				00										
40-		CORING	G TERMINATED AT 39.9 FB	39. 3S	9									
_														
-														
-44-														
-														
-														
48-														
-														
-52-														
_														
-														
-56-														
50														
_														
-														
_														
60														
60 Com <sub>l</sub>	pletior	n Depth (ft.):		marks: <b>Groundw</b>										
Date	Starte	ed:	4/20/18 dr	illing activities. E	Boring	y was	mov	ed to 9.6	offs	et. B	oring		;	
	Comp d By:	oleted:		ickfilled with cuti uck-mounted dril	ıngs. Iria F	Porii	ng Wa one v	is compl vere pro	videc	with I by N	a Jeel-	Scha	ffer	
	ed By		Buehler	ack-indunted alli	ıııy. E	.ıcval	UIIS V	vere hio	videc	ı Dy I	4CCI-4	Juid		



## **TEST BORING NO. M-2**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

	C	K. S. Ware & Associates, L.L.C. Geotechnical • CEI • Environmental	<b>PROJECT NO.: 300-18-0001</b> Sheet									1 of 2		
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): Location: N 245939.7841 E 2198  MATERIAL DESCRIPTI		Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit		
		ASPHALT (12 inches)	1.0											
· _		BASESTONE (7.2 inches) A-1 LEAN CLAY (CL), with traces of sand, b	1 <u>.0</u> 1.6 / prown and gray,	X	89		9 <b>-</b> 4-7			16.1				
4 -		A-7-5		X	89		3-3-5			24.3	56	24		
			8,1	X			4-2-4			37.5				
- 8 -		AUGER REFUSAL AT 8.1 FBGS BEGAN CORING AT 8.1 FBGS RUN 1 LIMESTONE, dark red and gray with second calcareous shale			100	96								
- 16		RUN 2  Zone of weatherd, fractured Limestone	13 <u>.</u> 1 14' - 15.2' 15.2		100	52								
		Zone of high angled fractures 17.5' - 18. RUN 3	5' <u>18.1</u> 18.5											
- 20 -		Zone of weatherd, fractured Limestone 2	21.5		100	56								
 -24- 		RUN 4	<u>23.</u> 1_		100	100								
			27.1_											
-28- 			29.3_		100	100								
Date Date Drille	pletion Starte Comp d By: ed By:	oleted: 4/16/18 back MW / Bill Woods truc	arks: Groundwa ng activities. Bo dfilled with cuttir k-mounted drillri	ring igs.	was Borir	move ng wa	ed to 7.6 s comp	' offs leted	et. B with	oring a	was			



## **TEST BORING NO. M-2**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PRO IECT NO : 300-18-0001

Shoot 2 of 2

		Geotechnical •	Associates, L.L.C. CEI • Environmental	PROJECT I	<b>PROJECT NO.: 300-18-0001</b> Sheet 2 of									2
Depth, feet	Graphic Log	Approx. S Location:	Surface El. (feet, M N 245939.7841 I	E 2198469.3014	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		Zone of fr	ractured Limestone 29.								>			
_														
32-						48	48							
				32	2.9									
_														
-		CODING	TEDMINIATED AT 24	34	.3									
_			TERMINATED AT 34.3											
36-			ADVANCER USED TO JE LOOSE ROCK COL	SET CASING TO 18.1 APSING IN HOLF										
_														
-	1													
_	-													
40 –														
-														
_	1													
14 –														
-	1													
-	-													
48-														
_														
-														
-	-													
52-														
_														
-	1													
-	-													
56-														
_														
-														
_	1													
<del>60</del> -														L
Com		Depth (ft.):	34.3 4/12/18	Remarks: Ground										
	Starte Comp		4/12/18 4/16/18	drilling activities. backfilled with cut	ttings ttings	was Borir	move na wa	ea to 7.6 is comp	OTTS leted	et. B with	oring a	was	;	
Orille	ed By:	ľ	MW / Bill Woods	truck-mounted dri	illrig E	levat	ດກs v	vere pro	vided	by N	veel-S	Scha	ffer.	
_ogg	ged By	: E	Buehler											_



## **TEST BORING NO. MCB-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PRO IECT NO : 300-18-0001 Shoot 1 of 2

	Geotechnical • CEI	Environmental	PROJECT	NO.: 3	00-18	3 <b>-</b> 000	1			;	Sheet	1 of	2
Depth, feet Graphic Log	Approx. Sur	face El. (feet, MS N 245514.4339 E	2200060.9280	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	:
	ASPHALT (3 BASESTONE A-1			0 <u>.</u> 3⁄ 2 <u>.</u> 5						_>			
4 -	LEAN CLAY A-7-5	(CL), gray, moist, fir	m to stiff, (FILL)	2.5	67		4-5-6			22.4	56	23	:
8 -					78		4-6-4			23.0			
-					67		2-2-5			31.1			
12-					100		2-3-5			28.7			
20-	LEAN CLAY A-7-5	(CL), gray, moist, ve	1, ery stiff, chert fragments	8.5	100		2-11-10			15.2			
24-					100		6-6-10			25.7			
-28	\ BEGAN COR RUN 1	USAL AT 27.2 FBG RING AT 27.2 FBGS , weathered with mu	S	7.2	100	43							
Completion Date Starte Date Completion Drilled By: Logged By	pleted: 4/19 MW	3/18	Remarks: Ground drilling activities. small rod drops. location. Elevator	Boring Elevatio	mov n wa	ed to s abo	12' offse out 0.5' le	et NE ower	. Drii than	ller re	port	ed 2 ed	



## **TEST BORING NO. MCB-1**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

PRO IECT NO : 300-18-0001 Shoot 2 of 2

		K. S. Ware & Associates, L.L.C.  Geotechnical • CEI • Environmental	PROJECT N	O.: 3	00-18	3-0001	I				Sheet	2 of	2
Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL): Location: N 245514.4339 E 2200  MATERIAL DESCRIPTION	0060.9280	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		RUN 2			88	50							
32			32.2										
-			33.4	Ш									
		RUN 3 LIMESTONE, gray, hard, argillaceous w partings											
36-				Ш	100	100							
-				Ш									
-		 RUN 4	38.4	44									
	$\Box$	NON 4		Ш									
40				Ш	100	100							
			40.4	Ш									
		CORING TERMINATED AT 42.4 FBGS	42.4										
44-													
-													
48-													
52-													
. 4													
-56-													
60 Comp	eletion	Depth (ft.): <b>42.4</b> Rema		ater w	⊥ ⁄as N	IOT e	ncounte	red c	∟ Iurino	or a	∟ ıfter		
Date Date	Starte	d: 4/18/18 drill leted: 4/19/18 sma MW / Bill Woods loca	ing activities. Bell rod drops. Election. Elevatons	oring evatio	mov on wa	ed to	12' offs out 0.5' l	et NE ower	. DriÌ than	ler re	port	ed 2 ed	



## **TEST BORING NO. MCB-2**

PROJECT NAME: TDOT I-75 Interchange LOCATION: Chattanooga, Tennessee

PRO IECT NO - 300-18-0001

Depth, feet	Graphic Log	Approx. Surface El. (feet, MSL Location: N 245335.1581 E 2	199861.8997	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
		ASPHALT (9.6 inches)  BASESTONE (26.4 inches)  A-1	<u>0.</u> 8		56		13-12-10			3.6			
· 4 –		LEAN CLAY (CL), brown and gray, A-7-5	moist and firm, (FILL)		0		3-4-4						
. –					100		2-2-5			29.3			
  - 12-					40		3-4-8			25.6			
  -16- 		LEAN CLAY (CL), Residual soil, m A-7-5		<u>,                                    </u>	100		8-5-6			18.8			
- 20- - -					100		5-6-9			19.8			
- 24 -   - 28 -		FAT CLAY (CH), brown to gary with to 1" A-7-6 Becoming wet from 24.3'	<u>23.</u> t chert fragments up	5	100		5-5-9			26.3			
Date Date Drille	pletion Starte Comp ed By:	d: 4/19/18 leted: 4/19/18 MW / Bill Woods	Remarks: Groundw Irilling activities. B packfilled with cutt ruck-mounted drill	oring ings.	was Borin	move ig wa	ed to 10' is compl	offse eted	et. Bowith	oring a	was	ffer.	



## **TEST BORING NO. MCB-2**

PROJECT NAME: TDOT I-75 Interchange

LOCATION: Chattanooga, Tennessee

	K. S. Ware & Associates, L.L.C. Geotechnical • CEI • Environmental	PROJECT NO	D.: 3	00-18	-000°	1				Sheet	2 of	2
Depth, feet Graphic Log	Approx. Surface El. (feet, MSL): Location: N 245335.1581 E 219	99861.8997	Samples	Recovery (%)	RQD (%)	SPT Values	Pocket Pen (tsf)	Percent Fines	Water Content (%)	Liquid Limit	Plastic Limit	
	MATERIAL DESCRIP	TION		100		5-7-11			×			Ļ.
-32	AUGER RFUSAL AT 31.1 FBGS BEGAN CORING AT 31.1 FBGS	31.1		,		0 7 11			16.5			
	RUN 1 LIMESTONE, gray, hard, argillaceous shale partings	with occasional	П	95	87							
	RUN 2	34.9	$\blacksquare$									
-36			П	98	84							
40	RUN 3	<u>39.</u> 9	H	100	100							
.	CORING TERMINATED AT 42.1	42.1										
44-												
-48-												
-52-												
-56-												
-60 - Completior Date Starte Date Comp Drilled By:	d: 4/19/18 dri bleted: 4/19/18 ba	marks: Groundwa Iling activities. Bo ckfilled with cuttin ck-mounted drillr	ring ngs.	was Borir	move ng wa	ed to 10' is compl	offse eted	et. Bowith	oring a	was		



5409 Maryland Way, Suite 150 Brentwood, Tennessee 37027 615.712.2180

May 2, 2022

Neel-Schaffer, Inc. 210 25<sup>th</sup> Avenue North, Suite 800 Nashville, Tennessee 37203

Attention: Mr. Richard Sullivan, PE, Associate DBIA

Subject: Geotechnical Exploration Data - Revision 1

I-24/I-75 Interchange Improvements Phase II - 30 Percent Report

Chattanooga, Tennessee File No. 24647-009-00

#### **INTRODUCTION**

GeoEngineers, Inc. (GeoEngineers) has completed the geotechnical exploration supporting the development of the 30 Percent Report for the I-24/I-75 Interchange Improvements Phase II project located in Chattanooga, Tennessee for Neel-Schaffer, Inc. (NS). This revised letter summarizes the details of the field exploration and laboratory testing and provides the data obtained. Our services were performed in accordance with our Revised Proposal for Geotechnical Services dated March 29, 2022 and we were authorized by Richard Sullivan of Neel-Schaffer, Inc. by signed acceptance of our proposal on March 31, 2022. We issued our original report on April 28, 2022. Subsequent to our report submittal, NS requested that we provide additional laboratory data. This revised report includes the requested information.

#### FIELD EXPLORATION

#### **General Field Exploration Information**

GeoEngineers' field exploration took place between March 21, 2022 to April 18, 2022. We performed our field exploration both during the day and night. Daytime field services took place during March 21, 2022 to April 4, 2022. Nighttime field services took place on April 7, 10, 12, 13, and 18, 2022. A rubber tiremounted drill rig with automatic hammer was used for the duration of the soil boring exploration.

#### **Exploration Coordination**

GeoEngineers contacted Tennessee "One-Call" to locate utilities prior to performing the field exploration. We obtained work zone permits from the Chattanooga Transportation Department, and the Tennessee Department of Transportation (TDOT). GeoEngineers also coordinated with traffic control subcontractors to provide the appropriate signage, lighting, and police presence during our field operations. GeoEngineers

representative Emily Reed, P.E. made a site visit on March 11, 2022 to meet with TDOT survey personnel and our driller to evaluate drill rig access, and adjust proposed boring locations previously staked in the field by TDOT. TDOT surveyed the as-built boring locations and provided the soil boring survey coordinates and elevations to GeoEngineers on April 11, 2022. This survey information is presented on the soil boring logs in Appendix A.

#### **Soil Borings**

A total of thirty-one (31) soil borings were advanced using hollow stem auger drilling methods. Of these borings, two borings (Boring RW1-1A and Boring RW11-1A) were offset from their proposed locations due to shallow refusal. Samples of the subgrade were mostly collected by performing standard penetration tests (SPT) in general accordance with ASTM D1586 using a 2-inch O.D. split spoon sampler. Where SPT tests were performed, blow counts are shown on the boring logs in Appendix A and a disturbed sample was collected for classification and further evaluation.

Soil boring termination depths ranged between 4-3/4 and 50 feet below ground surface. Sampling was conducted in general accordance with applicable ASTM standards.

Immediately upon retrieval from the subsurface, each sample was examined by our field representative and visually classified. Disturbed SPT samples were sealed in plastic bags, labeled, and transported to the laboratory for testing. Laboratory results for those samples selected for testing are provided on the borings logs in Appendix A and in Appendix B.

The soil borings were backfilled with auger cuttings and asphalt cold patch upon completion.

#### **Roadway Pavement Coring**

A total of six (6) roadway pavement corings were completed in Interstate 24 in both eastbound and westbound directions. The existing concrete pavement was cored using a 6-inch diameter core barrel to expose the underlying aggregate base course. The base course was excavated using hand tools to expose the underlying soil. Dynamic Cone Penetrometer (DCP) testing was performed on the soil to estimate California Bearing Ratio (CBR) values. Individual DCP readings and CBR estimates are provided in Appendix C. Summaries of the coring data obtained are provided in Tables 1 and 2 below.

TABLE 1. I-24 EASTBOUND ROADWAY PAVEMENT CORING DATA SUMMARY

Coring ID	EB-1	EB-2	EB-3
Latitude <sup>1</sup>	35°0'23.39"N	35°0'19.55"N	35°0'16.98"N
Longitude <sup>1</sup>	85°13'54.78"W	85°13'43.65"W	85°13'31.84"W
Travel Lane	Right	Middle	Left
Concrete Pavement Thickness (in)	12	12	12
Aggregate Base Course Thickness (in)	7	7	6
Average CBR Estimate <sup>2</sup>	31	24	31

 $<sup>{}^{1}\!\</sup>text{Coordinate}$  data is approximate and was obtained using a handheld GPS device.



<sup>&</sup>lt;sup>2</sup>Average of CBR estimates calculated for each boring. For individual CBR calculations, please see Appendix C.

TABLE 2. I-24 WESTBOUND ROADWAY PAVEMENT CORING DATA SUMMARY

Coring ID	WB-1	WB-2	WB-3
Latitude <sup>1</sup>	35°0'16.79"N	35°0'18.46"N	35°0'21.69"N
Longitude <sup>1</sup>	85°13'25.82"W	85°13'37.74"W	85°13'48.83"W
Travel Lane	Right	Middle	Left
Concrete Pavement Thickness (in)	12	12	12
Aggregate Base Course Thickness (in)	8	7	4 1/2
Average CBR Estimate <sup>2</sup>	45	37	13

<sup>&</sup>lt;sup>1</sup>Coordinate data is approximate and was obtained using a handheld GPS device.

#### **LIMITATIONS**

We have prepared this report exclusively for use by Neel-Schaffer for the I-24/I-75 Interchange Improvements Phase II project in Chattanooga, Tennessee.

Within the limitations of scope, schedule, and budget, our services have been executed in accordance with generally accepted practices in the field of geotechnical engineering in this area at the time this report was prepared. No warranty or other conditions, express or implied, should be understood.

An electronic form or hard copy of this document (e-mail, text, table, and/or figure), if provided, and any attachments are only a copy of a master document. The master hard copy is stored by GeoEngineers. and will serve as the official document of record.

Please refer to Appendix D entitled *Report Limitations and Guidelines for Use* for additional information pertaining to use of this report.

#### **CLOSING**

We appreciate the opportunity to be of service to Neel-Schaffer. If you have any questions about this letter, please email or call.

Sincerely,

GeoEngineers, Inc.

Emily C. Reed, PE Geotechnical Engineer

Attachments:

Appendix A. Logs of Soil Borings

Appendix B. Laboratory Test Results

Appendix C. CBR Estimates Based on DCP

Appendix D. Report Limitations and Guidelines for Use

Blake E. Cotton, PE Senior Principal



<sup>&</sup>lt;sup>2</sup>Average of CBR estimates calculated for each boring. For individual CBR calculations, please see Appendix C.



APPENDIX A
Logs of Soil Borings

#### **SOIL CLASSIFICATION CHART**

	AAJOR DIVIS	IONE	SYM	BOLS	TYPICAL		
	MAJUR DIVIS	IUNS	GRAPH	LETTER	DESCRIPTIONS		
	GRAVEL	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES		
	AND GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES		
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES		
30123	FRACTION RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES		
MORE THAN 50%	SAND	CLEAN SANDS		sw	WELL-GRADED SANDS, GRAVELLY SANDS		
RETAINED ON NO. 200 SIEVE	AND SANDY SOILS	(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND		
	MORE THAN 50% SANDS WIT OF COARSE FRACTION PASSING FINES			SM	SILTY SANDS, SAND - SILT MIXTURES		
	ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		sc	CLAYEY SANDS, SAND - CLAY MIXTURES		
				ML	INORGANIC SILTS, ROCK FLOUR, CLAYEY SILTS WITH SLIGHT PLASTICITY		
FINE GRAINED	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS		
SOILS				OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY		
MORE THAN 50% PASSING NO. 200 SIEVE				МН	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS SILTY SOILS		
	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		СН	INORGANIC CLAYS OF HIGH PLASTICITY		
				ОН	ORGANIC CLAYS AND SILTS OF MEDIUM TO HIGH PLASTICITY		
	HIGHLY ORGANIC S	SOILS		PT	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS		

NOTE: Multiple symbols are used to indicate borderline or dual soil classifications

#### **Sampler Symbol Descriptions**

2.4-inch I.D. split barrel / Dames & Moore (D&M)

Standard Penetration Test (SPT)

Shelby tube

Piston
Direct-Push

Bulk or grab

Continuous Coring

Blowcount is recorded for driven samplers as the number of blows required to advance sampler 12 inches (or distance noted). See exploration log for hammer weight and drop.

"P" indicates sampler pushed using the weight of the drill rig.

"WOH" indicates sampler pushed using the weight of the hammer.

#### **ADDITIONAL MATERIAL SYMBOLS**

SYM	BOLS	TYPICAL
GRAPH	LETTER	DESCRIPTIONS
	AC	Asphalt Concrete
	cc	Cement Concrete
<b>13</b>	CR	Crushed Rock/ Quarry Spalls
7 71 71 71 71 71 71 71 71 71 71 71 71 71	SOD	Sod/Forest Duff
	TS	Topsoil

#### **Groundwater Contact**



Measured groundwater level in exploration, well, or piezometer



Measured free product in well or piezometer

#### **Graphic Log Contact**

Distinct contact between soil strata

Approximate contact between soil strata

#### **Material Description Contact**

Contact between geologic units

\_\_\_\_\_ Contact between soil of the same geologic

#### **Laboratory / Field Tests**

%F Percent fines %G Percent gravel AL Atterberg limits CA Chemical analysis

**CP** Laboratory compaction test

CS Consolidation test
DD Dry density
DS Direct shear
HA Hydrometer analysis

MC Moisture content

MD Moisture content and dry density
Mohs Mohs hardness scale

OC Organic content
PM Permeability or hydraulic conductivity

PI Plasticity index
PL Point lead test

PP Pocket penetrometer
SA Sieve analysis

TX Triaxial compression

UC Unconfined compression

UU Unconsolidated undrained triaxial compression

VS Vane shear

#### **Sheen Classification**

NS No Visible Sheen SS Slight Sheen MS Moderate Sheen HS Heavy Sheen

NOTE: The reader must refer to the discussion in the report text and the logs of explorations for a proper understanding of subsurface conditions. Descriptions on the logs apply only at the specific exploration locations and at the time the explorations were made; they are not warranted to be representative of subsurface conditions at other locations or times.

### Key to Exploration Logs



Figure A-1

Drilled	<u>Start</u> 3/24/2022	<u>End</u> 3/24/2022	Total Depth (ft)	12	Logged B Checked	•	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger		
Surface Vertical	Elevation (ft) Datum		3.26 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X		
Easting Northing			175.21 78.3938		System Datum		Geographic NAD83 (feet)	Groundwater not observed at time of exploration			
Notes:	I-24 STA 102+	88.65, Offset -:	129.6885 fe	et							

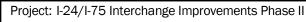
FIELD DATA Elevation (feet) Collected Sample Sample Name Testing Group Classification **MATERIAL** Graphic Log o Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (5 inches) Gravel base (9 inches) GW 15 Reddish brown lean clay with chert (stiff, moist) (residuum) CL 12 21.5 12 29

Boring terminated at approximately 12 feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols.

 ${\bf Coordinates\ Data\ Source:\ Coordinates\ and\ elevations\ provided\ by\ TDOT\ Region\ 2\ Survey\ Office.}$ 





Project Location: Chattanooga, Tennessee



Drilled	<u>Start</u> 3/24/2022	<u>End</u> 3/24/2022	Total Depth (ft)	11.75	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Vertical	Elevation (ft) Datum		2.91 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X	
Easting Northing			164.054 83.8355		System Datum		Geographic NAD83 (feet)	Groundwater not observed at time of exploration		
Notes:	I-24 STA 102+	-76.25, Offset -:	130.1964 fe	et						

FIELD DATA Interval Recovered (in) Elevation (feet) Collected Sample Sample Name Testing Group Classification **MATERIAL** Graphic Log o Depth (feet) Blows/foot Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS DESCRIPTION** AC Asphalt concrete pavement (5 inches) Gravel base (7 inches) GW Offset from boring RW1-1 about 15 feet Augering only, no SPT sampling west due to shallow refusal 10

Boring terminated at approximately  $11^3\!4$  feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols.

 ${\bf Coordinates\ Data\ Source:\ Coordinates\ and\ elevations\ provided\ by\ TDOT\ Region\ 2\ Survey\ Office.}$ 





Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/24/2022	<u>End</u> 3/24/2022	Total Depth (ft)	44.75	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		7.35 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			323.567 11.3646		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 104+	51.44, Offset -:	127.8224 fe	et					

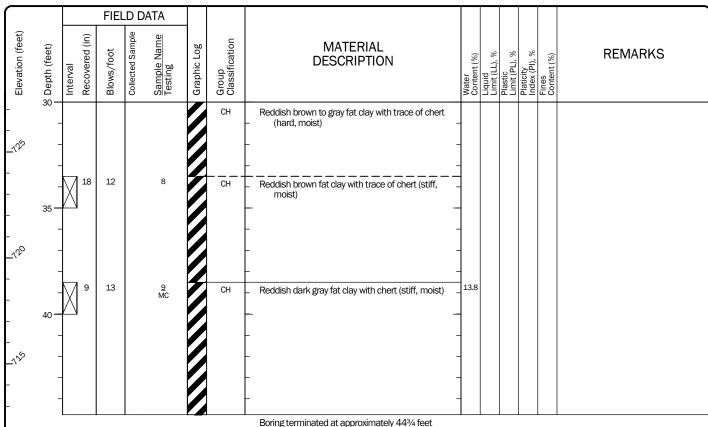
FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log o Depth (feet) Water Content (%) Liquid Limit (LL), % Plastic Limit (PL), % Platicity Index (PI), % **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (7½ inches) Gravel base (5 inches) GW 10 Reddish brown clayey sand with chert (firm, moist) (residuum) SC 15 14.3 35 20 15 21 AASHTO (GI) A-2-6 (0) MC; SA; AL 10 18  $\mathsf{CL}$ Tan silty lean clay with trace of chert (stiff, moist) 11 Tan lean clay with some chert (stiff, moist) 20 16 18 CL Reddish brown lean clay with chert (very stiff, 25 33 Reddish brown to gray fat clay with trace of chert (hard, moist) СН Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW1-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Boring terminated at approximately 443/4 feet below ground surface due to auger refusal

## Log of Boring RW1-2 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/23/2022	<u>End</u> 3/23/2022	Total Depth (ft)	50	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		7.89 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			162.605 53.6375		System Datum		Geographic NAD83 (feet)	See "Remar	ks" section for groundwater observed
Notes:	I-24 STA 106+	·01.91, Offset -:	130.7852 fee	et					

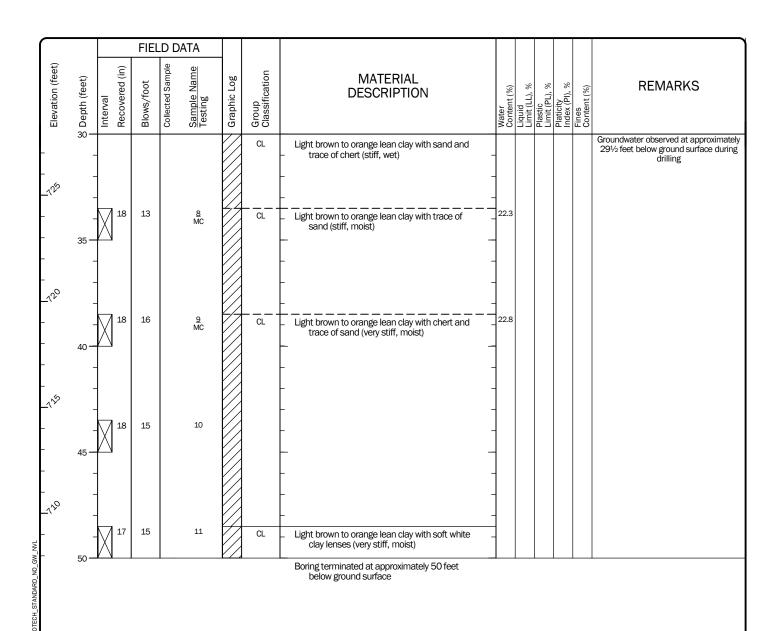
			FIEL	D D	ATA			
Elevation (feet)	o Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	MATERIAL Content (%) Initial (LL), % Heatich Initial (PL), % Heatich Initial (
- - _16 <sup>5</sup>	- - -	12.5	8		1		AC GW CL	Asphalt concrete pavement (7½ inches)  Gravel base (8½ inches)  Reddish brown to orange lean clay with chert (stiff, moist) (residuum)  -
- -	5 <del>-</del>	12	11		2			
- _160 - -	10-	12.5	13		<u>3</u> MC			
DARPO_NO_GW_NVL	- - - 15 —	15.5	15		4		CL	Reddish brown to orange lean clay with chert (very stiff, moist)
20 - 20 - 20 - 20 - 20 - 20 - 20 - 20 -	- - - 20 —	15	11		<u>5</u> MC		CL	Light brown to orange lean clay with trace of chert (stiff, moist)
	- - 25 —	12	11		6			
4947009/GNN (2494700900LBP) DELDIFAR/LIDRA VEDERANINEENS	30-	16	12		7 MC			Light brown to orange lean clay with sand and trace of chert (stiff, wet)
CC NC					anation of ordinates			s provided by TDOT Region 2 Survey Office.

# Log of Boring RW1-3



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



# Log of Boring RW1-3 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/23/2022	<u>End</u> 3/23/2022	Total Depth (ft)	26.5	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		3.71 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			597.576 92.3785		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 107+	50.12, Offset -:	128.8874 fe	et					

FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (12 inches) 8 GW Gravel base (4 inches) Orange to brown lean clay with trace of chert CL (stiff, moist) (residuum) 5  $\mathsf{CL}$ Orange to brown lean clay with trace of chert 18 14 Orange to brown lean clay with trace of chert and  $\mathsf{CL}$ soft white clay lenses (stiff, moist) 10 12 14 22.9 47 AASHTO (GI) A-7-6 (6) MC;  $\frac{4}{SA}$ ; AL SC Orange to brown clayey sand with chert (firm, 12 20 Orange to brown clayey sand with chert and soft white clay lenses (firm, moist) 13 10 SC 27.5 25 Boring terminated at approximately 26½ feet below ground surface due to auger refusal Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW1-4



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/22/2022	<u>End</u> 3/22/2022	Total Depth (ft)	50	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		5.21 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			730.589 32.6427		System Datum		Geographic NAD83 (feet)	See "Remar	ks" section for groundwater observed
Notes:	I-24 STA 108+	-95.92, Offset -:	127.5987 fee	et					

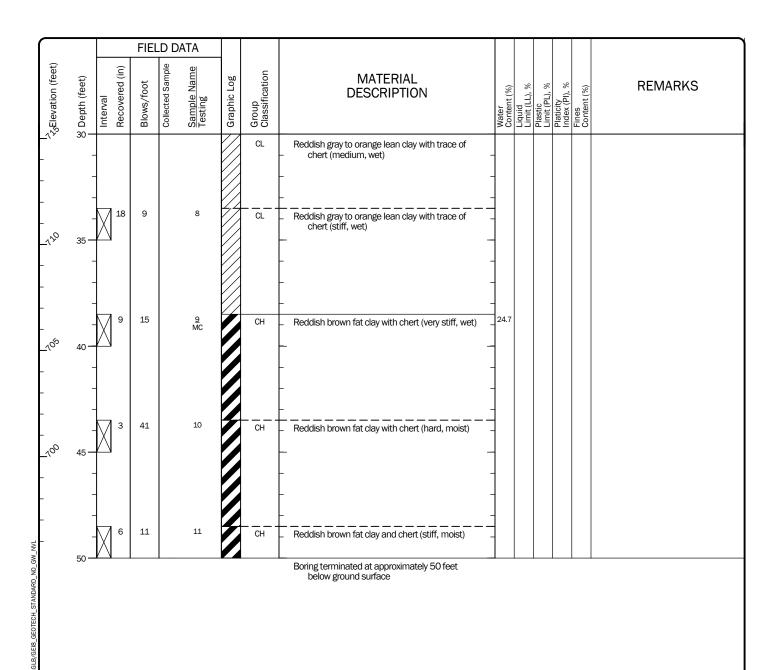
			FIEL	D D	ATA			
		Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	MATERIAL Content (%) Liquid Limit (LL), % Heating Fines Content (%) Platicity Fines Content (%) Conten
_^^" - -	0 —	6	15		1	2	AC GW CL	Asphalt concrete pavement (7½ inches)  Gravel base (4½ inches)  Reddish gray to orange lean clay (very stiff, moist) (residuum)
- _140 -	5 <b>-</b>	10	10		<u>2</u> MC		CL	Reddish gray to orange lean clay with trace of chert (stiff, moist)
- - ^5 1 -	- - 10 <del>-</del>	18	11		3			
H_STANDARD_NO_GW_NNL	- - 15 <del>-</del> -	5.5	5		4 MC		CL CL	Reddish gray to orange lean clay with trace of chert (medium, moist)
STD_US_JUNK_2017.61B/GEI8_GEOTEC	- 20 <del>-</del> -	2	WOH		<u>5</u> MC			Reddish gray to orange lean clay with trace of chert (very soft, wet)  Groundwater observed at approximately 18 feet below ground surface during drilling
1647009 (GINT) 2464700900 GPU DBLUbran/Librar/GEORNAINERS, DF. STD. US, JUNK 2017 GLB/GEB GEOTECH, STANDARD, NO. GW. MNI.	- 25 <b>-</b> -	7.5	21		6		CL	Reddish gray to orange clay with chert (very stiff, wet)
VGINT\2464700900.GPJ	- 30 —	13 e Figure	7 A-1 fo	r expl	7 MC anation of	f syml	CL	Reddish gray to orange lean clay with trace of chert (medium, wet)
Coord								s provided by TDOT Region 2 Survey Office.

# Log of Boring RW1-5



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



# Log of Boring RW1-5 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/22/2022	<u>End</u> 3/22/2022	Total Depth (ft)	50	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		5.96 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			171.062 94.2129		System Datum		Geographic NAD83 (feet)	See "Remarl	ks" section for groundwater observed
Notes:	I-24 STA 113+	-95.07, Offset -	36.1350 feet						

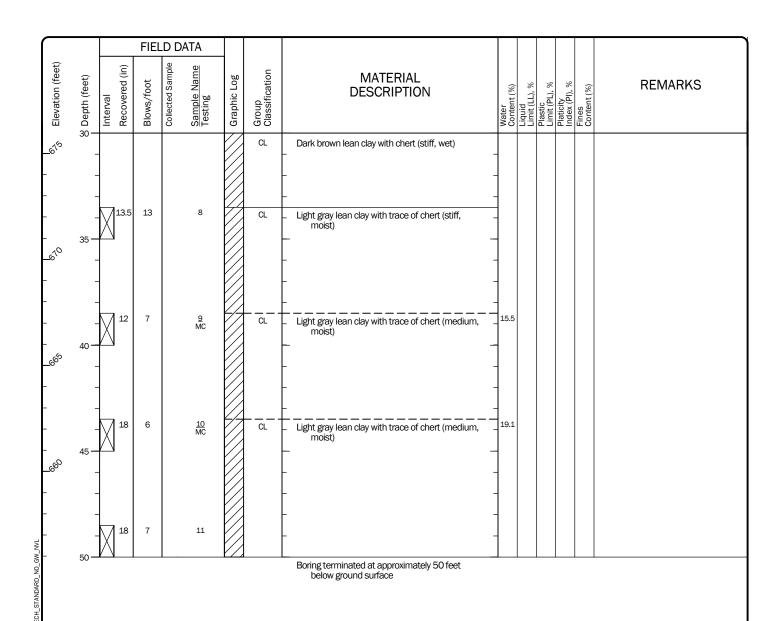
$\succeq$			FIEL	D D	ATA										
Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	MATERIAL DESCRIPTION		Water Content (%)	Liquid Limit (LL), %	Plastic Limit (PL), %	Platicity Index (PI), %	Fines Content (%)	REMARKS
_105	0-	18	9		1		TS CL	Topsoil (4 inches)  Dark brown lean clay (stiff, moist) (fill)							
-	-						CL	Grayish brown lean clay with trace chert (stiff, moist) (fill)	_						
-	5 <b>-</b>	18	10		2		CL	Light gray and orange lean clay (stiff, moist)     (residuum)	-						
_100 _100	-	-						- -	-						
-	-	18	12		<u>3</u> MC			- -	-	18.4					
_0g/s	10 —	Å			IVIC			_							
<u>-</u> 6	-	-						<del>-</del>	_						
- NAC	-	18	13		4		CL	Light gray and reddish orange lean clay (stiff,							
ADARD_NO_GW	15 —	Å						moist) 	_						
DF-SID_USE_JONE_2017.4EB/SEB_GEOTICE_SIANDARD_NO_GW_NNL	-	-						- -	_						
3/4	-	18	8		<u>5</u> MC; SA; AL		CL	Light gray lean clay with trace of chert (stiff,		21.2	30	19	11	86	AASHTO (GI) A-6 (8)
JUNE_2017.GLB	20 —	Й			IVIC, SA, AL			moist)	_						
0	-	-						-	_						
	-	18	8		<u>6</u> MC		CL	Gray and orange lean clay with chert (stiff, very)		19.4					
//Library:GEOENG	25 —	И			IVIC			moist to wet)							
DBLIbrary/Lil	-							- -	-						
74/003/GIN 1/2404/00300.GPJ DELUFARY/LDFAN/SERENSINEENS.	-	16	13		7 MC		CL	Dark brown lean clay with chert (stiff, wet)		24.6					Groundwater observed at approximately 28 feet below ground surface during drilling
GIN1/2404	30 <del>-</del>	e Figure	A-1 fo	r eynl	anation of	f symb	nols	_	_						uniling
Co	oordina	ites Data	Sour	ce: Co	ordinates	and e	elevation	s provided by TDOT Region 2 Survey Office.							

# Log of Boring RW1-6



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



# Log of Boring RW1-6 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

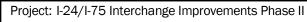
Drilled	<u>Start</u> 4/4/2022	<u>End</u> 4/4/2022	Total Depth (ft)	10.25	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical I	Elevation (ft) Datum		9.32 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting (			169.243 76.3326		System Datum		Geographic NAD83 (feet)	Groundwate	er not observed at time of exploration
Notes:	I-24 STA 139+	08.58, Offset -	76.1981 fee	t	·				

			FIEL	D D	ATA									
Elevation (feet)	, Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Water Content (%)	Liquid Limit (LL), %	Plastic Limit (PL), %	Platicity Index (PI), %	Fines Content (%)	REMARKS
-	0 —						TS	Topsoil (8 inches)						
-	-	8	10		1		CL	Tan lean clay with small roots (stiff, moist) (residuum)						
	_							- -						
_6/s	-	18	13		MC; $\frac{2}{SA}$ ; AL		CL	Gray sandy lean clay with chert (stiff, moist)	16.4	44	22	22	51	AASHTO (GI) A-7-6 (8)
-	5—													
-	_							-						
f	_							-						
_610	-	$\bigvee$ $\circ$	50		3			Gray sandy lean clay with chert (hard, moist)						
	10 —							Poring torminated at approximately 101/, foot						

Boring terminated at approximately  $10^{1/4}$  feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

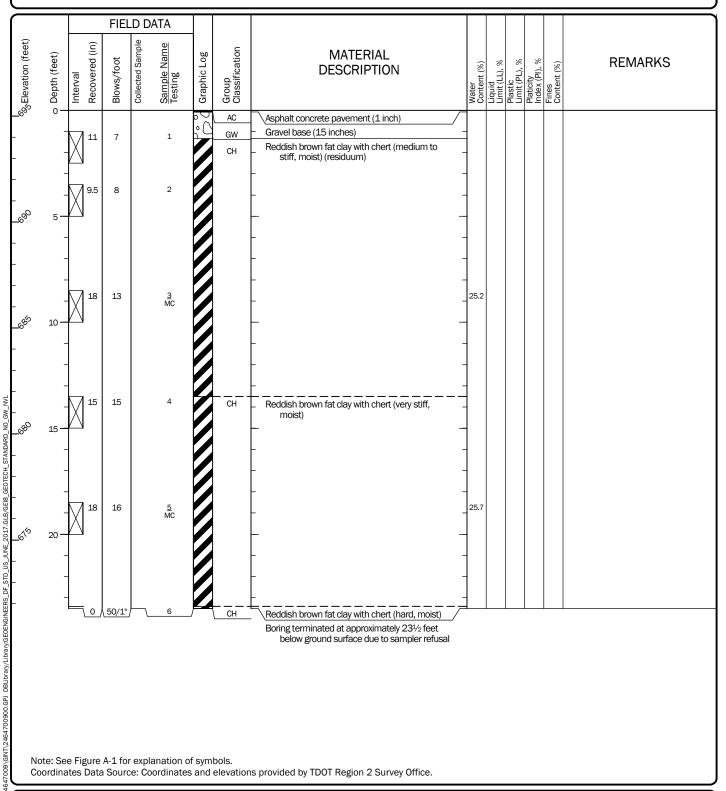




Project Location: Chattanooga, Tennessee



Drilled	<u>Start</u> 3/21/2022	<u>End</u> 3/21/2022	Total Depth (ft)	23.5	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		5.27 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			976.674 36.4734		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 155+	-14.81, Offset -:	167.9401 fe	et					



## Log of Boring RW3-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/21/2022	<u>End</u> 3/21/2022	Total Depth (ft)	23.5	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		4.42 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			133.783 17.857		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 156+	-88.55, Offset -	139.4983 fe	et					

FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval Asphalt concrete pavement (1 inch) Gravel base (13½ inches) GW 14 Reddish brown fat clay with chert (stiff, moist) (residuum) 13 15 18.3 9.5 Reddish brown fat clay with chert (very stiff, 10 16 AASHTO (GI) A-7-5 (36) 28.8 64 MC; SA; AL МН Grayish brown elastic silt (very stiff to hard, 18 <u>5</u> MC 25.6 Boring terminated at approximately 23½ feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

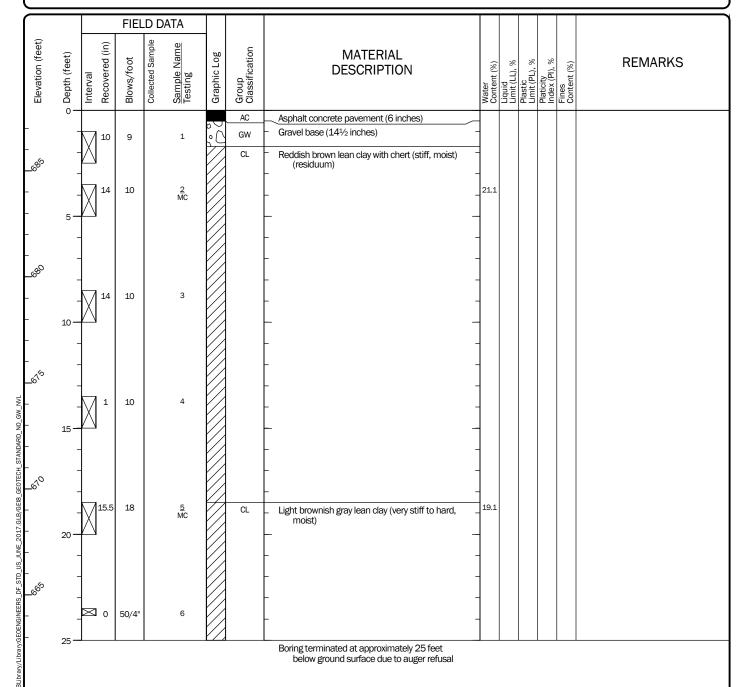
## Log of Boring RW3-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/21/2022	<u>End</u> 3/21/2022	Total Depth (ft)	25	Logged By Checked By	ECR RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Elevation (ft) Vertical Datum		687.86 NAVD88			Hammer Data	/ tatoriatio i farili i foi		Drilling Equipment	CME 550X	
Easting Northing		2200333.288 245443.2266		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration		
Notes: I-24 STA 159+03.94, Offset -108.3242 feet										



Note: See Figure A-1 for explanation of symbols.

Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

## Log of Boring RW3-3



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/25/2022	<u>End</u> 3/25/2022	Total Depth (ft)	50	Logged Checke	•	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger		
	Surface Elevation (ft) Vertical Datum		736.36 NAVD88		Hammer Data	-	Automatic Hammer 140 (lbs) / 30 (in) Drop		CME 550X		
	Easting (X) Northing (Y)		2195280.625 247262.5027		System Datum		Geographic NAD83 (feet)	See "Remar	ks" section for groundwater observed		
Notes:	Notes: I-24 STA 105+12.01, Offset 117.3423 feet										

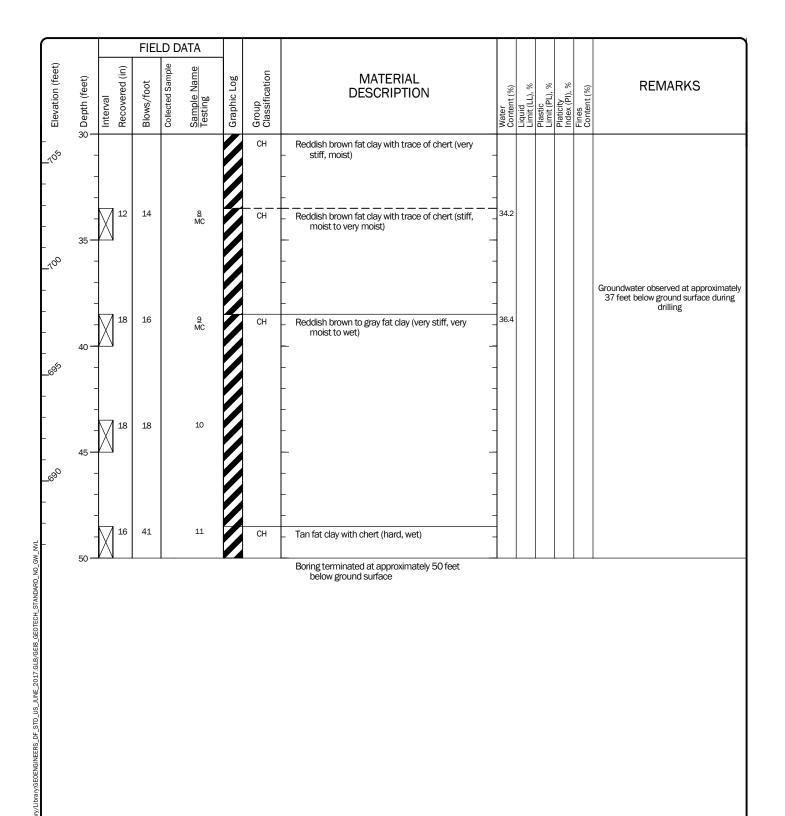
FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log o Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (4½ inches) Gravel base (8½ inches) GW 16 Reddish brown fat clay with chert (very stiff, moist) (residuum) 15 14 CL Tan lean clay with chert (stiff to very stiff, moist) 18 17.8 10 Tan lean clay with trace of chert (stiff, moist to very moist)  $\mathsf{CL}$ Reddish brown to gray lean clay with trace of chert (stiff, moist) 18 11 CL 27.2 18 18 СН Reddish brown fat clay with trace of chert (very stiff, moist) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW4-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



# Log of Boring RW4-1 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/25/2022	<u>End</u> 3/25/2022	Total Depth (ft)	39.5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Elevation (ft) Vertical Datum		737.98 NAVD88			Hammer Data	Automatic Hammer 140 (lbs) / 30 (in) Drop		Drilling Equipment	CME 550X	
Easting Northing		2195539.937 247150.9248			System Datum		Geographic NAD83 (feet)	See "Remar	ks" section for groundwater observed	
Notes: I-24 STA 107+94.30, Offset 115.3873 feet										

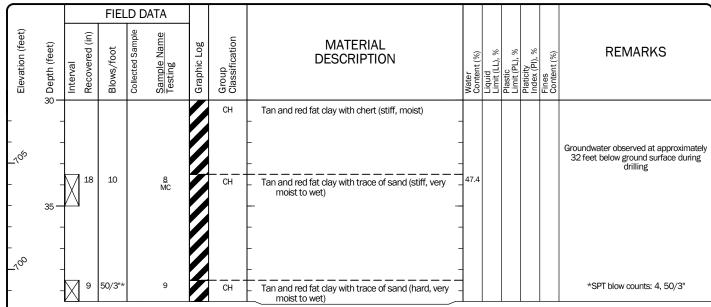
FIELD DATA Elevation (feet) Collected Sample Sample Name Testing Group Classification **MATERIAL** Graphic Log o Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (1 inch) Gravel base (5 inches) GW 11 1 Tan lean clay with chert (stiff, moist) (fill) 12 GP Gray gravel with sand and clay (firm, moist) (fill) 18 21.1 Tan fat clay with chert (very stiff, moist) 10 18 17  $\mathsf{CL}$ Tan to black lean clay with sand and chert (stiff to very stiff, moist) 13 24.7 20 14 MC;  $\frac{6}{\text{SA}}$ ; AL 45 82 AASHTO (GI) A-7-6 (17) 18 23.7 26 25 18 14 СН Tan and red fat clay with chert (stiff, moist) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW4-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Boring terminated at approximately 39½ feet below ground surface due to auger refusal

## Log of Boring RW4-2 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/28/2022	<u>End</u> 3/28/2022	Total Depth (ft)	28.5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Elevation (ft) Vertical Datum		734.19 NAVD88			Hammer Data	/ tatoriation larining		Drilling Equipment	CME 550X	
Easting (X) Northing (Y)		2195822.485 247027.6928		System Datum		Geographic NAD83 (feet)	Groundwate	er not observed at time of exploration		
Notes: I-24 STA 111+02.55, Offset 114.7737 feet										

FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval Asphalt concrete pavement (1 inch) Gravel base (12 inches) GW 8 Orange and brown fat clay with trace of chert СН (stiff, moist) (residuum) CH Orange and brown fat clay with chert (stiff to very 17 18 24.4 10 18 14 SC Orange and tan clayey sand with chert (firm, moist to very moist) 18.4 36 22 14 37.1 13 AASHTO (GI) A-6 (1) 18 <u>5</u> MC; SA; AL 20 Orange and tan fat clay with chert (stiff, very moist) 18 11 23.6 25 Boring terminated at approximately  $28\frac{1}{2}$  feet below ground surface due to sampler refusal Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

### Log of Boring RW4-3



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/28/2022	<u>End</u> 3/28/2022	Total Depth (ft)	45	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Elevation (ft) Vertical Datum		719.41 NAVD88			Hammer Data	Automatic Hammer 140 (lbs) / 30 (in) Drop		Drilling Equipment	CME 550X	
Easting Northing		2196082.656 246908.1161		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration		
Notes: I-24 STA 113+88.84, Offset 119.7990 feet										

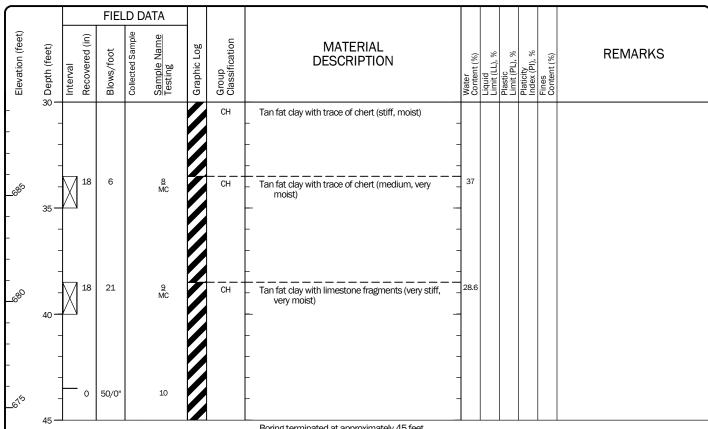
FIELD DATA Elevation (feet) Collected Sample Sample Name Testing Group Classification **MATERIAL** Graphic Log o Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** AC Asphalt concrete pavement (4½ inches) Gravel base (9 inches) GW 8 Brown and red lean clay with chert (stiff, moist) CL 10 17.9 Reddish brown lean clay with trace of chert (stiff, moist) (residuum) 18 Reddish brown fat clay with chert (stiff, moist) 13 27.3 Tan fat clay with trace of chert (stiff, moist) 16 18 14 Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW4-4



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Boring terminated at approximately 45 feet below ground surface due to auger refusal

# Log of Boring RW4-4 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/31/2022	<u>End</u> 3/31/2022	Total Depth (ft)	50	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Elevation (ft) Vertical Datum		710.82 NAVD88			Hammer Data	/ tatornation laminor		Drilling Equipment	CME 550X	
Easting Northing		2196254.28 246833.0678		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration		
Notes: I-24 STA 115+76.12, Offset 119.6505 feet										

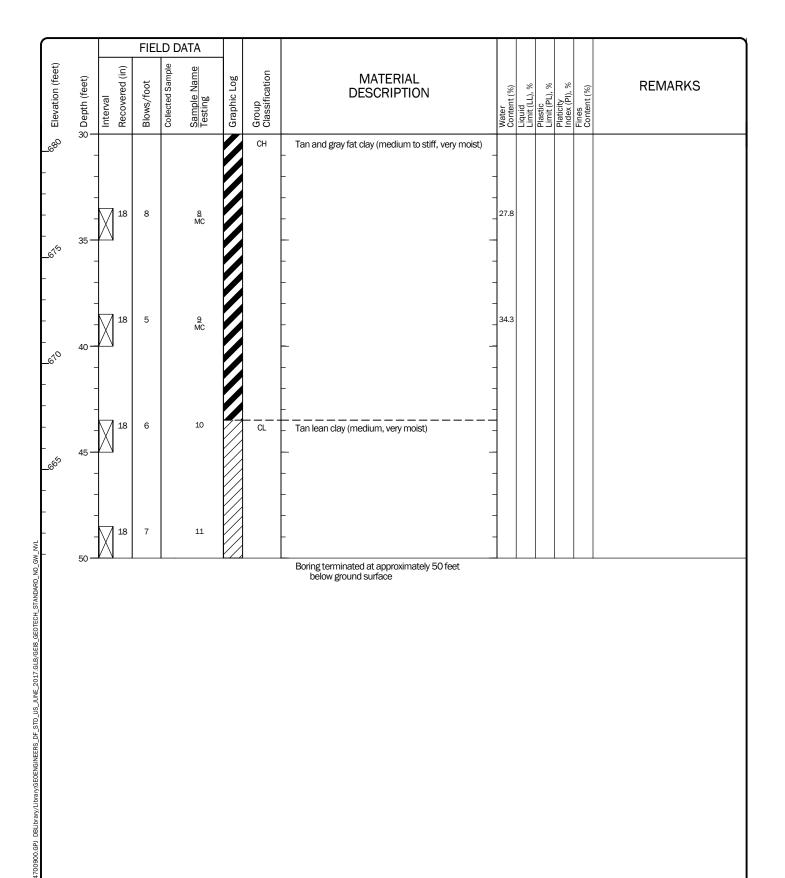
FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval Asphalt concrete pavement (4 inches) Gravel base (11 inches) GW 15 Reddish brown fat clay with chert and fine roots CH (very stiff, moist) (residuum) CH Reddish brown fat clay with chert (stiff, moist) 19 Reddish brown and gray fat clay with trace of chert (very stiff, moist) 22.7 18 Tan and gray fat clay (very stiff, moist) 18 17.9 18 СН 29.1 Tan and gray fat clay (stiff, very moist) 18 СН Tan and gray fat clay (medium to stiff, very moist) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW5-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



# Log of Boring RW5-1 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/31/2022	<u>End</u> 3/31/2022	Total Depth (ft)	50		Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
	urface Elevation (ft) 695.74 ertical Datum NAVD88				Har Dat	mmer ta		utomatic Hammer O (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2196470.067 Northing (Y) 246792.3681					stem tum		Geographic NAD83 (feet)	See "Remarl	ks" section for groundwater observed
Notes:	I-24 STA 117+	90.10, Offset 7	'0.3235 feet							

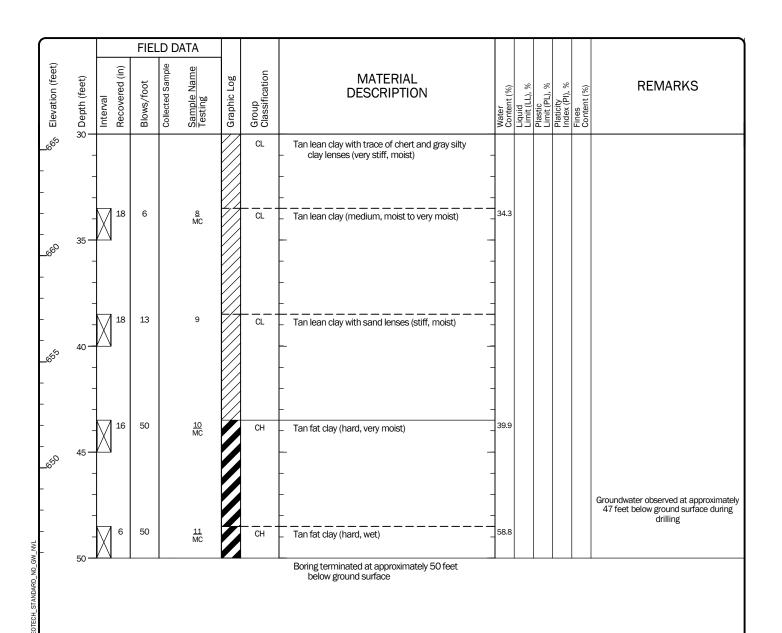
FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Water Content (%) Liquid Limit (LL), % Plastic Limit (PL), % Platicity Index (PI), % **REMARKS** Blows/foot **DESCRIPTION** Interval TS Topsoil (12 inches) 10 9 CH Reddish brown fat clay with chert (stiff, very CH Reddish brown fat clay with chert and pockets of gray silty clay (stiff, moist) (fill) 27.7 49 27 82 AASHTO (GI) A-7-6 (19) 18 9 Reddish brown and gray lean clay with sand and trace of chert (stiff, moist) (residuum) MC; SA; AL CL 10 18 16 Tan fat clay with trace of chert (very stiff, moist) 33 Tan fat clay with lenses of gray silty clay (stiff, 20 18 12 CL 30.1 Gray silty lean clay (stiff, moist) 25 18 15  $\mathsf{CL}$ Tan lean clay with trace of chert and gray silty clay lenses (very stiff, moist) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

## Log of Boring RW5-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Log of Boring RW5-2 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/29/2022	<u>End</u> 3/29/2022	Total Depth (ft)	10	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		9.82 VD88		Hammer Data		outomatic Hammer O (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			736.804 71.1963		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 131+	99.65, Offset 1	L30.8740 fee	et					

			FIEL	D D	ΑТА			
Elevation (feet)		Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification	MATERIAL Content (%) Liquid (IL), % Heartic (I
	0 —						TS	Topsoil (10 inches)
- -	-	12	27		1		GW	Gravel (firm, moist) (fill)
_&^	5 <b>—</b>	2	7		2		CL	Brown lean clay with trace of chert (medium, moist) (residuum)  —
- -	-							
_&o	10 —	9	50/3"*		3		CL	Brown lean clay with trace of chert and limestone fragments (hard, moist) specified with trace of chert and limestone fragments (hard, moist)
	10							Boring terminated at approximately 10 feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

## Log of Boring RW6-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/29/2022	<u>End</u> 3/29/2022	Total Depth (ft)	5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		8.78 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			024.149 69.7793		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 135+	-03.54, Offset 1	.08.4403 fee	t					

			FIEL	D DA	TA									
Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Water	Liquid Limit (LL). %	-	Platicity Index (PI), %	Fines Content (%)	REMARKS
-	0 <del>-</del> -	15	7	N	<u>1</u> 1C; SA; AL		CL CH	Topsoil (3 inches)  Brown and gray sandy gravelly lean clay (fill)  Brown fat clay with sand and trace of chert (medium, moist to very moist) (residuum)	29.	2 51	27	24	83	AASHTO (GI) A-7-6 (22)
_& -	- 5—	2	50/0"*		2			Brown fat clay with limestone fragments (hard, moist)						*SPT blow counts: 5, 7, 50/0"

Boring terminated at approximately 5 feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.





Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/29/2022	<u>End</u> 3/29/2022	Total Depth (ft)	19	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		4.15 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting Northing			292.844 15.8658		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 137+	99.37, Offset 1	.14.0966 fee	et					

FIELD DATA Elevation (feet) Collected Sample Sample Name Testing Group Classification **MATERIAL** Graphic Log Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (11/2 inches) Gravel base (15 inches) GW Reddish brown fat clay with chert (medium, moist to very moist) (fill) CH 19.6 12 CH Reddish brown fat clay with chert (stiff, moist) 13 18 10 18.8 19  $\mathsf{CL}$ Brown lean clay with trace of chert (very stiff to hard, moist)

Boring terminated at approximately 19 feet below ground surface due to sampler and

Note: See Figure A-1 for explanation of symbols.

Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

## Log of Boring RW6-3



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/29/2022	<u>End</u> 3/29/2022	Total Depth (ft)	24.5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
	Elevation (ft) Datum		7.92 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Vertical Datum         NAVD88           Easting (X)         2198431.0           Northing (Y)         245884.96				System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 139+	-50.43, Offset 1	L14.3999 fee	et					

			1 1111	_D DATA									
Elevation (feet)	. Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample Sample Name Testing	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Water Content (%)	Liquid Limit (LL), %	Plastic Limit (PL), %	Platicity Index (PI), %	Fines Content (%)	REMARKS
- - - -	0-	15	12	1		AC GW CH	Asphalt concrete pavement (4 inches)  Gravel base (4 inches)  Reddish brown and gray fat clay with chert (stiff, moist) (fill)						
-	5 <del>-</del>	18	15	<u>2</u> MC		СН	Reddish brown fat clay with chert (very stiff, moist) (fill)	27.8					
- _&^	-	16	10	3 MC; SA; AL		CL		23.2	49	27	22	56	AASHTO (GI) A-7-6 (10)
- - -	10 —	<u>                                     </u>											
	15	°	8	4			- - -						
GEIS_GEOTECH_STAND	- - -	15	28	5		CH							
anydeoenkaineers, pr_srp_us_junk_2017.018,018,018.0500.000,010,010,010,010,010,010,010,010,0	20 —					GI	Grayish brown fat clay with limestone fragments (very stiff to hard, very moist)  — — — — —						
ieoengineers_dr_std	- -	o	50/1"	6									

below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

## Log of Boring RW6-4



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 3/30/2022	<u>End</u> 3/30/2022	Total Depth (ft)	22	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Vertical	Elevation (ft) Datum		5.43 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X	
Easting Northing			659.176 33.6254		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration	
Notes: I-24 STA 142+00.02, Offset 115.6719 feet										

			FIEL	D D	ATA				
ිරි <sub>රි</sub> Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	WATERIAL Content (%) Liquid (Hz), % Plastic (Hz), % Plastic (Mz) (Mz) (Mz) (Mz) (Mz) (Mz) (Mz) (Mz)	
_ <sub>6</sub>	0 —					٥٩	AC	Asphalt concrete pavement (3 inches)	
-	-	8 1	10		1		GW	Gravel base (10 inches)	
-	-	M					CH	Reddish brown fat clay with chert and wood pieces (stiff, moist) (fill)	
	_								
	-	10	11		2		CH	Reddish brown fat clay with chert (stiff, moist) – (fill)	
_&	5 <b>—</b>	$\square$						_ \''''	
	-								
T .	_							_	
ŀ	_								
-	_	13	15		<u>3</u> MC		CH	Reddish brown to gray fat clay with chert (very 17.4	
<b>-</b> ,		IXI I			MC			Reddish brown to gray fat clay with chert (very stiff, moist) (fill)	
_ <sub>66</sub> 6	10 —	<u> </u>							
-	_							- 1	
1	-								
1	-								
W N	-	10	14		4		CH	Grayish brown fat clay with chert (stiff, moist) (residuum)	
o o o	15 —	ΜП							
NDARE	_								
- STA	_							_	
SEO TEC	_								
- GEI8_		7 5	10		<u>5</u> MC		CL	Greenish gray lean clay with limestone fragments 18.9	
7.GLB,	_	X			MC	V/A		Greenish gray lean clay with limestone fragments (stiff, moist to very moist)	
F 2017.	20 —					V/A			
IRS_DF_STD_US_JUNE_2017.GLB/GEB_GEOTECH_STANDARD_NO_GW_NNL	-								
F_STD_	-			L		1//		Boring terminated at approximately 22 feet	
RS_D	below ground surface due to auger refusal								

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Drilled	<u>Start</u> 3/30/2022	<u>End</u> 3/30/2022	Total Depth (ft)	18.5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger	
Surface Vertical	Elevation (ft) Datum		7.86 VD88		Hammer Data		utomatic Hammer O (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X	
Easting Northing			327.269 29.2885		System Datum		Geographic NAD83 (feet)	Groundwate	er not observed at time of exploration	
Notes: I-24 STA 143+75.79, Offset 97.9774 feet										

FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (2 inches) Gravel base (11 inches) GW Reddish brown fat clay with chert (stiff, moist to very moist) (fill) СН  $\mathsf{CL}$ Gray silty lean clay (medium, moist) (fill) 12 28.3 16 CL Tan lean clay (stiff, moist) (residuum) 10 <u>6</u>16 0 50/0" 8.9 27 AASHTO (GI) A-2-4 (0) MC;  $\frac{4}{SA}$ ; AL GC Gray clayey limestone gravel with sand (very dense, moist) 15

Boring terminated at approximately 181/2 feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols.

Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

## Log of Boring RW6-6



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/1/2022	<u>End</u> 4/1/2022	Total Depth (ft)	31	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical I	Elevation (ft) Datum		5.97 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
Easting ( Northing			351.236 31.6236		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 154+	60.25, Offset 1	L10.8743 fee	et					

$\overline{}$			FIEI	LD D	ATA			
Elevation (feet)	o Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	MATERIAL Content (%) India (Pl.), % Plastic I
  -	- - -	4	8		1		GW CH	Asphalt concrete pavement (4 inches)  Gravel base (10 inches)  Reddish brown fat clay with trace of chert (stiff, moist) (fill)
- - 	5 <del>-</del>	12	10		2		CH	Reddish brown fat clay with chert (stiff, moist)  (fill)  -
- - - _&	10 —	10	9		3			
25 ANDARD 100 GW 100 L	- - 15 —	`8	9		4		CL	Dark gray and tan lean clay with chert (stiff, moist) (fill)
	20 —	18	12		<u>5</u> MC			
	- 25 — -	14	17		6		СН	Tan and gray fat clay with trace of chert (very stiff, moist) (fill)
No Co	30 —	18	10		MC; <del>Z</del> SA; AL		CL	Dark gray clay with sand and chert (stiff, moist to very moist) (residuum)  AASHTO (GI) A-6-5 (5)
No Co	ote: Se ordina	e Figure ites Data	A-1 fo Sour	r expla	anation o ordinates	f symb	ools. elevation	s provided by TDOT Region 2 Survey Office.

# Log of Boring RW7-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

$\bigcap$			FIEL	D D	ATA									
Elevation (feet)	S Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Water Content (%)	quid mit (LL)	Plastic Limit (PL), %	Platicity Index (PI), %	Fines Content (%)	REMARKS
_&	30 —						CL	Dark gray clay with sand and chert (stiff, moist to very moist) (residuum)						

Boring terminated at approximately 31 feet below ground surface due to auger refusal

## Log of Boring RW7-1 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/1/2022	<u>End</u> 4/1/2022	Total Depth (ft)	34.5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface I Vertical I	Elevation (ft) Datum		97.2 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2199921.272 Northing (Y) 245320.4926				System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-24 STA 155+	29.47, Offset 1	L03.3581 fee	et					

			FIE	LD D	ATA			
Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	Sample Name Testing	Graphic Log	Group Classification	MATERIAL Content (%) Limit (H.), % Plastic Limit (H.), % Index (Pl.), % Plastic Content (%) Limit (H.), % Plastic Content (%) Remark (Pl.), % Fines Content (%)
-	0-					٥٧	AC	Asphalt concrete pavement (7 inches)  Gravel base (8 inches)
_00/2	_	6	8		1		GW CH	Tan fat clay with chert (stiff, moist) (fill)
	-							_
-	-	8	11		2		CH	Reddish tan fat clay with chert (stiff, moist) (fill)
-	5 <b>—</b>							-
-	-	_						-
_690	-	-						
-	-	14	6		3			
-	-		0		3		CH	Reddish tan fat clay with trace of chert (medium, _ moist) (fill)
-	10 —							
- 6860								
_6°	_							
- NAL	_	18	12		4			Reddish tan fat clay with trace of chert (stiff,
NO_GN	15 —	Ш						moist) (fill)
ANDARD	-							
S ECH_SI	-	-						
18_GE01	-	L						<u>-</u>
.GLB/GE	-	10	7		<u>5</u> MC		CL	Tan lean clay with chert (medium, very moist) (fill)
E_2017	20 —							-
Nnr sn	-	-						-
PF_STD_US	-	-						<u> </u>
NEERS_	-	18	11		6		CL	Dark gray lean clay with trace of chert (stiff
SEOENG	OF -						OL.	Dark gray lean clay with trace of chert (stiff, moist) (residuum)
Library:(	25 -							
DBLibrary/	_							
I GPJ DE	_							
1700900	_	18	11		<u>7</u> MC		CL	Gray lean clay with chert (stiff, very moist) 16
1647009\GINT\Z464700900.GPJ DBLUbrany/LibraryGEOENGINETRS_DF_STD_US_JUNE_2017.GLB/GEB_GEOTECH_STANDARD_NO_GW_NNL	30 —	$\square$				$\mathbb{Z}$		
o No	ote: Se ordina	e Figure ates Data	A-1 fo Sour	r expl ce: Co	anation of ordinates	symles and e	ools. elevation	is provided by TDOT Region 2 Survey Office.

# Log of Boring RW7-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

			FIEL	D D	ATA								
Elevation (feet)	S Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification	MATERIAL DESCRIPTION	Water Content (%)	il d	Platicity Index (PI), %	Fines Content (%)	REMARKS
-	30 —						CL	Gray lean clay with chert (stiff, very moist)					
	-							- - -					
-	-	<b>×</b> 2	50/3"		8		CL	Tan lean clay with limestone fragments (hard, moist)	-				

Boring terminated at approximately 34½ feet below ground surface due to auger refusal

## Log of Boring RW7-2 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/4/2022	<u>End</u> 4/4/2022	Total Depth (ft)	48	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface I Vertical I	Elevation (ft) Datum		)3.6 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2210731.088 Northing (Y) 247660.3245				System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-75 STA 443+	62.20, Offset -	77.8689 feet						

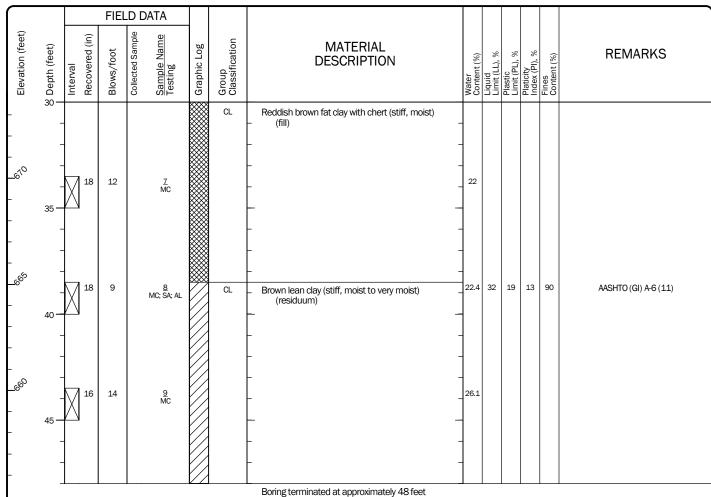
FIELD DATA Elevation (feet) Sample Name Testing Recovered (in) Collected Sample Group Classification **MATERIAL** Graphic Log Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval Gravel (3½ feet) *00*/2 8  $\mathsf{CL}$ Light brown lean clay with gravel and wood pieces (stiff, moist) (fill) 13 18 CH Reddish brown fat clay with chert (stiff, moist to very moist) (fill) 10 10 9 23 СН Reddish brown fat clay with chert (very stiff, 20 Gray silty lean clay with trace of chert and roots (stiff, moist) (fill) 12 12 CL 14.7 16 13 СН Reddish brown fat clay with chert (stiff, moist) (fill) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW8-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Boring terminated at approximately 48 feet below ground surface due to auger refusal

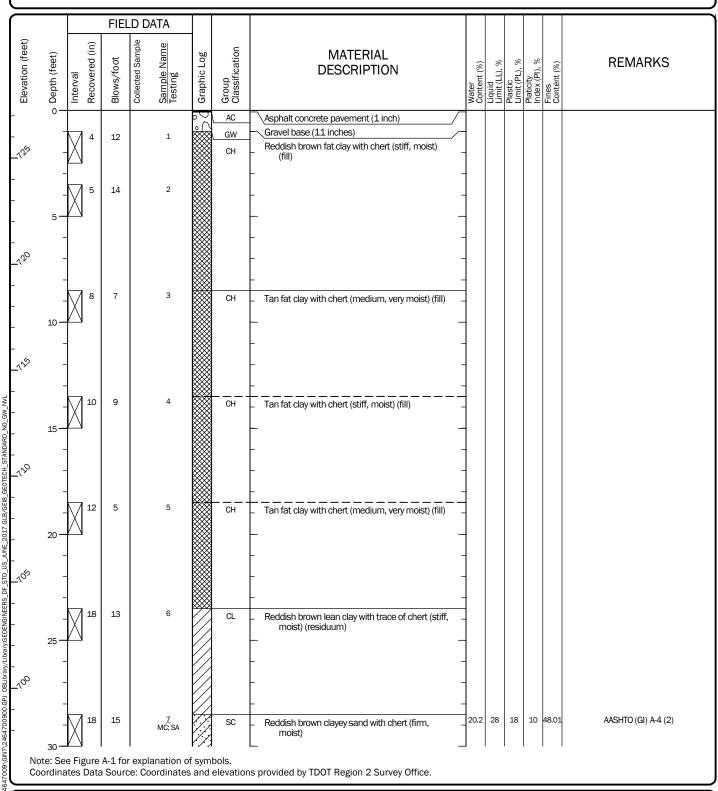
# Log of Boring RW8-1 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/7/2022	<u>End</u> 4/7/2022	Total Depth (ft)	50	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical I	Elevation (ft) Datum	. –	7.26 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2211854.689 Northing (Y) 247901.8534				System Datum		Geographic NAD83 (feet)	Groundwate	er not observed at time of exploration
Notes:	I-75 STA 455+	02.85, Offset 6	62.5913 feet						

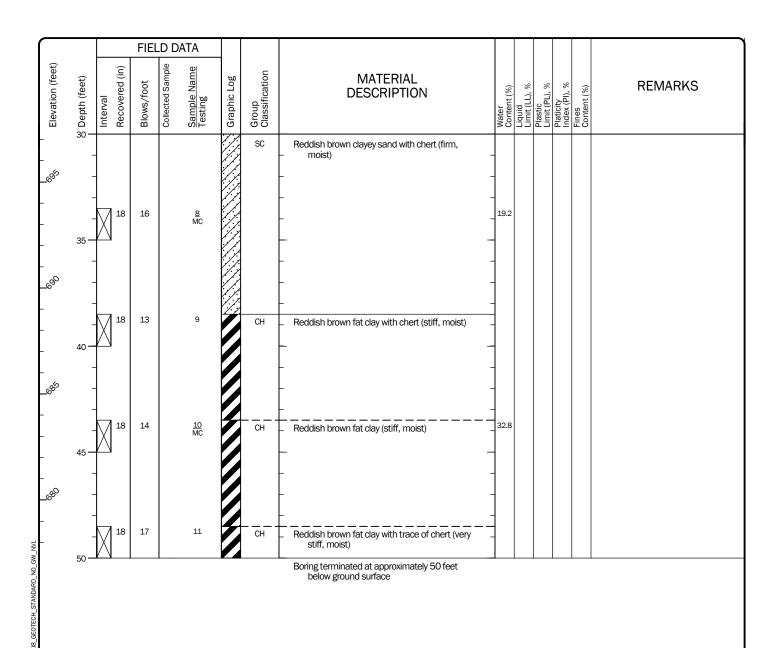


# Log of Boring RW10-1



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



# Log of Boring RW10-1 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/8/2022	<u>End</u> 4/8/2022	Total Depth (ft)	50	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface I Vertical I	Elevation (ft) Datum		7.81 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2211950.687 Northing (Y) 247935.5495				System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-75 STA 456+	04.59, Offset 6	62.2543 feet						

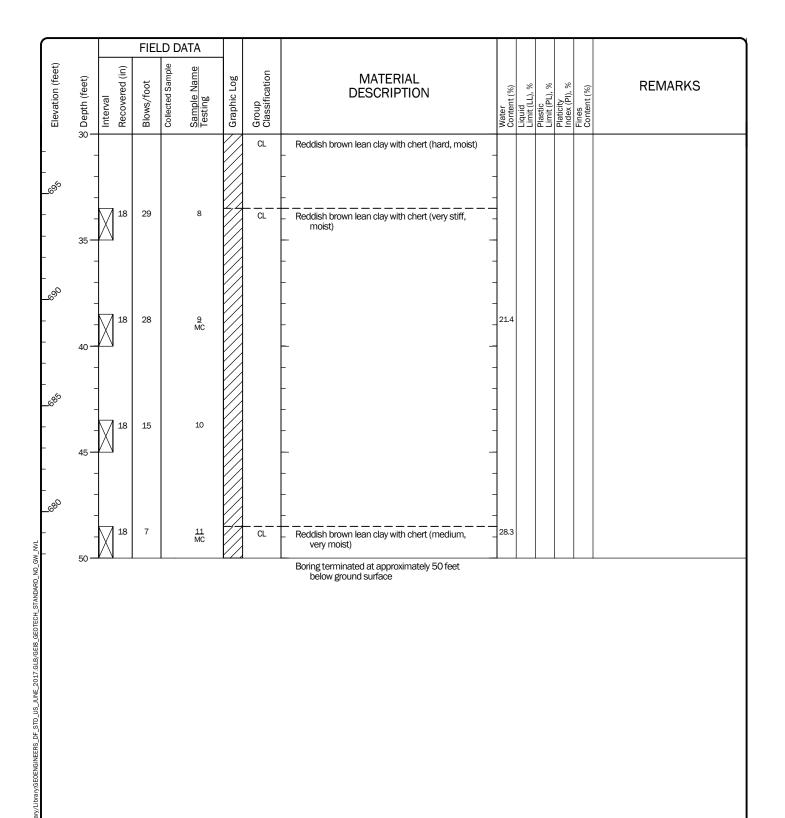
FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Depth (feet) Water Content (%) Liquid Limit (LL), % Plastic Limit (PL), % Platicity Index (PI), % **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (1 inch) Gravel base (8 inches) GW 1 10 16 Reddish brown fat clay with chert (very stiff, CH moist) (fill) 11 CH Reddish brown fat clay with chert (stiff, moist) 9 15.5 CL Tan lean clay with chert (stiff, very moist) (fill) 10 5  $\mathsf{CL}$ Tan lean clay with chert (medium, very moist) (fill) 10 Reddish brown fat clay with chert (stiff, moist) 20 Gray silty lean clay with trace of chert (stiff, moist) (residuum) 13 CL 14.9 16 50 CL Reddish brown lean clay with chert (hard, moist) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW10-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



## Log of Boring RW10-2 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/10/2022	<u>End</u> 4/10/2022	Total Depth (ft)	7.5	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		2.29 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2212418.7567 Northing (Y) 248107.3746				System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-75 STA 460+	99.45, Offset 6	2.7959 feet						

			FIEL	D D	ATA			
Elevation (feet)	Depth (feet)	Interval Recovered (in)	Blows/foot	Collected Sample	<u>Sample Name</u> Testing	Graphic Log	Group Classification	WATERIAL Content (%) Liquid Limit (PL), % Plastif (LL), % Plastif (PL), % Plas
-	0 —					70	AC	Asphalt concrete pavement (1 inch)
-		10	28		1		GW 	Gravel base (10 inches)  Orange to tan lean clay with chert (very stiff,
_130	_						CL	moist) (fill)
-	-		25		2			
-	_	XI I						
-	5 <b>—</b>							_
- 6	_							1
-15°	_					$\bowtie$		- 1
								Boring terminated at approximately 7½ feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.



## Log of Boring RW11-1

Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

Drilled	<u>Start</u> 4/10/2022	<u>End</u> 4/10/2022	Total Depth (ft)	17	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger		
Surface Vertical	Elevation (ft) Datum		2.21 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X		
Easting Northing			112.219 04.8755		System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration		
Notes: I-75 STA 460+92.57, Offset 62.5900 feet											

FIELD DATA Elevation (feet) Collected Sample Sample Name Testing Recovered (in) Group Classification **MATERIAL** Graphic Log o Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (1 inch) Gravel base (10 inches) GW Offset from boring RW11-1 about 10 feet Augering only, no SPT sampling south due to shallow refusal 20 16 CL Orange to tan lean clay with chert (very stiff, 10 120 15 15.9 18 СН Tan fat clay with chert (very stiff, moist) (fill)

Boring terminated at approximately 17 feet below ground surface due to auger refusal

Note: See Figure A-1 for explanation of symbols.

Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Drilled	<u>Start</u> 4/10/2022	<u>End</u> 4/10/2022	Total Depth (ft)	50	Logged By Checked By	HH RDH	Driller Tri-State Drilling LLC		Drilling Method Hollow-stem Auger
Surface Vertical	Elevation (ft) Datum		3.29 VD88		Hammer Data		utomatic Hammer 0 (lbs) / 30 (in) Drop	Drilling Equipment	CME 550X
	Easting (X) 2212608.141 Northing (Y) 248193.8873				System Datum		Geographic NAD83 (feet)	Groundwate	r not observed at time of exploration
Notes:	I-75 STA 463+	-04.36, Offset 6	61.4832 feet						

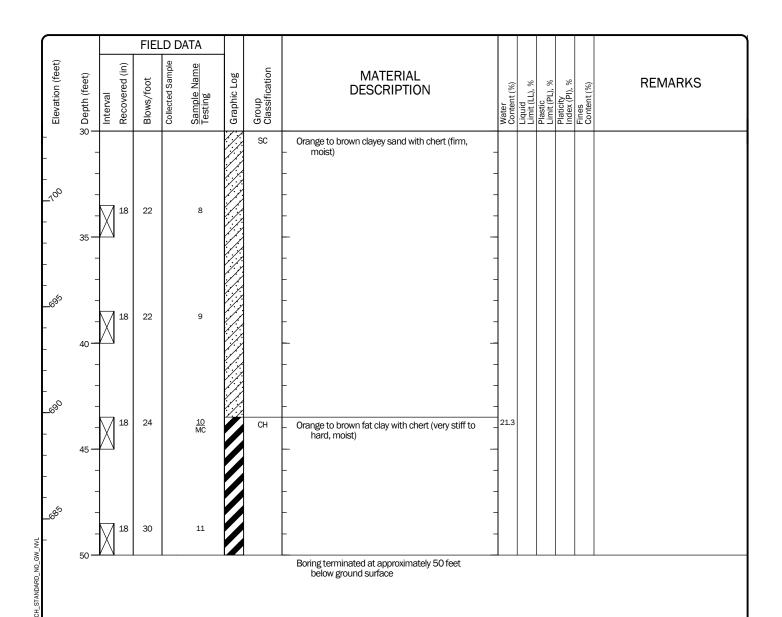
FIELD DATA Elevation (feet) Sample Name Testing Collected Sample Group Classification **MATERIAL** Graphic Log Depth (feet) Water
Content (%)
Liquid
Limit (LL), %
Plastic
Limit (PL), %
Platicity
Index (Pl), %
Fines
Content (%) **REMARKS** Blows/foot **DESCRIPTION** Interval AC Asphalt concrete pavement (2 inches) \Gravel base (6 inches) GW 29 Orange to tan lean clay with chert (very stiff, moist) (fill) CL <u>130</u> 16 10 17 Orange to brown clayey sand with chert (firm, moist) (residuum) 17.1 42 20 AASHTO (GI) A-7-6 (4) <u>5</u> MC; SA; AL 20 50 Orange to brown clayey sand with chert (dense, moist) 10 SC 25 18 28 SC Orange to brown clayey sand with chert (firm, moist) Note: See Figure A-1 for explanation of symbols. Coordinates Data Source: Coordinates and elevations provided by TDOT Region 2 Survey Office.

# Log of Boring RW11-2



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee



Log of Boring RW11-2 (continued)



Project: I-24/I-75 Interchange Improvements Phase II

Project Location: Chattanooga, Tennessee

**APPENDIX B**Laboratory Test Results



April 15, 2022

Project No. N2022-051-001

Emily Reed GeoEngineers, Inc. 5409 Maryland Way, Suite 150 Brentwood, TN 37027

# <u>Transmittal</u> <u>Laboratory Test Results</u> 24647-009-00, I-24/I-75 Interchange

Please find attached the laboratory test results for the above referenced project. The testing was performed in general accordance with the methods listed on the enclosed data sheets. The test results are believed to be representative of the samples that were submitted for testing and are indicative only of the specimens which were evaluated. We have no direct knowledge of the origin of the samples and imply no position regarding the nature of the test results, i.e., pass/fail and no claims as to the suitability of the material for its intended use. The client should evaluate the data and interpret design parameters based on their knowledge of the Project.

The test data and all associated project information provided shall be held in strict confidence and disclosed to other parties only with authorization by our Client. The test data submitted herein is considered integral with this report and is not to be reproduced except in whole and only with the authorization of the Client and Geotechnics. The remaining sample materials for this project will be retained for a minimum of 90 days as directed by the Geotechnics' Quality Program.

We are pleased to provide these testing services. Should you have any questions or if we may be of further assistance, please contact our office.

Respectfully submitted, *Geotechnics*, *Inc*.

Wm. Daniel Smith, P.E. Regional Manager

m. Daniel Smith

We understand that you have a choice in your laboratory services and we thank you for choosing Geotechnics.



ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	001	002	003	004	005
Boring No.:	RW1-1	RW1-1	RW1-2	RW1-2	RW1-2
Depth (ft):	3.5-5	8.5-10	8.5-10	13.5-15	28.5-30
Sample No.:	2	3	3	4	7
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	1	2	27	3	4
	223.03	220.77	581.14	211.13	213.18
	185.09	173.05	533.93	155.89	183.31
	8.36	8.31	202.79	8.34	8.35
	37.94	47.72	47.21	55.24	29.87
	176.73	164.74	331.14	147.55	174.96
Water Content (%)	21.5	29.0	14.3	37.4	17.1
Lab ID	006	007	008	009	010
Boring No.	RW1-2	RW1-3	RW1-3	RW1-3	RW1-3
Depth (ft)	38.5-40	8.5-10	18.5-20	29.5-30	33.5-35
Sample No.	9	3	5	7	8
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	5	6	7	8	9
	219.11	223.77	224.31	216.85	214.68
	193.57	182.09	188.61	176.47	177.05
	8.20	8.12	8.10	8.26	8.26
	25.54	41.68	35.70	40.38	37.63
	185.37	173.97	180.51	168.21	168.79
Water Content (%)	13.8	24.0	19.8	24.0	22.3

Tested By PM Date 4/13/22 Checked By WDS Date 4/15/22

page 1 of 1 DCN: CT-S1 DATE: 3/18/13 REVISION: 4



ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	011	012	013	014	015
Boring No.:	RW1-3	RW1-4	RW1-4	RW1-4	RW1-5
Depth (ft):	38.5-40	3.5-5	13.5-15	23.5-25	3.5-5
Sample No.:	9	2	4	6	2
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	10	11	29	12	13
	211.39	212.78	665.09	212.31	211.81
	173.71	156.41	579.12	168.35	167.07
	8.22	8.25	203.08	8.23	8.26
	37.68	56.37	85.97	43.96	44.74
	165.49	148.16	376.04	160.12	158.81
Water Content (%)	22.8	38.0	22.9	27.5	28.2
Lab ID	016	017	018	019	020
Boring No.	RW1-5	RW1-5	RW1-5	RW1-5	RW1-6
Depth (ft)	13.5-15	18.5-20	28.5-30	38.5-40	8.5-10
Sample No.	4	5	7	9	3
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	14	15	16	17	18
	216.85	150.53	216.94	226.35	215.10
	167.47	113.82	166.61	183.16	182.89
	8.29	8.26	8.25	8.25	8.23
	49.38	36.71	50.33	43.19	32.21
	159.18	105.56	158.36	174.91	174.66
Water Content (%)	31.0	34.8	31.8	24.7	18.4

Notes:

Tested Bv	PM	Date	4/13/22	Checked By	WDS	Date	4/15/22	

page 1 of 1 DCN: CT-S1 DATE: 3/18/13 REVISION: 4



ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	021	022	023	024	025
Boring No.:	RW1-6	RW1-6	RW1-6	RW1-6	RW1-6
Depth (ft):	18.5-20	23.5-25	28.5-30	38.5-40	43.5-45
Sample No.:	5	6	7	9	10
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	48	19	1	2	3
	1054.13	231.38	360.52	352.85	371.72
	905.08	195.09	317.65	324.92	334.91
	200.91	8.24	143.10	144.34	142.20
	149.05	36.29	42.87	27.93	36.81
	704.17	186.85	174.55	180.58	192.71
Water Content (%)	21.2	19.4	24.6	15.5	19.1
Lab ID	026	027	028	029	030
Boring No.	RW3-1	RW3-1	RW3-2	RW3-2	RW3-2
Depth (ft)	8.5-10	18.5-20	8.5-10	13.5-15	18.5-20
Sample No.	3	5	3	4	5
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	4	5	6	55	7
	357.93	367.00	361.20	756.43	356.00
	314.72	321.09	327.52	632.35	312.60
	143.16	142.39	143.33	201.26	142.86
	43.21	45.91	33.68	124.08	43.40
	171.56	178.70	184.19	431.09	169.74
Water Content (%)	25.2	25.7	18.3	28.8	25.6

Tested B	v PM	Date	4/13/22	Checked By	WDS	Date	4/15/22	
, 00t0a <u>D</u>	,	Date	., . o,	onconta by		Date	.,,	



ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	031	032	033	034	035
Boring No.:	RW3-3	RW3-3	RW4-1	RW4-1	RW4-1
Depth (ft):	3.5-5	18.5-20	13.5-15	23.5-25	33.5-35
Sample No.:	2	5	4	6	8
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	8	9	10	11	1
	361.44	357.14	351.75	365.86	214.16
	323.05	322.73	320.22	317.81	161.73
	141.38	142.57	142.85	141.07	8.36
	38.39	34.41	31.53	48.05	52.43
	181.67	180.16	177.37	176.74	153.37
Water Content (%)	21.1	19.1	17.8	27.2	34.2
Lab ID	036	037	038	039	040
Boring No.	RW4-1	RW4-2	RW4-2	RW4-2	RW4-2
Depth (ft)	38.5-40	8.5-10	18.5-20	23.5-25	28.5-30
Sample No.	9	3	5	6	7
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	2	3	4	31	5
	213.17	224.41	212.34	1095.29	234.68
	158.49	186.81	171.88	924.32	190.19
	8.32	8.34	8.37	201.88	8.19
	54.68	37.60	40.46	170.97	44.49
	150.17	178.47	163.51	722.44	182.00
Water Content (%)	36.4	21.1	24.7	23.7	24.4

Tested By PM Date 4/13/22 Checked By WDS Date 4/15/22

page 1 of 1 DCN: CT-S1 DATE: 3/18/13 REVISION: 4



ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	041	042	043	044	045
Boring No.:	RW4-2	RW4-3	RW4-3	RW4-3	RW4-4
Depth (ft):	33.5-35	8.5-10	18.5-20	23.5-25	8.5-10
Sample No.:	8	3	5	6	3
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	6	7	26	8	9
	224.51	228.99	927.02	221.08	228.28
	154.95	185.61	813.85	180.40	194.87
	8.13	8.11	198.55	8.30	8.31
	69.56	43.38	113.17	40.68	33.41
	146.82	177.50	615.30	172.10	186.56
Water Content (%)	47.4	24.4	18.4	23.6	17.9
Lab ID	046	047	048	049	050
Boring No.	RW4-4	RW4-4	RW4-4	RW5-1	RW5-1
Depth (ft)	18.5-20	33.5-35	38.5-40	8.5-10	18.5-20
Sample No.	5	8	9	3	5
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	10	11	12	13	14
	214.45	237.31	215.26	222.31	246.62
	170.24	175.46	169.28	182.69	210.46
	8.26	8.26	8.24	8.26	8.28
	44.21	61.85	45.98	39.62	36.16
	161.98	167.20	161.04	174.43	202.18
Water Content (%)	27.3	37.0	28.6	22.7	17.9

Teste	d Bv	PM	Date	4/14/22	Checked Bv	WDS	Date	4/15/22
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ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	051	052	053	054	055
Boring No.:	RW5-1	RW5-1	RW5-1	RW5-2	RW5-2
Depth (ft):	23.5-25	33.5-35	38.5-40	3.5-5	8.5-10
Sample No.:	6	8	9	2	3
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	15	16	17	18	Z18
	210.40	213.24	245.14	230.33	756.47
	164.80	168.60	184.62	183.74	635.97
	8.30	8.30	8.31	8.26	200.56
	45.60	44.64	60.52	46.59	120.50
	156.50	160.30	176.31	175.48	435.41
Water Content (%)	29.1	27.8	34.3	26.6	27.7
Lab ID	056	057	058	059	060
Boring No.	RW5-2	RW5-2	RW5-2	RW5-2	RW5-2
Depth (ft)	18.5-20	23.5-25	33.5-35	43.5-45	48.5-50
Sample No.	5	6	8	10	11
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	19	1	2	3	4
	228.89	353.25	363.64	409.21	241.48
	174.13	304.65	307.61	333.06	205.06
	8.26	143.12	144.37	142.20	143.16
	54.76	48.60	56.03	76.15	36.42
	165.87	161.53	163.24	190.86	61.90
Water Content (%)	33.0	30.1	34.3	39.9	58.8

Tested By PM Date 4/14/22 Checked By WDS Date 4/15/22



ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID:	061	062	063	064	065
Boring No.:	RW6-2	RW6-3	RW6-3	RW6-4	RW6-4
Depth (ft):	1-2.5	3.5-5	13.5-15	3.5-5	8.5-10
Sample No.:	1	2	4	2	3
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	51	5	6	7	Z10
	623.33	383.08	368.97	388.43	687.11
	527.31	343.60	333.32	335.05	595.22
	198.71	142.39	143.33	142.87	199.79
	96.02	39.48	35.65	53.38	91.89
	328.60	201.21	189.99	192.18	395.43
Water Content (%)	29.2	19.6	18.8	27.8	23.2
Lab ID	066	067	068	069	070
Boring No.	RW6-5	RW6-5	RW6-6	RW6-6	RW7-1
Depth (ft)	8.5-10	18.5-20	8.5-10	13.5-14.9	18.5-20
Sample No.	3	5	3	4	5
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	8	9	10	1569	11
	385.34	352.86	367.82	862.84	364.08
	349.27	319.41	318.21	817.33	332.95
	141.43	142.58	142.86	306.70	141.09
	36.07	33.45	49.61	45.51	31.13
	207.84	176.83	175.35	510.63	191.86
Water Content (%)	17.4	18.9	28.3	8.9	16.2

Tested	l By	PM	Date	4/14/22	Checked By	WDS	Date	4/15/22
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ASTM D 2216-19

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00 I-24/I-75 Interchange

Project No.: N-2022-051-001

Lab ID: Boring No.: Depth (ft): Sample No.:	071	072	073
	RW7-1	RW7-2	RW7-2
	28.5-30	18.5-20	28.5-30
	10	5	7
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	585	12	13
	1064.11	380.47	371.25
	950.94	344.95	339.90
	308.64	141.01	144.09
	113.17	35.52	31.35
	642.30	203.94	195.81
Water Content (%)	17.6	17.4	16.0

Notes:

Tested By PM Date 4/14/22 Checked By WDS Date 4/15/22



### ATTERBERG LIMITS

ASTM D 4318-17

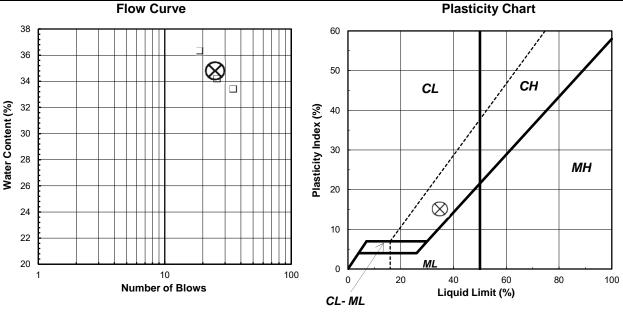
Client: GeoEngineers, Inc. Boring No.: RW1-2 Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 8.5-10 Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-003 Soil Description: ORANGISH BROWN LEAN CLAY **Note:** The USCS symbol used with this test refers only to the minus **No. 40** (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture		Liquid Limit Test				
ASTM D2216-19		1	2	3	M	
Tare Number:	27	С	U	E	U	
Wt. of Tare & Wet Sample (g):	581.14	32.46	33.74	32.93	L	
Wt. of Tare & Dry Sample (g):	533.93	30.24	31.18	30.41	Т	
Weight of Tare (g):	202.79	23.59	23.69	23.47	I	
Weight of Water (g):	47.2	2.2	2.6	2.5	Р	
Weight of Dry Sample (g):	331.1	6.7	7.5	6.9	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%):	14.3	33.4	34.2	36.3	N	
Number of Blows:		35	26	19	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	G	Т		Liquid Limit (%):	35
Wt. of Tare & Wet Sample (g):	34.33	32.07			
Wt. of Tare & Dry Sample (g):	32.57	30.67		Plastic Limit (%):	20
Weight of Tare (g):	23.58	23.54			
Weight of Water (g):	1.8	1.4		Plasticity Index (%):	15
Weight of Dry Sample (g):	9.0	7.1			
				USCS Symbol:	CL
Moisture Content (%):	19.6	19.6	-0.1		
Note: The acceptable range of the	e two Moistu	re Conten	ts is $\pm$ 1.12		



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Date

Tested By

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4/15/22

Date

Checked By

NC

4/12/22



### SIEVE AND HYDROMETER ANALYSIS

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-2 Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 8.5-10 Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-003 Soil Color: Orangish Brown

	SIEVE ANALYSIS HYDROMETER							
USCS	cobbles	gravel	sand	silt and clay fraction				
AASHTO	cobbles	gravel	sand	silt and clay fraction				
100	12" 6"	3" 3/4" 3/8" #4	#10 #20 #40 #1p0 #2	00				
90		H N						
80								
70		<del>                                     </del>						
Weight								
Percent Finer By Weight								
Percent								
30								
10								

Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	46.18		
100	100.00	Gravel	27.58	Sand	33.26	Gravel	27.58
2	53.82	Sand	51.85	Coarse Sand	19.01	Sand	51.85
0.075	20.56	Silt&Clay	20.56	Fine Sand	14.25	Silt	6.83
0.05	19.01			Silt & Clay	20.56	Clay	13.73
0.005	13.73			Silt	8.62	•	
0.002	11.94			Clay	11.94		
AASHTO (	GI):		JSCS Symbo	ol:	•	D50 =	1.50

Particle Diameter (mm)

AASHTO (GI): USCS Symbol: A - 2 - 6 (0) SC, TESTED

USCS Classification
CLAYEY SAND WITH GRAVEL

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### **WASH SIEVE ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-2
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 8.5-10
Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-003 Soil Color: Orangish Brown

Moisture Content of Passing 3/4" Material		Moisture Content of Retained 3/4" Material	
Tara Na .	27	Tara Na .	NI A
Tare No.:	27	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	417.08	Weight of Tare & Wet Sample (g):	NA
Wt. of Tare & Dry Sample (g):	417.08	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	202.79	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	214.29	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	214.29
Dry Weight of - 3/4" Sample (g):	214.29	Weight of minus #200 Material (g):	44.06
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	170.23
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	214.29		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	3.98		1.86	1.86	98.14	98.14
3/8"	9.50	11.83		5.52	7.38	92.62	92.62
#4	4.75	43.30		20.21	27.58	72.42	72.42
#10	2.00	39.85		18.60	46.18	53.82	53.82
#20	0.85	24.44	( ** )	11.41	57.59	42.41	42.41
#40	0.425	16.29		7.60	65.19	34.81	34.81
#60	0.250	12.75		5.95	71.14	28.86	28.86
#140	0.106	14.53		6.78	77.92	22.08	22.08
#200	0.075	3.26		1.52	79.44	20.56	20.56
Pan	-	44.06		20.56	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

_	Tested By	JV	Date	4/14/22	Checked By	NC	Date	4/15/22	



### **HYDROMETER ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-2
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 8.5-10
Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-003 Soil Color: Orangish Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction C	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	23.25	23.9	5.8	17.4	84.2	0.01284	0.0321	17.3
5	22.50	23.9	5.8	16.7	80.5	0.01284	0.0204	16.6
15	22.00	24.0	5.8	16.2	78.3	0.01282	0.0118	16.1
30	21.25	24.0	5.8	15.5	74.6	0.01282	0.0084	15.3
60	20.00	24.0	5.8	14.2	68.6	0.01282	0.0060	14.1
250	18.50	24.0	5.8	12.7	61.3	0.01282	0.0030	12.6
1440	17.00	24.0	5.8	11.2	54.1	0.01282	0.0012	11.1

Soil Specimen Data		Other Corrections	
Tare No.	13		
Wt. of Tare & Dry Material (g):	325.21	a - Factor	0.993
Weight of Tare (g):	299.65		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	20.56
Weight of Dry Material (g):	20.56		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

LL = 35

PL = 20

PI = 15

Tested By JV Date 4/12/22 Checked By NC Date 4/15/22

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### ATTERBERG LIMITS

ASTM D 4318-17

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW1-4

 Client Reference:
 24647-009-00, I-24/I-75 Interchange
 Depth (ft):
 13.5-15

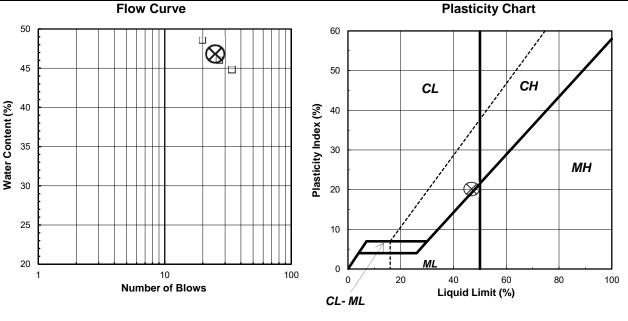
 Project No.:
 N2022-051-001
 Sample No.:
 4

Lab ID: N2022-051-001-013 Soil Description: YELLOWISH BROWN LEAN CLAY **Note:** The USCS symbol used with this test refers only to the minus **No. 40** (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	As Received Moisture Content			Liquid Limit Test				
ASTM D2216-19	1	2	3	M				
Tare Number:	29	Q	0	R	U			
Wt. of Tare & Wet Sample (g):	665.09	32.22	33.96	34.10	L			
Wt. of Tare & Dry Sample (g):	579.12	29.56	30.61	30.61	Т			
Weight of Tare (g):	203.08	23.62	23.33	23.42	I			
Weight of Water (g):	86.0	2.7	3.4	3.5	Р			
Weight of Dry Sample (g):	376.0	5.9	7.3	7.2	0			
Was As Received MC Preserved:	Yes				I			
Moisture Content (%):	22.9	44.8	46.0	48.5	N			
Number of Blows:		34	27	20	Т			

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	Α	F		Liquid Limit (%):	47
Wt. of Tare & Wet Sample (g):	35.20	33.15		Liquid Lillin (70).	7,
Wt. of Tare & Dry Sample (g):	32.74	31.16		Plastic Limit (%):	27
Weight of Tare (g):	23.59	23.71			
Weight of Water (g):	2.5	2.0		Plasticity Index (%):	20
Weight of Dry Sample (g):	9.2	7.5			
				USCS Symbol:	CL
Moisture Content (%):	26.9	26.7	0.2		
Note: The acceptable range of the	e two Moistu	re Conten	ts <i>i</i> s ± 1.12		



page 1 of 1 DCN: CTS4B, REV. 8, 5/22/18

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Date

NC

Checked By

4/12/22



ASTM D 422-63 (2007), AASHTO T88

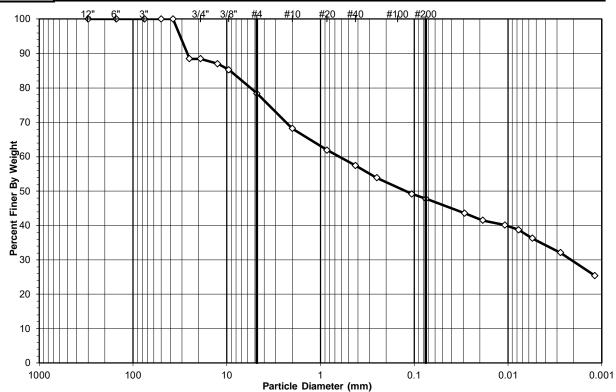
 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW1-4

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 13.5-15

 Project No.:
 N2022-051-001
 Sample No.:
 4

Lab ID: N2022-051-001-013 Soil Color: Yellowish Brown

		SIEVE	HYDROMETER	
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	31.80		
100	100.00	Gravel	21.65	Sand	20.46	Gravel	21.65
2	68.20	Sand	30.62	Coarse Sand	10.79	Sand	30.62
0.075	47.74	Silt&Clay	47.74	Fine Sand	9.67	Silt	12.05
0.05	45.96			Silt & Clay	47.74	Clay	35.69
0.005	35.69			Silt	18.19		
0.002	29.55			Clay	29.55		
AASHTO (	GI):	<u> </u>	JSCS Symbo	<u>l:</u>		D50 =	0.12

AASHTO (GI): USCS Symbo
A - 7 - 6 (6) SC, TESTED

USCS Classification

CLAYEY SAND WITH GRAVEL

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ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-4
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 13.5-15
Project No.: N2022-051-001 Sample No.: 4

Lab ID: N2022-051-001-013 Soil Color: Yellowish Brown

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material				
Tare No.:	29	Tare No.:	NA			
Wt. of Tare & Wet Sample (g):	476.24	Weight of Tare & Wet Sample (g):	NA NA			
Wt. of Tare & Dry Sample (g):	476.24	Weight of Tare & Dry Sample (g):	NA			
Weight of Tare (g):	203.08	Weight of Tare (g):	NA			
Weight of Water (g):	0.00	Weight of Water (g):	NA			
Weight of Dry Soil (g):	273.16	Weight of Dry Soil (g):	NA			
Moisture Content (%):	0.0	Moisture Content (%):	0.0			

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	273.16
Dry Weight of - 3/4" Sample (g):	241.68	Weight of minus #200 Material (g):	130.40
Wet Weight of +3/4" Sample (g):	31.48	Weight of plus #200 Material (g):	142.76
Dry Weight of +3/4" Sample (g):	31.48		
Total Dry Weight of Sample (g):	273.16		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	31.48		11.52	11.52	88.48	88.48
3/4"	19.0	0.00		0.00	11.52	88.48	88.48
1/2"	12.5	3.89		1.42	12.95	87.05	87.05
3/8"	9.50	4.87		1.78	14.73	85.27	85.27
#4	4.75	18.89		6.92	21.65	78.35	78.35
#10	2.00	27.74		10.16	31.80	68.20	68.20
#20	0.85	17.18	( ** )	6.29	38.09	61.91	61.91
#40	0.425	12.29		4.50	42.59	57.41	57.41
#60	0.250	9.72		3.56	46.15	53.85	53.85
#140	0.106	12.79		4.68	50.83	49.17	49.17
#200	0.075	3.91		1.43	52.26	47.74	47.74
Pan	-	130.40		47.74	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

_	Tested By	JV	Date	4/14/22	Checked By	NC	Date	4/15/22	



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-4
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 13.5-15

Project No.: N2022-051-001 Sample No.: 4

Lab ID: N2022-051-001-013 Soil Color: Yellowish Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	37.00	23.9	5.8	31.2	91.3	0.01284	0.0290	43.6
5	35.50	23.9	5.8	29.7	86.9	0.01284	0.0186	41.5
15	34.50	24.0	5.8	28.7	84.0	0.01282	0.0108	40.1
30	33.50	24.0	5.8	27.7	81.1	0.01282	0.0077	38.7
60	31.75	24.0	5.8	26.0	76.0	0.01282	0.0055	36.3
250	28.75	24.0	5.8	23.0	67.2	0.01282	0.0028	32.1
1440	24.00	24.0	5.8	18.2	53.3	0.01282	0.0012	25.4

Soil Specimen Data		Other Corrections	
Tare No.	14		
Wt. of Tare & Dry Material (g):	339.09	a - Factor	0.993
Weight of Tare (g):	300.18		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	47.74
Weight of Dry Material (g):	33.91		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

II = 47

PL = 27

PI = 20

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22
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### ATTERBERG LIMITS

ASTM D 4318-17

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW1-6

 Client Reference:
 24647-009-00, I-24/I-75 Interchange
 Depth (ft):
 18.5-20

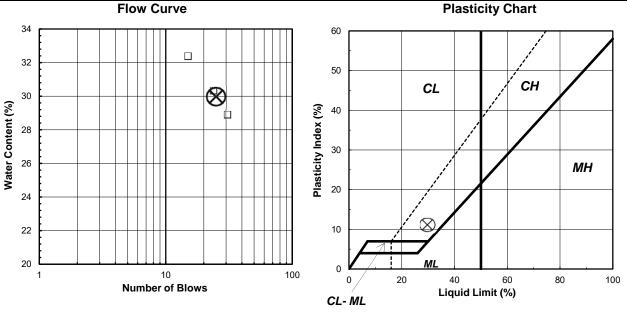
 Project No.:
 N2022-051-001
 Sample No.:
 5

Lab ID: N2022-051-001-021 Soil Description: BROWNISH YELLOW LEAN CLAY **Note:** The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	As Received Moisture Content			Liquid Limit Test				
ASTM D2216-19	1	2	3	M				
Tare Number:	48	W	Н	Р	U			
Wt. of Tare & Wet Sample (g):	1054.13	32.23	32.67	32.76	L			
Wt. of Tare & Dry Sample (g):	905.08	30.31	30.51	30.55	Т			
Weight of Tare (g):	200.91	23.66	23.38	23.72	I			
Weight of Water (g):	149.1	1.9	2.2	2.2	Р			
Weight of Dry Sample (g):	704.2	6.7	7.1	6.8	0			
Was As Received MC Preserved:	Yes				I			
Moisture Content (%):	21.2	28.9	30.3	32.4	N			
Number of Blows:		31	24	15	Т			

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	J	V		Liquid Limit (%):	30
Wt. of Tare & Wet Sample (g):	37.06	35.87			
Wt. of Tare & Dry Sample (g):	34.89	33.88		Plastic Limit (%):	19
Weight of Tare (g):	23.53	23.53			
Weight of Water (g):	2.2	2.0		Plasticity Index (%):	11
Weight of Dry Sample (g):	11.4	10.4			
				USCS Symbol:	CL
Moisture Content (%):	19.1	19.2	-0.1		
Note: The acceptable range of the	e two Moistu	re Conten	ts is ± 1.12		



Tested By JV Date 4/12/22 Checked By NC Date 4/15/22



ASTM D 422-63 (2007), AASHTO T88

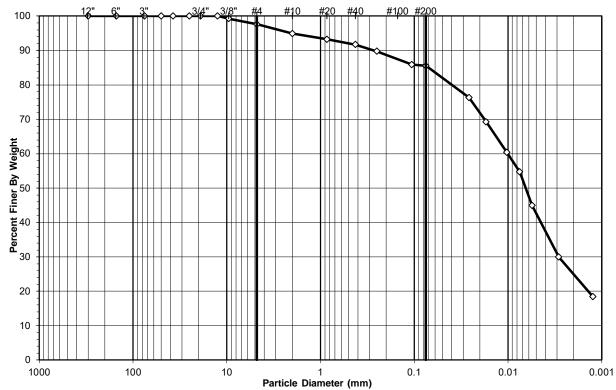
 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW1-6

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 18.5-20

 Project No.:
 N2022-051-001
 Sample No.:
 5

Lab ID: N2022-051-001-021 Soil Color: Brownish Yellow

		SIEVE	HYDROMETER		
USCS	cobbles	gravel	sand	silt and clay fraction	
AASHTO	cobbles	gravel	sand	silt and clay fraction	



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	5.07		
100	100.00	Gravel	2.35	Sand	9.38	Gravel	2.35
2	94.93	Sand	12.10	Coarse Sand	3.21	Sand	12.10
0.075	85.55	Silt&Clay	85.55	Fine Sand	6.17	Silt	42.91
0.05	82.02			Silt & Clay	85.55	Clay	42.65
0.005	42.65			Silt	60.59		
0.002	24.96			Clay	24.96		

AASHTO (GI): A - 6 (8) USCS Symbol: CL, TESTED

USCS Classification

LEAN CLAY

page 1 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-6
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 18.5-20

Project No.: N2022-051-001 Sample No.: 5

Lab ID: N2022-051-001-021 Soil Color: Brownish Yellow

Moisture Content (%):	0.0	Moisture Content (%):	0.0
Weight of Dry Soil (g):	426.64	Weight of Dry Soil (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Tare (g):	200.91	Weight of Tare (g):	NA
Wt. of Tare & Dry Sample (g):	627.55	Weight of Tare & Dry Sample (g):	NA
Wt. of Tare & Wet Sample (g):	627.55	Weight of Tare & Wet Sample (g):	NA
Tare No.:	48	Tare No.:	NA
Moisture Content of Passing 3/4" I	Material Moisture Content of Retained 3/4" Material		

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	426.64
Dry Weight of - 3/4" Sample (g):	426.64	Weight of minus #200 Material (g):	365.01
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	61.63
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	426.64		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	0.00		0.00	0.00	100.00	100.00
3/8"	9.50	3.21		0.75	0.75	99.25	99.25
#4	4.75	6.81		1.60	2.35	97.65	97.65
#10	2.00	11.60		2.72	5.07	94.93	94.93
#20	0.85	7.23	( ** )	1.69	6.76	93.24	93.24
#40	0.425	6.46		1.51	8.28	91.72	91.72
#60	0.250	8.37		1.96	10.24	89.76	89.76
#140	0.106	16.48		3.86	14.10	85.90	85.90
#200	0.075	1.47		0.34	14.45	85.55	85.55
Pan	-	365.01	•	85.55	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW1-6
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 18.5-20

Project No.: N2022-051-001 Sample No.: 5

Lab ID: N2022-051-001-021 Soil Color: Brownish Yellow

Elapsed	R	Temp.	Composite	R	N	_ K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	49.00	24.0	5.8	43.2	89.2	0.01282	0.0261	76.3
5	45.00	24.0	5.8	39.2	81.0	0.01282	0.0171	69.3
15	40.00	24.0	5.8	34.2	70.6	0.01282	0.0103	60.4
30	36.75	24.0	5.8	31.0	63.9	0.01282	0.0075	54.7
60	31.25	24.0	5.8	25.5	52.6	0.01282	0.0055	45.0
250	22.75	24.0	5.8	17.0	35.0	0.01282	0.0029	30.0
1440	16.25	24.0	5.8	10.5	21.6	0.01282	0.0012	18.5

Soil Specimen Data		Other Corrections	
Tare No.	15		
Wt. of Tare & Dry Material (g):	352.15	a - Factor	0.993
Weight of Tare (g):	299.07		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	85.55
Weight of Dry Material (g):	48.08		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

# **Atterberg Limits Test Results:**

LL = 30 PL = 19 PI = 11

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22
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(Minus No. 40 sieve material, Air dried)

### ATTERBERG LIMITS

ASTM D 4318-17

Client: Boring No.: RW3-2 GeoEngineers, Inc. Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 13.5-15

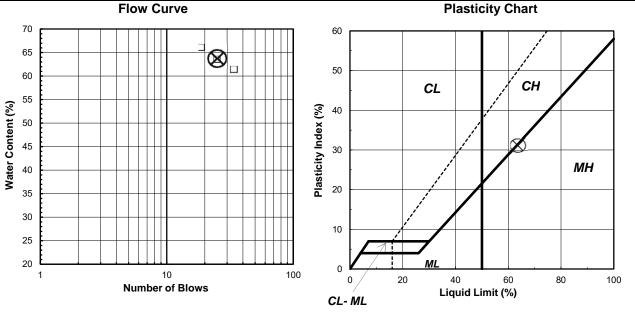
Project No.: N2022-051-001 Sample No.: 4

Lab ID: N2022-051-001-029 Soil Description: BROWN ELASTIC SILT Note: The USCS symbol used with this test refers only to the minus No. 40

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture		Liquid Limit Test				
ASTM D2216-19		1	2	3	M	
Tare Number:	55	М	N	K	U	
Wt. of Tare & Wet Sample (g):	756.43	33.04	32.39	32.14	L	
Wt. of Tare & Dry Sample (g):	632.35	29.48	28.86	28.76	Т	
Weight of Tare (g):	201.26	23.68	23.30	23.64	I	
Weight of Water (g):	124.1	3.6	3.5	3.4	Р	
Weight of Dry Sample (g):	431.1	5.8	5.6	5.1	0	
Was As Received MC Preserved:	Yes				1	
Moisture Content (%):	28.8	61.4	63.5	66.0	N	
Number of Blows:		34	25	19	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	X	ı		Liquid Limit (%):	64
Wt. of Tare & Wet Sample (g):	33.65	32.62		Liquid Ellille (70).	04
Wt. of Tare & Dry Sample (g):	31.12	30.36		Plastic Limit (%):	33
Weight of Tare (g):	23.45	23.57			
Weight of Water (g):	2.5	2.3		Plasticity Index (%):	31
Weight of Dry Sample (g):	7.7	6.8			
				USCS Symbol:	MH
Moisture Content (%):	33.0	33.3	-0.3		
Note: The acceptable range of the	e two Moistu	re Conten	ts is ± 0.84		



DCN: CTS4B, REV. 8, 5/22/18

JV

Date

Tested By

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4/15/22

Date

Checked By

NC

4/12/22



ASTM D 422-63 (2007), AASHTO T88

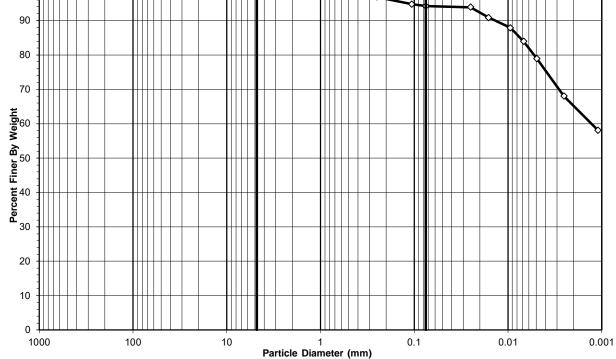
 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW3-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 13.5-15

 Project No.:
 N2022-051-001
 Sample No.:
 4

 Lab ID:
 N2022-051-001-029
 Soil Color:
 Brown

		SIEVE AI	HYDROMETER	
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
100 1	12" 6" (	3" > 3/4" > 3/8" #4	#10 #20 #40 #100 #2	200 
90				
-				
80				



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	0.60		
100	100.00	Gravel	0.08	Sand	5.19	Gravel	0.08
2	99.40	Sand	5.71	Coarse Sand	1.46	Sand	5.71
0.075	94.21	Silt&Clay	94.21	Fine Sand	3.73	Silt	15.03
0.05	94.08			Silt & Clay	94.21	Clay	79.18
0.005	79.18			Silt	29.01		
0.002	65.20			Clay	65.20		

AASHTO (GI): A - 7 - 5 (36) USCS Symbol: MH, TESTED

USCS Classification ELASTIC SILT

page 1 of 3  $\,$  DCN: CT-S3X  $\,$  DATE: 4/30/18  $\,$  REVISION: 8  $\,$ 

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ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW3-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 13.5-15

 Project No.:
 N2022-051-001
 Sample No.:
 4

 Lab ID:
 N2022-051-001-029
 Soil Color:
 Brown

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material	
Tare No.:	55	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	503.85	Weight of Tare & Wet Sample (g):	NA NA
Wt. of Tare & Dry Sample (g):	503.85	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	201.26	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	302.59	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g): NA Weight of the Dry Sample (g): 302.59 Dry Weight of - 3/4" Sample (g): 302.59 Weight of minus #200 Material (g): 285.07 Wet Weight of +3/4" Sample (g): 0.00 Weight of plus #200 Material (g): 17.52 Dry Weight of +3/4" Sample (g): 0.00 Total Dry Weight of Sample (g): 302.59

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	0.00		0.00	0.00	100.00	100.00
3/8"	9.50	0.00		0.00	0.00	100.00	100.00
#4	4.75	0.24		0.08	0.08	99.92	99.92
#10	2.00	1.58		0.52	0.60	99.40	99.40
#20	0.85	1.68	( ** )	0.56	1.16	98.84	98.84
#40	0.425	2.73		0.90	2.06	97.94	97.94
#60	0.250	3.35		1.11	3.17	96.83	96.83
#140	0.106	6.22		2.06	5.22	94.78	94.78
#200	0.075	1.72		0.57	5.79	94.21	94.21
Pan	-	285.07		94.21	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

Tested By JV Date 4/14/22 Checked By NC Date 4/15/22

 $page \ 2 \ of \ 3 \quad \ \ \text{DCN: CT-S3TW DATE: 8/19/19} \quad \text{REVISION: 0}$ 



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW3-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 13.5-15

 Project No.:
 N2022-051-001
 Sample No.:
 4

 Lab ID:
 N2022-051-001-029
 Soil Color:
 Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	53.00	24.0	5.8	47.2	99.6	0.01282	0.0250	93.9
5	51.50	24.0	5.8	45.7	96.5	0.01282	0.0161	90.9
15	50.00	24.0	5.8	44.2	93.3	0.01282	0.0094	87.9
30	48.00	24.0	5.8	42.2	89.1	0.01282	0.0068	83.9
60	45.50	24.0	5.8	39.7	83.8	0.01282	0.0049	78.9
250	40.00	24.0	5.8	34.2	72.2	0.01282	0.0025	68.0
1440	35.00	24.0	5.8	29.2	61.6	0.01282	0.0011	58.1

Soil Specimen Data		Other Corrections	
Tare No.	16		
Wt. of Tare & Dry Material (g):	352.41	a - Factor	0.993
Weight of Tare (g):	300.36		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	94.21
Weight of Dry Material (g):	47.05		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

## **Atterberg Limits Test Results:**

PL = 33 PI = 31

Tostad By	v .IV	Data	4/12/22	Checked By	NC.	Date	4/15/22



(Minus No. 40 sieve material, Air dried)

#### ATTERBERG LIMITS

ASTM D 4318-17

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW4-2

 Client Reference:
 24647-009-00, I-24/I-75 Interchange
 Depth (ft):
 23.5-25

 Project No.:
 N2022-051-001
 Sample No.:
 6

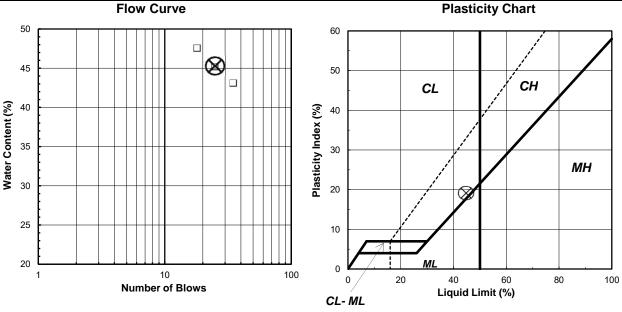
Note: The USCS symbol used with this test refers only to the minus No. 40

Lab ID: N2022-051-001-039 Soil Description: BROWNISH ORANGE LEAN CLAY

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture		Liquid Limit Test				
ASTM D2216-19		1	2	3	M	
Tare Number:	31	N	L	0	U	
Wt. of Tare & Wet Sample (g):	1095.29	32.40	33.57	32.61	L	
Wt. of Tare & Dry Sample (g):	924.32	29.66	30.46	29.62	Т	
Weight of Tare (g):	201.88	23.30	23.57	23.33	I	
Weight of Water (g):	171.0	2.7	3.1	3.0	Р	
Weight of Dry Sample (g):	722.4	6.4	6.9	6.3	0	
Was As Received MC Preserved:	Yes				1	
Moisture Content (%):	23.7	43.1	45.1	47.5	N	
Number of Blows:		35	25	18	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	Q	С		Liquid Limit (%):	45
Wt. of Tare & Wet Sample (g):	34.18	34.03			
Wt. of Tare & Dry Sample (g):	31.98	31.86		Plastic Limit (%):	26
Weight of Tare (g):	23.62	23.60			
Weight of Water (g):	2.2	2.2		Plasticity Index (%):	19
Weight of Dry Sample (g):	8.4	8.3			
				USCS Symbol:	CL
Moisture Content (%):	26.3	26.3	0.0		
Note: The acceptable range of the	e two Moistu	re Conten	ts is ± 1.12		



page 1 of 1 DCN: CTS4B, REV. 8, 5/22/18

JV

Date

Tested By

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4/15/22

Date

Checked By

NC

4/13/22



ASTM D 422-63 (2007), AASHTO T88

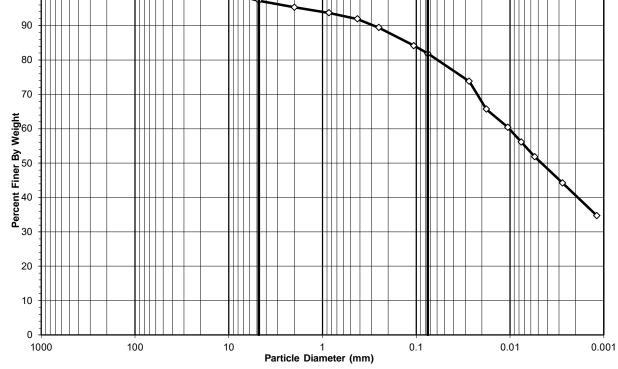
 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW4-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 23.5-25

 Project No.:
 N2022-051-001
 Sample No.:
 6

Lab ID: N2022-051-001-039 Soil Color: Brownish Orange

		SIEVE ANA	HYDROMETER	
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
100	12" 6"	3" \$\sqrt{3/8"} #4 ;	#10 #20 #40 #100 #2	200
80				



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	4.69		
100	100.00	Gravel	2.78	Sand	13.47	Gravel	2.78
2	95.31	Sand	15.38	Coarse Sand	3.39	Sand	15.38
0.075	81.84	Silt&Clay	81.84	Fine Sand	10.08	Silt	30.98
0.05	78.61			Silt & Clay	81.84	Clay	50.86
0.005	50.86			Silt	41.25		
0.002	40.59			Clay	40.59		

AASHTO (GI): A - 7 - 6 (17) USCS Symbol: CL, TESTED

USCS Classification
LEAN CLAY WITH SAND

page 1 of 3  $\,$  DCN: CT-S3X  $\,$  DATE: 4/30/18  $\,$  REVISION: 8  $\,$ 

 ${\it S:/Excel/Excell~QA/Spreadsheets/SIEVE~AASHTO~SieveHyd.xls}$ 



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW4-2
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 23.5-25
Project No.: N2022-051-001 Sample No.: 6

Lab ID: N2022-051-001-039 Soil Color: Brownish Orange

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material	
Tare No.:	31	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	592.58	Weight of Tare & Wet Sample (g):	NA
Wt. of Tare & Dry Sample (g):	592.58	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	201.88	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	390.70	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	390.70
Dry Weight of - 3/4" Sample (g):	390.70	Weight of minus #200 Material (g):	319.75
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	70.95
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	390.70		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	3.11		0.80	0.80	99.20	99.20
3/8"	9.50	0.00		0.00	0.80	99.20	99.20
#4	4.75	7.76		1.99	2.78	97.22	97.22
#10	2.00	7.44		1.90	4.69	95.31	95.31
#20	0.85	6.37	( ** )	1.63	6.32	93.68	93.68
#40	0.425	6.89		1.76	8.08	91.92	91.92
#60	0.250	9.79		2.51	10.59	89.41	89.41
#140	0.106	20.48		5.24	15.83	84.17	84.17
#200	0.075	9.11		2.33	18.16	81.84	81.84
Pan	-	319.75	•	81.84	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW4-2
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 23.5-25

Project No.: N2022-051-001 Sample No.: 6

Lab ID: N2022-051-001-039 Soil Color: Brownish Orange

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction C	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	44.50	24.0	5.8	38.7	90.1	0.01282	0.0272	73.8
5	40.25	24.0	5.8	34.5	80.2	0.01282	0.0179	65.7
15	37.50	24.0	5.8	31.7	73.8	0.01282	0.0105	60.4
30	35.25	24.0	5.8	29.5	68.6	0.01282	0.0076	56.1
60	33.00	24.0	5.8	27.2	63.3	0.01282	0.0055	51.8
250	29.00	24.0	5.8	23.2	54.0	0.01282	0.0028	44.2
1440	24.00	24.0	5.8	18.2	42.4	0.01282	0.0012	34.7

Soil Specimen Data		Other Corrections	
Tare No.	17		
Wt. of Tare & Dry Material (g):	346.96	a - Factor	0.993
Weight of Tare (g):	299.32		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	81.84
Weight of Dry Material (g):	42.64		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

## **Atterberg Limits Test Results:**

LL = 45

PL = 26

PI = 19

Tester	4 D./ I	\/	Date	A/12/22	Checked By	NC	Date	4/15/22



(Minus No. 40 sieve material, Air dried)

### **ATTERBERG LIMITS**

ASTM D 4318-17

Client: GeoEngineers, Inc. Boring No.: RW4-3
Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 18.5-20
Project No.: N2022-051-001 Sample No.: 5

Note: The USCS symbol used with this test refers only to the minus No. 40

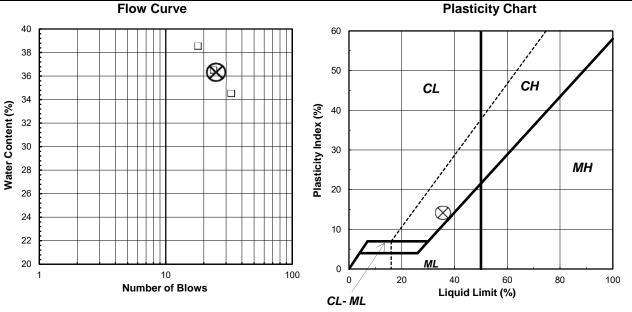
Lab ID: N2022-051-001 Sample No.: 5

Soil Description: ORANGISH BROWN LEAN CLAY

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	Content		Liquid Limit Test					
ASTM D2216-19		1	2	3	M			
Tare Number:	26	В	Р	Н	U			
Wt. of Tare & Wet Sample (g):	927.02	33.72	33.45	32.61	L			
Wt. of Tare & Dry Sample (g):	813.85	31.08	30.85	30.04	Т			
Weight of Tare (g):	198.55	23.43	23.72	23.37	I			
Weight of Water (g):	113.2	2.6	2.6	2.6	Р			
Weight of Dry Sample (g):	615.3	7.7	7.1	6.7	0			
Was As Received MC Preserved:	Yes				I			
Moisture Content (%):	18.4	34.5	36.5	38.5	N			
Number of Blows:		33	24	18	Т			

Plastic Limit Test	1	2	Range	Test Results				
Tare Number:	U	K		Liquid Limit (%):	36			
Wt. of Tare & Wet Sample (g):	36.73	34.60						
Wt. of Tare & Dry Sample (g):	34.39	32.65		Plastic Limit (%):	22			
Weight of Tare (g):	23.68	23.64						
Weight of Water (g):	2.3	2.0		Plasticity Index (%):	14			
Weight of Dry Sample (g):	10.7	9.0						
				USCS Symbol:	CL			
Moisture Content (%):	21.8	21.6	0.2					
Note: The acceptable range of the two Moisture Contents is ± 1.12								



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JV

Date

Tested By

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4/15/22

Date

Checked By

NC

4/13/22



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW4-3

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 18.5-20

 Project No.:
 N2022-051-001
 Sample No.:
 5

Lab ID: N2022-051-001-043 Soil Color: Orangish Brown

		SIEVE ANALYSIS					HYDROMETER	
USCS	cobbles	gravel	L.,	sand				clay fraction
AASHTO	cobbles	gravel		sand			silt and	clay fraction
100 1	12" 6"	3"	4 #1	0 #20 #40	#100 #20	00		
1								
90 🚻		<b>                                     </b>						
]								
80 1		<del>                                     </del>						
_ [		N						
70								
<b>E</b> 60								
<b>M M</b>			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \					
<u>a</u> <sub>50</sub> 1∭								
Percent Finer By Weight					<u>,                                       </u>			
= 40 <del>}</del> ₩								
						$\qquad \qquad \qquad \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$		
30								
- 1								
20								
10								<u>                                     </u>
10								
1				[			_   <b> </b>	

Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	41.18		
100	100.00	Gravel	29.79	Sand	21.72	Gravel	29.79
2	58.82	Sand	33.11	Coarse Sand	10.88	Sand	33.11
0.075	37.10	Silt&Clay	37.10	Fine Sand	10.84	Silt	13.46
0.05	35.99			Silt & Clay	37.10	Clay	23.64
0.005	23.64			Silt	18.68		
0.002	18.42			Clay	18.42		
AASHTO (GI): USCS Symb			ol:		D50 =	0.59	

Particle Diameter (mm)

0.1

 AASHTO (GI):
 USCS Symbol:

 A - 6
 (1)

 SC, TESTED

100

10

USCS Classification
CLAYEY SAND WITH GRAVEL

1000

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0.01

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ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW4-3
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 18.5-20
Project No.: N2022-051-001 Sample No.: 5

Lab ID: N2022-051-001-043 Soil Color: Orangish Brown

Moisture Content of Passing 3/4" M	1aterial	Moisture Content of Retained 3/4" Material				
Tare No.:	26	Tare No.:	NA			
Wt. of Tare & Wet Sample (g):	522.45	Weight of Tare & Wet Sample (g):	NA			
Wt. of Tare & Dry Sample (g):	522.45	Weight of Tare & Dry Sample (g):	NA			
Weight of Tare (g):	198.55	Weight of Tare (g):	NA			
Weight of Water (g):	0.00	Weight of Water (g):	NA			
Weight of Dry Soil (g):	323.90	Weight of Dry Soil (g):	NA			
Moisture Content (%):	0.0	Moisture Content (%):	0.0			

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	323.90
Dry Weight of - 3/4" Sample (g):	323.90	Weight of minus #200 Material (g):	120.18
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	203.72
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	323.90		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	35.33		10.91	10.91	89.09	89.09
3/8"	9.50	17.64		5.45	16.35	83.65	83.65
#4	4.75	43.51		13.43	29.79	70.21	70.21
#10	2.00	36.89		11.39	41.18	58.82	58.82
#20	0.85	21.13	( ** )	6.52	47.70	52.30	52.30
#40	0.425	14.11		4.36	52.06	47.94	47.94
#60	0.250	14.00		4.32	56.38	43.62	43.62
#140	0.106	16.48		5.09	61.47	38.53	38.53
#200	0.075	4.63		1.43	62.90	37.10	37.10
Pan	-	120.18		37.10	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW4-3
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 18.5-20

Project No.: N2022-051-001 Sample No.: 5

Lab ID: N2022-051-001-043 Soil Color: Orangish Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time (min)	Measured	(°C)	Correction Corrected		Factor (%)		(mm)	(%)
()		( 0)			(70)			(70)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	30.00	24.0	5.8	24.2	93.4	0.01282	0.0306	34.6
5	27.25	24.0	5.8	21.5	82.8	0.01282	0.0197	30.7
15	26.00	24.0	5.8	20.2	77.9	0.01282	0.0115	28.9
30	24.00	24.0	5.8	18.2	70.2	0.01282	0.0082	26.1
60	23.00	24.0	5.8	17.2	66.4	0.01282	0.0059	24.6
250	20.00	24.0	5.8	14.2	54.8	0.01282	0.0029	20.3
1440	17.00	24.0	5.8	11.2	43.2	0.01282	0.0012	16.0

Soil Specimen Data		Other Corrections			
Tare No.	18				
Wt. of Tare & Dry Material (g):	330.66	a - Factor	0.993		
Weight of Tare (g):	299.92				
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	37.10		
Weight of Dry Material (g):	25.74				
, , ,		Specific Gravity	2.70 Assumed		

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

LL = 36

PL = 22

PI = 14

Tested By JV Date 4/12/22 Checked By NC Date 4/15/22

page 3 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8



### ATTERBERG LIMITS

ASTM D 4318-17

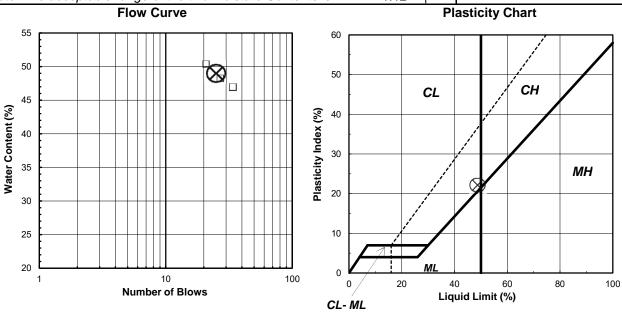
Client: GeoEngineers, Inc. Boring No.: RW5-2 Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 8.5-10 Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-055 Soil Description: RED LEAN CLAY

Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried)

As Received Moisture	As Received Moisture Content				est	
ASTM D2216-19		1	2	3	M	
Tare Number:	Z18	D	S	W	U	
Wt. of Tare & Wet Sample (g):	756.47	33.37	33.50	33.26	L	
Wt. of Tare & Dry Sample (g):	635.97	30.22	30.27	30.05	Т	
Weight of Tare (g):	200.56	23.50	23.57	23.67	I	
Weight of Water (g):	120.5	3.2	3.2	3.2	Р	
Weight of Dry Sample (g):	435.4	6.7	6.7	6.4	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%): 27.7		46.9	48.2	50.3	N	
Number of Blows:		34	27	21	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	13	14		Liquid Limit (%):	49
Wt. of Tare & Wet Sample (g):	27.95	26.78			
Wt. of Tare & Dry Sample (g):	26.11	25.01		Plastic Limit (%):	27
Weight of Tare (g):	19.35	18.58			
Weight of Water (g):	1.8	1.8		Plasticity Index (%):	22
Weight of Dry Sample (g):	6.8	6.4			
				USCS Symbol:	CL
Moisture Content (%):	27.2	27.5	-0.3		
Note: The acceptable range of the	e two Moistu	ire Conten	ts is ± 1.12		



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Tested By

JV

Date

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4/15/22

Date

Checked By

NC

4/13/22



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW5-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 8.5-10

 Project No.:
 N2022-051-001
 Sample No.:
 3

 Lab ID:
 N2022-051-001-055
 Soil Color:
 Red

		SIEVE	ANALYSIS	HYDROMETER
USCS cobbles		gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
100	12" 6"	3" \\ \sigma \si	4 #10 #20 #40 #100 #2	00 
90				
80				
70 1				
Percent Finer By Weight				
ent Fine				
30 1				
20				
10				
<sub>0</sub> ‡				

Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	4.36		
100	100.00	Gravel	2.24	Sand	13.94	Gravel	2.24
2	95.64	Sand	16.06	Coarse Sand	4.69	Sand	16.06
0.075	81.70	Silt&Clay	81.70	Fine Sand	9.24	Silt	23.62
0.05	78.70			Silt & Clay	81.70	Clay	58.07
0.005	58.07			Silt	32.76		
0.002	48.94			Clay	48.94		

Particle Diameter (mm)

AASHTO (GI): A - 7 - 6 (19)

1000

USCS Symbol: CL, TESTED

USCS Classification
LEAN CLAY WITH SAND

page 1 of 3  $\,$  DCN: CT-S3X  $\,$  DATE: 4/30/18  $\,$  REVISION: 8  $\,$ 

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ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW5-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 8.5-10

 Project No.:
 N2022-051-001
 Sample No.:
 3

 Lab ID:
 N2022-051-001-055
 Soil Color:
 Red

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material				
Tare No.:	Z18	Tare No.:	NA			
Wt. of Tare & Wet Sample (q):	415.47	Weight of Tare & Wet Sample (g):	NA NA			
Wt. of Tare & Dry Sample (g):	415.47	Weight of Tare & Dry Sample (g):	NA			
Weight of Tare (g):	200.56	Weight of Tare (g):	NA			
Weight of Water (g):	0.00	Weight of Water (g):	NA			
Weight of Dry Soil (g): 214.91		Weight of Dry Soil (g):	NA			
Moisture Content (%):	0.0	Moisture Content (%):	0.0			

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	214.91
Dry Weight of - 3/4" Sample (g):	214.91	Weight of minus #200 Material (g):	175.58
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	39.33
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	214.91		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	0.00		0.00	0.00	100.00	100.00
3/8"	9.50	1.19		0.55	0.55	99.45	99.45
#4	4.75	3.63		1.69	2.24	97.76	97.76
#10	2.00	4.56		2.12	4.36	95.64	95.64
#20	0.85	4.50	( ** )	2.09	6.46	93.54	93.54
#40	0.425	5.59		2.60	9.06	90.94	90.94
#60	0.250	10.42		4.85	13.91	86.09	86.09
#140	0.106	8.94		4.16	18.07	81.93	81.93
#200	0.075	0.50		0.23	18.30	81.70	81.70
Pan	-	175.58	•	81.70	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW5-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 8.5-10

 Project No.:
 N2022-051-001
 Sample No.:
 3

 Lab ID:
 N2022-051-001-055
 Soil Color:
 Red

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction C	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	47.50	24.2	5.7	41.8	90.6	0.01279	0.0264	74.0
5	45.25	24.2	5.7	39.5	85.7	0.01279	0.0170	70.0
15	42.75	24.2	5.7	37.0	80.3	0.01279	0.0101	65.6
30	41.00	24.2	5.7	35.3	76.5	0.01279	0.0072	62.5
60	38.75	24.2	5.7	33.0	71.6	0.01279	0.0052	58.5
250	35.00	23.9	5.8	29.2	63.3	0.01284	0.0026	51.7
1440	30.00	24.8	5.6	24.4	53.0	0.01270	0.0011	43.3

Soil Specimen Data		Other Corrections	
Tare No.	1		
Wt. of Tare & Dry Material (g):	357.15	a - Factor	0.993
Weight of Tare (g):	306.36		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	81.70
Weight of Dry Material (g):	45.79		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

LL = 49

PL = 27

PI = 22

Tested By JV Date 4/13/22 Checked By NC Date 4/15/22



### ATTERBERG LIMITS

ASTM D 4318-17

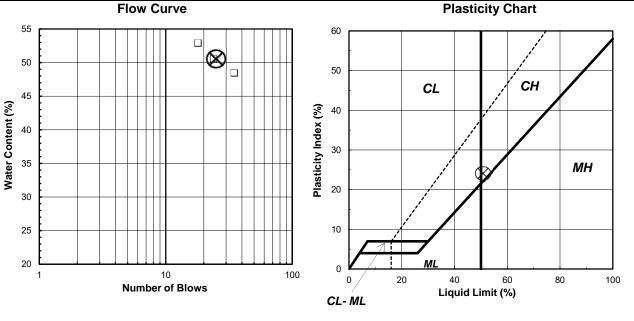
Client: GeoEngineers, Inc. Boring No.: RW6-2 Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 1-2.5 Project No.: N2022-051-001 Sample No.: 1

Lab ID: N2022-051-001-061 Soil Description: BROWN FAT CLAY

Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried) sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	Content		Liquid Limit Test  1 2 3 M  M G X U			
ASTM D2216-19		1	2	3	M	
Tare Number:	51	М	G	X	U	
Wt. of Tare & Wet Sample (g):	623.33	33.15	33.96	32.73	L	
Wt. of Tare & Dry Sample (g):	527.31	30.06	30.48	29.52	Т	
Weight of Tare (g):	198.71	23.68	23.59	23.45	I	
Weight of Water (g):	96.0	3.1	3.5	3.2	Р	
Weight of Dry Sample (g):	328.6	6.4	6.9	6.1	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%):	29.2	48.4	50.5	52.9	N	
Number of Blows:		35	24	18	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	Α	J		Liquid Limit (%):	51
Wt. of Tare & Wet Sample (g):	30.34	34.41			
Wt. of Tare & Dry Sample (g):	28.89	32.07		Plastic Limit (%):	27
Weight of Tare (g):	23.59	23.55			
Weight of Water (g):	1.5	2.3		Plasticity Index (%):	24
Weight of Dry Sample (g):	5.3	8.5			
				USCS Symbol:	CH
Moisture Content (%):	27.4	27.5	-0.1		
Note: The acceptable range of the	e two Moistu	re Conten	ts is ± 1.4		



page 1 of 1 DCN: CTS4B, REV. 8, 5/22/18

JV

Date

Tested By

S:\Excel\Excel QA\Spreadsheets\Limit 3Pt.xls

4/15/22

Date

Checked By

NC

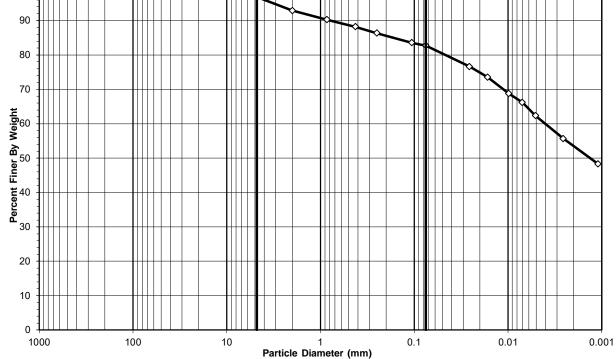
4/13/22



ASTM D 422-63 (2007), AASHTO T88

Client: RW6-2 GeoEngineers, Inc. Boring No.: Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 1-2.5 Project No.: Sample No.: 1 N2022-051-001 Soil Color: Lab ID: N2022-051-001-061 Brown

		SIEVE	ANALYSIS	HYDROMETER
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
400	12" 6,"	3" ^3/4" ^3/8" #	4 #10 #20 #40 #100 #2	200
100 Ⅲ				
90 #				
1				
80 ]				
]				
				<b> </b>



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	7.09		
100	100.00	Gravel	3.19	Sand	10.21	Gravel	3.19
2	92.91	Sand	14.11	Coarse Sand	4.73	Sand	14.11
0.075	82.70	Silt&Clay	82.70	Fine Sand	5.48	Silt	20.55
0.05	80.38			Silt & Clay	82.70	Clay	62.16
0.005	62.16			Silt	29.22		
0.002	53.49			Clay	53.49		

AASHTO (GI): A - 7 - 6 (22) **USCS Symbol:** CH, TESTED

**USCS Classification** FAT CLAY WITH SAND

page 1 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW6-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 1-2.5

 Project No.:
 N2022-051-001
 Sample No.:
 1

 Lab ID:
 N2022-051-001-061
 Soil Color:
 Brown

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material	
Tare No.:	51	Tare No.:	NA
Wt. of Tare & Wet Sample (q):	418.85	Weight of Tare & Wet Sample (g):	NA NA
Wt. of Tare & Dry Sample (g):	418.85	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	198.71	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	220.14	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	220.14
Dry Weight of - 3/4" Sample (g):	220.14	Weight of minus #200 Material (g):	182.06
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	38.08
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	220.14		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	0.00		0.00	0.00	100.00	100.00
3/8"	9.50	1.07		0.49	0.49	99.51	99.51
#4	4.75	5.95		2.70	3.19	96.81	96.81
#10	2.00	8.58		3.90	7.09	92.91	92.91
#20	0.85	5.92	( ** )	2.69	9.78	90.22	90.22
#40	0.425	4.49		2.04	11.82	88.18	88.18
#60	0.250	4.09		1.86	13.67	86.33	86.33
#140	0.106	6.14		2.79	16.46	83.54	83.54
#200	0.075	1.84		0.84	17.30	82.70	82.70
Pan	-	182.06		82.70	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/15/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW6-2

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 1-2.5

 Project No.:
 N2022-051-001
 Sample No.:
 1

 Lab ID:
 N2022-051-001-061
 Soil Color:
 Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	50.00	24.2	5.7	44.3	92.6	0.01279	0.0257	76.6
5	48.25	24.2	5.7	42.5	88.9	0.01279	0.0166	73.6
15	45.50	24.2	5.7	39.8	83.2	0.01279	0.0098	68.8
30	44.00	24.2	5.7	38.3	80.0	0.01279	0.0070	66.2
60	41.75	24.2	5.7	36.0	75.3	0.01279	0.0051	62.3
250	38.00	23.9	5.8	32.2	67.3	0.01284	0.0026	55.7
1440	33.50	24.8	5.6	27.9	58.4	0.01270	0.0011	48.3

Soil Specimen Data		Other Corrections	
Tare No.	2		
Wt. of Tare & Dry Material (g):	362.89	a - Factor	0.993
Weight of Tare (g):	310.43		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	82.70
Weight of Dry Material (g):	47.46		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

LL = 51

PL = 27

PI = 24

Tested By JV Date 4/13/22 Checked By NC Date 4/15/22

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### ATTERBERG LIMITS

ASTM D 4318-17

Client: GeoEngineers, Inc. Boring No.: RW6-4
Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 8.5-10
Project No.: N2022-051-001 Sample No.: 3

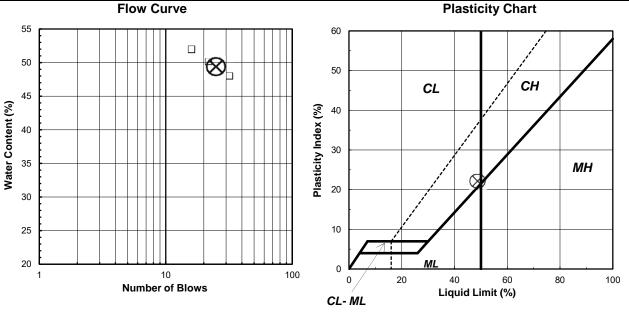
Lab ID: N2022-051-001-065 Soil Description: BROWNISH ORANGE LEAN CLAY

Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	Content		Liquid Limit Test			
ASTM D2216-19		1	2	3	M	
Tare Number:	Z10	R	E	V	U	
Wt. of Tare & Wet Sample (g):	687.11	32.61	32.04	33.39	L	
Wt. of Tare & Dry Sample (g):	595.22	29.63	29.18	30.02	Т	
Weight of Tare (g):	199.79	23.42	23.47	23.53	I	
Weight of Water (g):	91.9	3.0	2.9	3.4	Р	
Weight of Dry Sample (g):	395.4	6.2	5.7	6.5	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%):	23.2	48.0	50.1	51.9	N	
Number of Blows:		32	22	16	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	F	Т		Liquid Limit (%):	49
Wt. of Tare & Wet Sample (g):	33.09	33.67			
Wt. of Tare & Dry Sample (g):	31.08	31.49		Plastic Limit (%):	27
Weight of Tare (g):	23.71	23.54			
Weight of Water (g):	2.0	2.2		Plasticity Index (%):	22
Weight of Dry Sample (g):	7.4	8.0			
				USCS Symbol:	CL
Moisture Content (%):	27.3	27.4	-0.1		
Note: The acceptable range of the	e two Moistu	ire Content	ts <i>i</i> s ± 1.12		



Tested By JV Date 4/13/22 Checked By NC Date 4/15/22

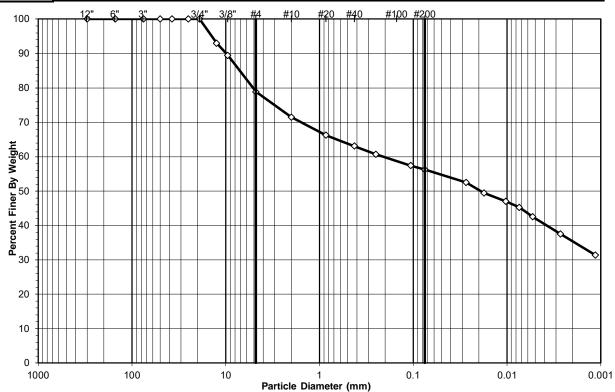


ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW6-4
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 8.5-10
Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-065 Soil Color: Brownish Orange

		SIEVE	HYDROMETER	
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	28.53		
100	100.00	Gravel	21.17	Sand	15.26	Gravel	21.17
2	71.47	Sand	22.62	Coarse Sand	8.39	Sand	22.62
0.075	56.20	Silt&Clay	56.20	Fine Sand	6.87	Silt	14.13
0.05	54.73			Silt & Clay	56.20	Clay	42.07
0.005	42.07			Silt	20.82		
0.002	35.38			Clay	35.38		

AASHTO (GI): USCS Symbol: A - 7 - 6 (10) CL, TESTED

USCS Classification

SANDY LEAN CLAY WITH GRAVEL

page 1 of 3  $\,$  DCN: CT-S3X  $\,$  DATE: 4/30/18  $\,$  REVISION: 8  $\,$ 



ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW6-4

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 8.5-10

 Project No.:
 N2022-051-001
 Sample No.:
 3

Lab ID: N2022-051-001-065 Soil Color: Brownish Orange

Moisture Content of Passing 3/4" N	/laterial	Moisture Content of Retained 3/4" Material			
Tare No.:	Z10	Tare No.:	NA		
Wt. of Tare & Wet Sample (g):	494.07	Weight of Tare & Wet Sample (g):	NA		
Wt. of Tare & Dry Sample (g):	494.07	Weight of Tare & Dry Sample (g):	NA		
Weight of Tare (g):	199.79	Weight of Tare (g):	NA		
Weight of Water (g):	0.00	Weight of Water (g):	NA		
Weight of Dry Soil (g):	294.28	Weight of Dry Soil (g):	NA		
Moisture Content (%):	0.0	Moisture Content (%):	0.0		

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	294.28
Dry Weight of - 3/4" Sample (g):	294.28	Weight of minus #200 Material (g):	165.40
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	128.88
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	294.28		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	20.61		7.00	7.00	93.00	93.00
3/8"	9.50	10.45		3.55	10.55	89.45	89.45
#4	4.75	31.24		10.62	21.17	78.83	78.83
#10	2.00	21.67		7.36	28.53	71.47	71.47
#20	0.85	15.39	( ** )	5.23	33.76	66.24	66.24
#40	0.425	9.30		3.16	36.92	63.08	63.08
#60	0.250	7.00		2.38	39.30	60.70	60.70
#140	0.106	9.71		3.30	42.60	57.40	57.40
#200	0.075	3.51		1.19	43.80	56.20	56.20
Pan	-	165.40		56.20	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/15/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW6-4
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 8.5-10

Project No.: N2022-051-001 Sample No.: 3

Lab ID: N2022-051-001-065 Soil Color: Brownish Orange

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	43.75	24.2	5.7	38.0	93.4	0.01279	0.0273	52.5
5	41.50	24.2	5.7	35.8	87.9	0.01279	0.0176	49.4
15	39.75	24.2	5.7	34.0	83.6	0.01279	0.0103	47.0
30	38.50	24.2	5.7	32.8	80.5	0.01279	0.0074	45.3
60	36.50	24.2	5.7	30.8	75.6	0.01279	0.0053	42.5
250	33.00	23.8	5.9	27.1	66.7	0.01285	0.0027	37.5
1440	28.25	24.8	5.6	22.7	55.8	0.01270	0.0011	31.3

0.993
56.20
2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

LL = 49

PL = 27

PI = 22

Tested By JV Date 4/13/22 Checked By NC Date 4/15/22

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### ATTERBERG LIMITS

ASTM D 4318-17

Client: GeoEngineers, Inc. Boring No.: RW6-6
Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 13.5-14.9

Project No.: N2022-051-001 Sample No.: 4

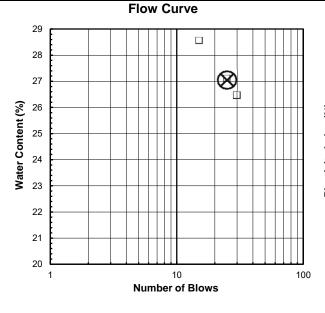
Lab ID: N2022-051-001-069 Soil Description: GRAYISH GREEN LEAN CLAY

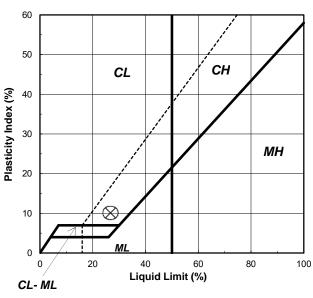
Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried)

sieve material. See the	"Sieve and Hydromete	er Δnalvsis" granh i	nage for the com	plete material description.
Sieve iliaterial. See the	Oleve allu liyulolliek	71 Allalysis ylapii j	vage for the com	piele ilialeriai description .

As Received Moisture	As Received Moisture Content				Liquid Limit Test				
ASTM D2216-19		1	2	3	M				
Tare Number:	1569	1	2	3	U				
Wt. of Tare & Wet Sample (g):	862.84	26.80	28.13	28.66	L				
Wt. of Tare & Dry Sample (g):	817.33	24.76	26.06	26.45	T				
Weight of Tare (g):	306.70	17.05	18.42	18.71	I				
Weight of Water (g):	45.5	2.0	2.1	2.2	Р				
Weight of Dry Sample (g):	510.6	7.7	7.6	7.7	0				
Was As Received MC Preserved:	Yes				I				
Moisture Content (%):	8.9	26.5	27.1	28.6	N				
Number of Blows:		30	25	15	Т				

Plastic Limit Test	1	2	Range	Test Results
Tare Number:	15	16		Liquid Limit (%): 27
Wt. of Tare & Wet Sample (g):	26.59	27.30		
Wt. of Tare & Dry Sample (g):	25.51	26.00		Plastic Limit (%): 17
Weight of Tare (g):	19.30	18.55		` ` `
Weight of Water (g):	1.1	1.3		Plasticity Index (%): 10
Weight of Dry Sample (g):	6.2	7.5		
				USCS Symbol: CL
Moisture Content (%):	17.4	17.4	-0.1	
Note: The acceptable range of the	e two Moistu	ire Content	s is ± 1.12	
Flow Curve	е	•		Plasticity Chart





Tested By JV Date 4/13/22 Checked By NC Date 4/15/22



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW6-6
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 13.5-14.9

Project No.: N2022-051-001 Sample No.: 4

Lab ID: N2022-051-001-069 Soil Color: Grayish Green

		SIEVE	ANALYSIS	HYDROMETER
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
100	12" 6"	3/4" 3/8" #/	4 #10 #20 #40 #1 <u>00</u> #.	200
90		<b>\</b>		
80		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		
70		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		
Percent Finer By Weight				
iner By				
40 1				
30				
20				
10				
0 ‡∐ 1000	100	10	1 0.1	0.01 0.001

Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	57.45		
100	100.00	Gravel	49.85	Sand	18.72	Gravel	49.85
2	42.55	Sand	26.32	Coarse Sand	11.97	Sand	26.32
0.075	23.83	Silt&Clay	23.83	Fine Sand	6.75	Silt	8.46
0.05	22.94			Silt & Clay	23.83	Clay	15.38
0.005	15.38			Silt	13.56		
0.002	10.28			Clay	10.28		
AASHTO (	GI):	<u> </u>	JSCS Symbo	<u>l:</u>	·	D50 =	4.67

Particle Diameter (mm)

A - 2 - 4 (0) GC, TESTED

<u>USCS Classification</u> CLAYEY GRAVEL WITH SAND

page 1 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8

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ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW6-6
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 13.5-14.9

Project No.: N2022-051-001 Sample No.: 4

Lab ID: N2022-051-001-069 Soil Color: Grayish Green

Moisture Content of Passing 3/4" Material		Moisture Content of Retained 3/4" Material			
Tare No.:	1569	Tare No.:	NA		
Wt. of Tare & Wet Sample (g):	570.41	Weight of Tare & Wet Sample (g):	NA		
Wt. of Tare & Dry Sample (g):	570.41	Weight of Tare & Dry Sample (g):	NA		
Weight of Tare (g):	306.70	Weight of Tare (g):	NA		
Weight of Water (g):	0.00	Weight of Water (g):	NA		
Weight of Dry Soil (g):	263.71	Weight of Dry Soil (g):	NA		
Moisture Content (%):	0.0	Moisture Content (%):	0.0		

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	263.71
Dry Weight of - 3/4" Sample (g):	206.15	Weight of minus #200 Material (g):	62.85
Wet Weight of +3/4" Sample (g):	57.56	Weight of plus #200 Material (g):	200.86
Dry Weight of +3/4" Sample (g):	57.56		
Total Dry Weight of Sample (g):	263.71		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	46.51		17.64	17.64	82.36	82.36
3/4"	19.0	11.05		4.19	21.83	78.17	78.17
1/2"	12.5	29.54		11.20	33.03	66.97	66.97
3/8"	9.50	13.42		5.09	38.12	61.88	61.88
#4	4.75	30.93		11.73	49.85	50.15	50.15
#10	2.00	20.05		7.60	57.45	42.55	42.55
#20	0.85	19.72	( ** )	7.48	64.93	35.07	35.07
#40	0.425	11.85		4.49	69.42	30.58	30.58
#60	0.250	7.08		2.68	72.11	27.89	27.89
#140	0.106	8.24		3.12	75.23	24.77	24.77
#200	0.075	2.47		0.94	76.17	23.83	23.83
Pan	-	62.85		23.83	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22



ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW6-6
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 13.5-14.9

Project No.: N2022-051-001 Sample No.: 4

Lab ID: N2022-051-001-069 Soil Color: Grayish Green

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured	_	Correction C	orrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	24.50	24.2	5.7	18.8	92.1	0.01279	0.0317	21.9
5	23.25	24.2	5.7	17.5	85.9	0.01279	0.0202	20.5
15	22.25	24.2	5.7	16.5	81.0	0.01279	0.0117	19.3
30	20.75	24.2	5.7	15.0	73.7	0.01279	0.0084	17.6
60	19.75	24.2	5.7	14.0	68.8	0.01279	0.0060	16.4
250	16.50	23.8	5.9	10.6	52.3	0.01285	0.0030	12.5
1440	12.25	24.8	5.6	6.7	32.8	0.01270	0.0013	7.8

Soil Specimen Data		Other Corrections	
Tare No.	4		
Wt. of Tare & Dry Material (g):	339.33	a - Factor	0.993
Weight of Tare (g):	314.10		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	23.83
Weight of Dry Material (g):	20.23		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

### **Atterberg Limits Test Results:**

PL = 17

PI = 10

Tested By	I\/	Date	1/13/22	Checked By	NC:	Date	4/15/22



#### ATTERBERG LIMITS

ASTM D 4318-17

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW7-1

 Client Reference:
 24647-009-00, I-24/I-75 Interchange
 Depth (ft):
 28.5-30

 Project No.:
 N2022-051-001
 Sample No.:
 10

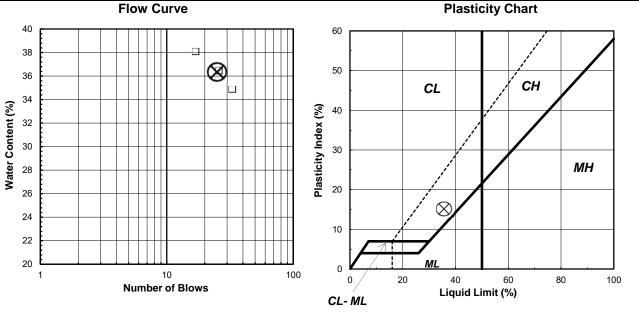
Lab ID: N2022-051-001-071 Soil Description: BROWNISH GRAY LEAN CLAY

Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture		Liquid Limit Test					
ASTM D2216-19		1	2	3	M		
Tare Number:	585	4	5	6	U		
Wt. of Tare & Wet Sample (g):	1064.11	26.99	27.69	27.81	L		
Wt. of Tare & Dry Sample (g):	950.94	24.63	25.25	25.29	Т		
Weight of Tare (g):	308.64	17.86	18.55	18.67	I		
Weight of Water (g):	113.2	2.4	2.4	2.5	Р		
Weight of Dry Sample (g):	642.3	6.8	6.7	6.6	0		
Was As Received MC Preserved:	Yes				I		
Moisture Content (%):	17.6	34.9	36.4	38.1	N		
Number of Blows:		33	26	17	T		

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	17	18		Liquid Limit (%):	36
Wt. of Tare & Wet Sample (g):	27.97	28.84		Liquid Lillit (70).	30
Wt. of Tare & Dry Sample (g):	26.33	27.18		Plastic Limit (%):	21
Weight of Tare (g):	18.49	19.21			
Weight of Water (g):	1.6	1.7		Plasticity Index (%):	15
Weight of Dry Sample (g):	7.8	8.0			
				USCS Symbol:	CL
Moisture Content (%):	20.9	20.8	0.1		
Note: The acceptable range of the	e two Moistu	re Conten	ts is ± 1.12		



Tested By JV Date 4/13/22 Checked By NC Date 4/15/22



#### SIEVE AND HYDROMETER ANALYSIS

ASTM D 422-63 (2007), AASHTO T88

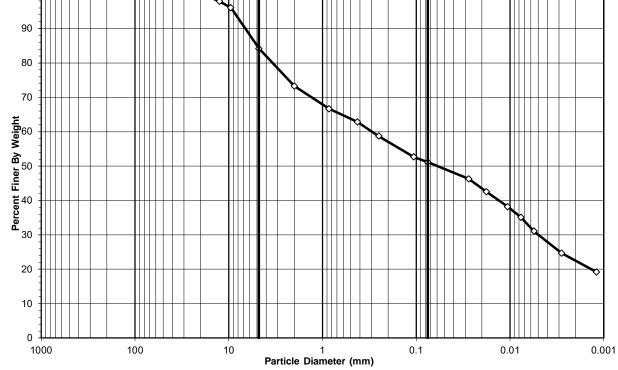
 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW7-1

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 28.5-30

 Project No.:
 N2022-051-001
 Sample No.:
 10

Lab ID: N2022-051-001-071 Soil Color: Brownish Gray

		SIEVE AN	HYDROMETER	
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
90	12" 6"	3" 3/8" #4	#10 #20 #40 #100 #2	200
80				



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	26.76		
100	100.00	Gravel	15.85	Sand	22.12	Gravel	15.85
2	73.24	Sand	33.03	Coarse Sand	10.43	Sand	33.03
0.075	51.12	Silt&Clay	51.12	Fine Sand	11.70	Silt	21.04
0.05	49.16			Silt & Clay	51.12	Clay	30.08
0.005	30.08			Silt	28.66		
0.002	22.46			Clay	22.46		

 AASHTO (GI):
 USCS Symbol:

 A - 6
 (5)

 CL, TESTED

USCS Classification
SANDY LEAN CLAY WITH GRAVEL

page 1 of 3  $\,$  DCN: CT-S3X  $\,$  DATE: 4/30/18  $\,$  REVISION: 8  $\,$ 



#### **WASH SIEVE ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW7-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 28.5-30
Project No.: N2022-051-001 Sample No.: 10

Lab ID: N2022-051-001-071 Soil Color: Brownish Gray

Weight of Tare (g): Weight of Water (g): Weight of Dry Soil (g):	NA
Weight of Tare (g): Weight of Water (g):	NA NA
. (0)	
Weight of Tale & Dry Sample (g).	1 17
Weight of Tare & Dry Sample (g):	NA
Weight of Tare & Wet Sample (g):	NA
Tare No.:	NA

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	286.52
Dry Weight of - 3/4" Sample (g):	286.52	Weight of minus #200 Material (g):	146.48
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	140.04
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	286.52		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	(*)	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	6.11		2.13	2.13	97.87	97.87
3/8"	9.50	5.18		1.81	3.94	96.06	96.06
#4	4.75	34.12		11.91	15.85	84.15	84.15
#10	2.00	31.25		10.91	26.76	73.24	73.24
#20	0.85	18.82	( ** )	6.57	33.32	66.68	66.68
#40	0.425	11.05		3.86	37.18	62.82	62.82
#60	0.250	11.80		4.12	41.30	58.70	58.70
#140	0.106	17.32		6.04	47.34	52.66	52.66
#200	0.075	4.39		1.53	48.88	51.12	51.12
Pan	-	146.48		51.12	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

Tested By	JV	Date	4/12/22	Checked By	NC	Date	4/15/22	



#### **HYDROMETER ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW7-1

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 28.5-30

 Project No.:
 N2022-051-001
 Sample No.:
 10

Lab ID: N2022-051-001-071 Soil Color: Brownish Gray

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	43.00	24.2	5.7	37.3	90.5	0.01279	0.0275	46.3
5	40.00	24.2	5.7	34.3	83.2	0.01279	0.0179	42.5
15	36.50	24.2	5.7	30.8	74.7	0.01279	0.0106	38.2
30	34.00	24.2	5.7	28.3	68.6	0.01279	0.0076	35.1
60	30.75	24.2	5.7	25.0	60.7	0.01279	0.0055	31.0
250	25.75	23.8	5.9	19.9	48.3	0.01285	0.0028	24.7
1440	21.00	24.8	5.6	15.4	37.5	0.01270	0.0012	19.2

		-
5		
358.36	a - Factor	0.993
312.47		
5.0	Percent Finer than # 200	51.12
40.89		
	Specific Gravity	2.70 Assumed
	358.36 312.47 5.0	358.36 a - Factor 312.47 5.0 Percent Finer than # 200 40.89

**Note:** Hydrometer test is performed on - # 200 sieve material.

#### **Atterberg Limits Test Results:**

PL = 21

PI = 15

Tested By JV Date 4/13/22 Checked By NC Date 4/15/22

page 3 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8



April 21, 2022

Project No. N2022-051-002

Emily Reed GeoEngineers, Inc. 5409 Maryland Way, Suite 150 Brentwood, TN 37027

## <u>Transmittal</u> <u>Laboratory Test Results</u> 24647-009-00, I-24/I-75 Interchange

Please find attached the laboratory test results for the above referenced project. The testing was performed in general accordance with the methods listed on the enclosed data sheets. The test results are believed to be representative of the samples that were submitted for testing and are indicative only of the specimens which were evaluated. We have no direct knowledge of the origin of the samples and imply no position regarding the nature of the test results, i.e., pass/fail and no claims as to the suitability of the material for its intended use. The client should evaluate the data and interpret design parameters based on their knowledge of the Project.

The test data and all associated project information provided shall be held in strict confidence and disclosed to other parties only with authorization by our Client. The test data submitted herein is considered integral with this report and is not to be reproduced except in whole and only with the authorization of the Client and Geotechnics. The remaining sample materials for this project will be retained for a minimum of 90 days as directed by the Geotechnics' Quality Program.

We are pleased to provide these testing services. Should you have any questions or if we may be of further assistance, please contact our office.

Respectfully submitted, *Geotechnics*, *Inc*.

Wm. Daniel Smith, P.E. Regional Manager

m. Daniel Smith

We understand that you have a choice in your laboratory services and we thank you for choosing Geotechnics.



#### **MOISTURE CONTENT**

ASTM D 2216-10

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00, I-24/I-75 Interchange

Project No.: N2022-051-002

Lab ID:	001	002	003	004	005
Boring No.:	RW2-1	RW8-1	RW8-1	RW8-1	RW8-1
Depth (ft):	3.5-5	23.5-25	33.5-35	38.5-40	43.5-45
Sample No.:	2	5	7	8	9
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	26	1519	1482	51	1439
	968.88	497.28	811.69	1249.25	680.88
	860.21	452.48	691.80	1057.12	569.92
	198.55	147.67	147.65	198.66	144.79
	108.67	44.80	119.89	192.13	110.96
	661.66	304.81	544.15	858.46	425.13
Water Content (%)	16.4	14.7	22.0	22.4	26.1
Lab ID: Boring No.: Depth (ft): Sample No.:	006	007	008	009	010
	RW10-1	RW10-1	RW10-1	RW10-2	RW10-2
	28.5-30	33.5-35	43.5-45	8.5-10	23.5-25
	7	9	10	3	6
Tare Number Wt. of Tare & Wet Sample (g) Wt. of Tare & Dry Sample (g) Weight of Tare (g) Weight of Water (g) Weight of Dry Sample (g)	55	1416	1545	29	1506
	1137.79	871.09	822.24	510.45	477.64
	980.49	754.28	655.49	469.19	434.66
	201.27	145.71	147.36	203.05	145.70
	157.30	116.81	166.75	41.26	42.98
	779.22	608.57	508.13	266.14	288.96
Water Content (%)	20.2	19.2	32.8	15.5	14.9

Notes:

Tested By JV Date 4/15/22 Checked By NC Date 4/20/22

page 1 of 1

DCN: CT-S1 DATE: 3/18/13 REVISION: 4



#### **MOISTURE CONTENT**

ASTM D 2216-10

Client: GeoEngineers, Inc.

Client Reference: 24647-009-00, I-24/I-75 Interchange

Project No.: N2022-051-002

Lab ID: Boring No.: Depth (ft): Sample No.:	011 RW10-2 38.5-40 9	012 RW10-2 48.5-50 11	013 RW11-1A 13.5-15 2	014 RW11-2 18.5-20 5	015 RW11-2 43.5-45 10
Tare Number	1556	1461	1470	27	1546
Wt. of Tare & Wet Sample (g)	629.83	710.85	779.88	1014.30	660.26
Wt. of Tare & Dry Sample (g)	544.79	586.32	693.20	895.80	570.19
Weight of Tare (g)	146.66	146.14	146.58	202.80	147.61
Weight of Water (g)	85.04	124.53	86.68	118.50	90.07
Weight of Dry Sample (g)	398.13	440.18	546.62	693.00	422.58
Water Content (%)	21.4	28.3	15.9	17.1	21.3

Notes:

Tested By JV Date 4/15/22 Checked By NC Date 4/20/22

page 1 of 1

DCN: CT-S1 DATE: 3/18/13 REVISION: 4

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#### ATTERBERG LIMITS

ASTM D 4318-17

Client: GeoEngineers, Inc. Boring No.: RW2-1 Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 3.5-5 Project No.: N2022-051-002 Sample No.: 2

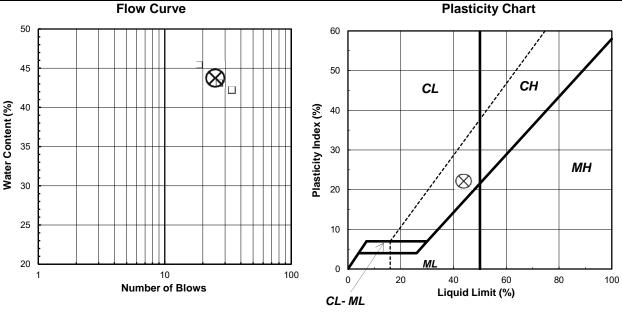
Lab ID: N2022-051-002-001 Soil Description: YELLOWISH BROWN LEAN CLAY

Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	Content		Liquid Limit Test				
ASTM D2216-19	1	2	3	M			
Tare Number:	26	Н	R	S	U		
Wt. of Tare & Wet Sample (g):	968.88	32.98	33.27	33.63	L		
Wt. of Tare & Dry Sample (g):	860.21	30.13	30.30	30.49	Т		
Weight of Tare (g):	198.55	23.37	23.41	23.57	I		
Weight of Water (g):	108.7	2.9	3.0	3.1	Р		
Weight of Dry Sample (g):	661.7	6.8	6.9	6.9	0		
Was As Received MC Preserved:	Yes				I		
Moisture Content (%):	16.4	42.2	43.1	45.4	N		
Number of Blows:		34	27	19	T		

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	K	J		Liquid Limit (%):	44
Wt. of Tare & Wet Sample (g):	34.79	33.45			
Wt. of Tare & Dry Sample (g):	32.78	31.64		Plastic Limit (%):	22
Weight of Tare (g):	23.63	23.54			
Weight of Water (g):	2.0	1.8		Plasticity Index (%):	22
Weight of Dry Sample (g):	9.2	8.1			
				USCS Symbol:	CL
Moisture Content (%):	22.0	22.3	-0.4		
Note: The acceptable range of the	e two Moistu	re Conten	ts is $\pm$ 1.12		



page 1 of 1 DCN: CTS4B, REV. 8, 5/22/18

JV

Date

Tested By

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4/20/22

Date

Checked By

NC

4/19/22



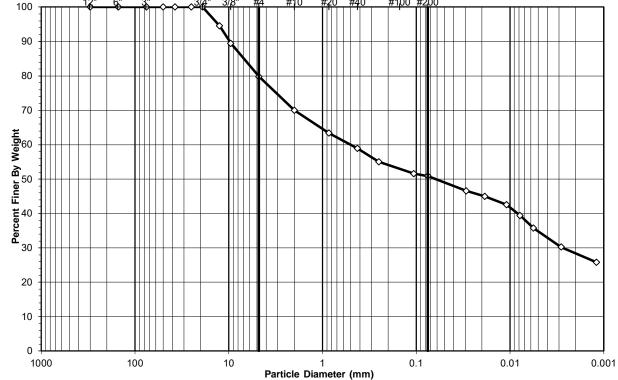
#### SIEVE AND HYDROMETER ANALYSIS

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW2-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 3.5-5
Project No.: N2022-051-002 Sample No.: 2

Lab ID: N2022-051-002-001 Soil Color: Yellowish Brown

			HYDROMETER			
USCS	cobbles	gravel		sand		silt and clay fraction
AASHTO	cobbles	gravel		sand		silt and clay fraction
100	12" 6,"	3" ^ ^3/4" 3/8" #	4 #10	#20 #40	#100 #200	



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	30.02		
100	100.00	Gravel	20.24	Sand	19.11	Gravel	20.24
2	69.98	Sand	28.89	Coarse Sand	11.08	Sand	28.89
0.075	50.87	Silt&Clay	50.87	Fine Sand	8.04	Silt	16.07
0.05	49.02			Silt & Clay	50.87	Clay	34.80
0.005	34.80			Silt	22.45		
0.002	28.42			Clay	28.42		

AASHTO (GI): USCS Symbol: A - 7 - 6 (8) CL, TESTED

USCS Classification
SANDY LEAN CLAY WITH GRAVEL

page 1 of 3  $\,$  DCN: CT-S3X  $\,$  DATE: 4/30/18  $\,$  REVISION: 8  $\,$ 



#### **WASH SIEVE ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW2-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 3.5-5
Project No.: N2022-051-002 Sample No.: 2

Lab ID: N2022-051-002-001 Soil Color: Yellowish Brown

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material	
Tare No.:	26	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	518.33	Weight of Tare & Wet Sample (g):	NA
Wt. of Tare & Dry Sample (g):	518.33	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	198.55	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	319.78	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	319.78
Dry Weight of - 3/4" Sample (g):	319.78	Weight of minus #200 Material (g):	162.67
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	157.11
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	319.78		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	17.47		5.46	5.46	94.54	94.54
3/8"	9.50	16.28		5.09	10.55	89.45	89.45
#4	4.75	30.98		9.69	20.24	79.76	79.76
#10	2.00	31.26		9.78	30.02	69.98	69.98
#20	0.85	21.27	( ** )	6.65	36.67	63.33	63.33
#40	0.425	14.15		4.42	41.09	58.91	58.91
#60	0.250	12.39		3.87	44.97	55.03	55.03
#140	0.106	10.96		3.43	48.40	51.60	51.60
#200	0.075	2.35		0.73	49.13	50.87	50.87
Pan	-	162.67		50.87	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

Tested By	JV	Date	4/19/22	Checked By	NC	Date	4/20/22



#### **HYDROMETER ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW2-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 3.5-5

 Project No.:
 N2022-051-002
 Sample No.:
 2

 Lab ID:
 N2022-051-002-001
 Soil Color:
 Yellowish Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction C	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	35.00	24.8	5.6	29.4	91.5	0.01270	0.0292	46.6
5	34.00	24.8	5.6	28.4	88.4	0.01270	0.0186	45.0
15	32.50	24.7	5.6	26.9	83.7	0.01272	0.0109	42.6
30	30.50	24.7	5.6	24.9	77.5	0.01272	0.0078	39.4
60	28.25	24.5	5.7	22.6	70.3	0.01275	0.0056	35.8
250	25.00	23.6	5.9	19.1	59.4	0.01288	0.0028	30.2
1440	22.00	24.4	5.7	16.3	50.8	0.01276	0.0012	25.8

Soil Specimen Data		Other Corrections	
Tare No.	14		
Wt. of Tare & Dry Material (g):	337.11	a - Factor	0.993
Weight of Tare (g):	300.19		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	50.87
Weight of Dry Material (g):	31.92		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

#### **Atterberg Limits Test Results:**

11 = 44

PL = 22

PI = 22

Tested By JV Date 4/19/22 Checked By NC Date 4/21/22

page 3 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8



(Minus No. 40 sieve material, Air dried)

#### ATTERBERG LIMITS

ASTM D 4318-17

Client: GeoEngineers, Inc. Boring No.: RW8-1 Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 38.5-40

Project No.: N2022-051-002 Sample No.: 8

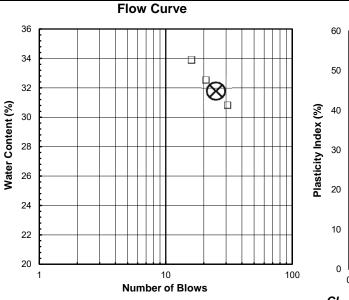
Note: The USCS symbol used with this test refers only to the minus No. 40

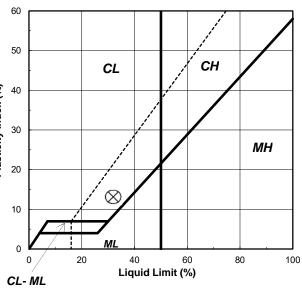
Lab ID: N2022-051-002-004 Soil Description: BROWN LEAN CLAY

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture	As Received Moisture Content			iid Limit To	est	
ASTM D2216-19	1	2	3	M		
Tare Number:	51	Α	Q	Т	U	
Wt. of Tare & Wet Sample (g):	1249.25	34.87	33.97	33.42	L	
Wt. of Tare & Dry Sample (g):	1057.12	32.21	31.43	30.92	T	
Weight of Tare (g):	198.66	23.58	23.62	23.54	I	
Weight of Water (g):	192.1	2.7	2.5	2.5	Р	
Weight of Dry Sample (g):	858.5	8.6	7.8	7.4	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%):	22.4	30.8	32.5	33.9	N	
Number of Blows:		31	21	16	Т	

Plastic Limit Test	1	2	Range		Test Results	
Tare Number:	X	С			Liquid Limit (%):	32
Wt. of Tare & Wet Sample (g):	33.99	37.59			' ' '	
Wt. of Tare & Dry Sample (g):	32.28	35.30			Plastic Limit (%):	19
Weight of Tare (g):	23.45	23.59			ì	
Weight of Water (g):	1.7	2.3			Plasticity Index (%):	13
Weight of Dry Sample (g):	8.8	11.7				
					USCS Symbol:	CL
Moisture Content (%):	19.4	19.6	-0.2			
Note: The acceptable range of the	e two Moistu	ts is ±	1.12			
Flow Curve	9			Plasticity Chart		





Tested By JV Date 4/19/22 Checked By NC Date 4/20/22



#### SIEVE AND HYDROMETER ANALYSIS

ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW8-1

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 38.5-40

 Project No.:
 N2022-051-002
 Sample No.:
 8

 Lab ID:
 N2022-051-002-004
 Soil Color:
 Brown

		SIEVE ANA	AL YSIS	HYDROMETER
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
100 111	12" 6"	3"	#10 #20 #40 #100 #2	200
11				
90 🚻				
111				
80 🚻				
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70				
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Percent Finer By Weight				
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Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	0.62		
100	100.00	Gravel	0.20	Sand	9.69	Gravel	0.20
2	99.38	Sand	10.12	Coarse Sand	2.67	Sand	10.12
0.075	89.69	Silt&Clay	89.69	Fine Sand	7.03	Silt	49.40
0.05	84.24			Silt & Clay	89.69	Clay	40.28
0.005	40.28			Silt	61.58		
0.002	28.11			Clay	28.11		

Particle Diameter (mm)

<u>AASHTO (GI):</u> A - 6 (11)

1000

USCS Symbol: CL, TESTED

10

USCS Classification LEAN CLAY

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100

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0.1

0.001



#### **WASH SIEVE ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

 Client:
 GeoEngineers, Inc.
 Boring No.:
 RW8-1

 Client Reference:
 24647-009-00 I-24/I-75 Interchange
 Depth (ft):
 38.5-40

 Project No.:
 N2022-051-002
 Sample No.:
 8

 Lab ID:
 N2022-051-002-004
 Soil Color:
 Brown

Moisture Content of Passing 3/4" Material		Moisture Content of Retained 3/4" Material	
Tare No.:	51	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	628.25	Weight of Tare & Wet Sample (g):	NA
Wt. of Tare & Dry Sample (g):	628.25	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	198.66	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	429.59	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	429.59
Dry Weight of - 3/4" Sample (g):	429.59	Weight of minus #200 Material (g):	385.28
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	44.31
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	429.59		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	0.00		0.00	0.00	100.00	100.00
3/8"	9.50	0.00		0.00	0.00	100.00	100.00
#4	4.75	0.84		0.20	0.20	99.80	99.80
#10	2.00	1.84		0.43	0.62	99.38	99.38
#20	0.85	3.53	( ** )	0.82	1.45	98.55	98.55
#40	0.425	7.92		1.84	3.29	96.71	96.71
#60	0.250	8.84		2.06	5.35	94.65	94.65
#140	0.106	14.01		3.26	8.61	91.39	91.39
#200	0.075	7.33		1.71	10.31	89.69	89.69
Pan	-	385.28		89.69	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

Tested By	JV	Date	4/19/22	Checked By	NC	Date	4/20/22



#### **HYDROMETER ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW8-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 38.5-40

 Project No.:
 N2022-051-002
 Sample No.:
 8

 Lab ID:
 N2022-051-002-004
 Soil Color:
 Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	49.25	24.8	5.6	43.7	84.0	0.01270	0.0258	75.3
5	44.00	24.8	5.6	38.4	73.9	0.01270	0.0171	66.3
15	37.75	24.7	5.6	32.1	61.8	0.01272	0.0104	55.5
30	33.75	24.6	5.6	28.1	54.1	0.01273	0.0076	48.5
60	30.00	24.5	5.7	24.3	46.8	0.01275	0.0056	42.0
250	24.00	23.6	5.9	18.1	34.8	0.01288	0.0029	31.2
1440	19.50	24.4	5.7	13.8	26.6	0.01276	0.0012	23.8

Soil Specimen Data		Other Corrections	
Tare No.	15		
Wt. of Tare & Dry Material (g):	355.63	a - Factor	0.993
Weight of Tare (g):	299.00		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	89.69
Weight of Dry Material (g):	51.63		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

#### **Atterberg Limits Test Results:**

LL = 32 PL = 19

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	Tested B	y JV	Date	4/19/22	Checked By	, NC	Date	4/21/22
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13



#### ATTERBERG LIMITS

ASTM D 4318-17

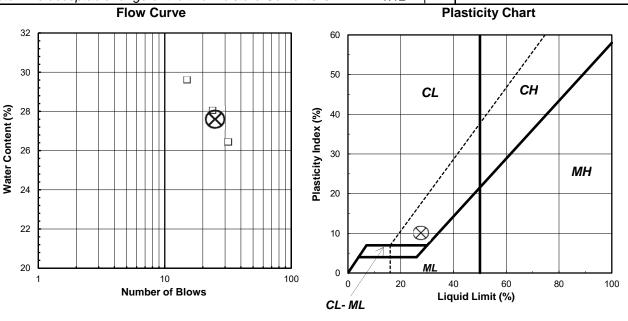
Client: Boring No.: RW10-1 GeoEngineers, Inc. Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 28.5-30

Project No.: N2022-051-002 Sample No.: 7

Lab ID: N2022-051-002-006 Soil Description: BROWNISH ORANGE LEAN CLAY Note: The USCS symbol used with this test refers only to the minus No. 40 (Minus No. 40 sieve material, Air dried) sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description

As Received Moisture		Liquid Limit Test				
ASTM D2216-19	1	2	3	M		
Tare Number:	55	F	W	N	U	
Wt. of Tare & Wet Sample (g):	1137.79	32.61	33.49	33.02	L	
Wt. of Tare & Dry Sample (g):	980.49	30.75	31.34	30.80	Т	
Weight of Tare (g):	201.27	23.71	23.67	23.30	I	
Weight of Water (g):	157.3	1.9	2.2	2.2	Р	
Weight of Dry Sample (g):	779.2	7.0	7.7	7.5	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%):	20.2	26.4	28.0	29.6	N	
Number of Blows:		32	24	15	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tare Number:	D	М		Liquid Limit (%):	28
Wt. of Tare & Wet Sample (g):	33.56	33.95			
Wt. of Tare & Dry Sample (g):	32.02	32.38		Plastic Limit (%):	18
Weight of Tare (g):	23.50	23.69			
Weight of Water (g):	1.5	1.6		Plasticity Index (%):	10
Weight of Dry Sample (g):	8.5	8.7			
, , , , , ,				USCS Symbol:	CL
Moisture Content (%):	18.1	18.1	0.0	_	
Note: The acceptable range of the	e two Moistu	ire Conten	ts is ± 1.12		



4/19/22 Checked By NC 4/20/22 Tested By JV Date Date

DCN: CTS4B, REV. 8, 5/22/18

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#### SIEVE AND HYDROMETER ANALYSIS

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW10-1 Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 28.5-30 Sample No.: 7 Project No.: N2022-051-002

Soil Color: Lab ID: N2022-051-002-006 **Brownish Orange** 

		SIEVE	ANALYSIS	HYDROMETER
USCS	cobbles	gravel	sand	silt and clay fraction
AASHTO	cobbles	gravel	sand	silt and clay fraction
100	12" 6"	3" ^ 3/4" 3/8" #4	#10 #20 #40 #1,00 #2	00
100				
90 1				
30				
80				
00 III				
70				
111				
<b>a</b>				
By Weight				
<u>a</u>				
Fig. 50				
<u>ш</u> ,				
<b>1</b> 40 <del> </del>				

USCS AASHTO **ASTM** Sieve Percent Size (mm) **Finer** (%) (%) (%) Gravel 20.33 100 100.00 Gravel 11.66 Sand Gravel 11.66 31.66 Sand 40.33 Coarse Sand Sand 40.33 2 79.67 15.38 0.075 48.01 Silt&Clay 48.01 Fine Sand Silt 25.16 16.29 0.05 44.95 Silt & Clay 48.01 Clay 22.84 0.005 22.84 Silt 32.38 0.002 15.63 Clay 15.63 AASHTO (GI): **USCS Symbol:** D50 = 0.10

Particle Diameter (mm)

(2)

A - 4

20

10

0

1000

**USCS Classification CLAYEY SAND** 

page 1 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8

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#### **WASH SIEVE ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW10-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 28.5-30
Project No.: N2022-051-002 Sample No.: 7

Lab ID: N2022-051-002-006 Soil Color: Brownish Orange

Moisture Content of Passing 3/4" N	1aterial	Moisture Content of Retained 3/4" Material	
Tare No.:	55	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	649.37	Weight of Tare & Wet Sample (g):	NA
Wt. of Tare & Dry Sample (g):	649.37	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	201.27	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	448.10	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	448.10
Dry Weight of - 3/4" Sample (g):	448.10	Weight of minus #200 Material (g):	215.13
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	232.97
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	448.10		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	13.46		3.00	3.00	97.00	97.00
3/8"	9.50	10.46		2.33	5.34	94.66	94.66
#4	4.75	28.33		6.32	11.66	88.34	88.34
#10	2.00	38.84		8.67	20.33	79.67	79.67
#20	0.85	40.38 (	** )	9.01	29.34	70.66	70.66
#40	0.425	28.52		6.36	35.70	64.30	64.30
#60	0.250	27.28		6.09	41.79	58.21	58.21
#140	0.106	35.70		7.97	49.76	50.24	50.24
#200	0.075	10.00		2.23	51.99	48.01	48.01
Pan	-	215.13	<del>-</del>	48.01	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

Tested By	/ JV	Date	4/19/22	Checked By	NC	Date	4/20/22
•							



#### **HYDROMETER ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW10-1
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 28.5-30
Project No.: N2022-051-002 Sample No.: 7

Lab ID: N2022-051-002 Sample No.: 7

Soil Color: Brownish Orange

Elapsed Time	R Measured	Temp.	Composite Correction (	R	N	K Factor	Diameter	N'
(min)	INICASUICU	(°C)	Correction	Jonecleu	(%)	ractor	(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	32.75	24.7	5.6	27.1	85.4	0.01272	0.0297	41.0
5	29.00	24.7	5.6	23.4	73.6	0.01272	0.0193	35.4
15	26.00	24.7	5.6	20.4	64.2	0.01272	0.0114	30.8
30	23.25	24.6	5.6	17.6	55.5	0.01273	0.0082	26.6
60	21.75	24.4	5.7	16.1	50.6	0.01276	0.0059	24.3
250	18.00	23.6	5.9	12.1	38.0	0.01288	0.0030	18.3
1440	14.00	24.4	5.7	8.3	26.2	0.01276	0.0013	12.6

Soil Specimen Data		Other Corrections	
Tare No.	16		
Wt. of Tare & Dry Material (g):	336.85	a - Factor	0.993
Weight of Tare (g):	300.30		
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	48.01
Weight of Dry Material (g):	31.55		
		Specific Gravity	2.70 Assumed

**Note:** Hydrometer test is performed on - # 200 sieve material.

#### **Atterberg Limits Test Results:**

PL = 18 PI = 10

Tested By	JV	Date	4/19/22	Checked By	NC	Date	4/21/22
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#### ATTERBERG LIMITS

ASTM D 4318-17

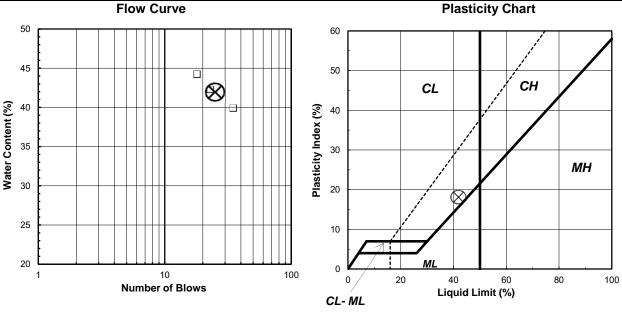
Client: GeoEngineers, Inc. Boring No.: RW11-2 Client Reference: 24647-009-00, I-24/I-75 Interchange Depth (ft): 18.5-20 Project No.: N2022-051-002 Sample No.: 5

Lab ID: N2022-051-002-014 Soil Description: ORANGISH BROWN LEAN CLAY **Note:** The USCS symbol used with this test refers only to the minus **No. 40** (Minus No. 40 sieve material, Air dried)

sieve material. See the "Sieve and Hydrometer Analysis" graph page for the complete material description.

As Received Moisture		Liquid Limit Test				
ASTM D2216-19		1	2	3	M	
Tare Number:	27	L	E	G	U	
Wt. of Tare & Wet Sample (g):	1014.30	34.48	33.94	33.67	L	
Wt. of Tare & Dry Sample (g):	895.80	31.37	30.83	30.58	T	
Weight of Tare (g):	202.80	23.57	23.47	23.59	I	
Weight of Water (g):	118.5	3.1	3.1	3.1	Р	
Weight of Dry Sample (g):	693.0	7.8	7.4	7.0	0	
Was As Received MC Preserved:	Yes				I	
Moisture Content (%):	17.1	39.9	42.3	44.2	N	
Number of Blows:		35	23	18	Т	

Plastic Limit Test	1	2	Range	Test Results	
Tana Niversham	Б	Б		Limit d Limit (0/)	40
Tare Number:	В	Р		Liquid Limit (%):	42
Wt. of Tare & Wet Sample (g):	32.78	32.69			
Wt. of Tare & Dry Sample (g):	30.98	30.97		Plastic Limit (%):	24
Weight of Tare (g):	23.44	23.72			
Weight of Water (g):	1.8	1.7		Plasticity Index (%):	18
Weight of Dry Sample (g):	7.5	7.3			
				USCS Symbol:	CL
Moisture Content (%):	23.9	23.7	0.1		
Note: The acceptable range of the	e two Moistu	re Content	ts is $\pm$ 1.12		



page 1 of 1 DCN: CTS4B, REV. 8, 5/22/18

JV

Date

Tested By

S:\Excel\Excel QA\Spreadsheets\Limit 3Pt.xls

4/20/22

Date

Checked By

NC

4/19/22



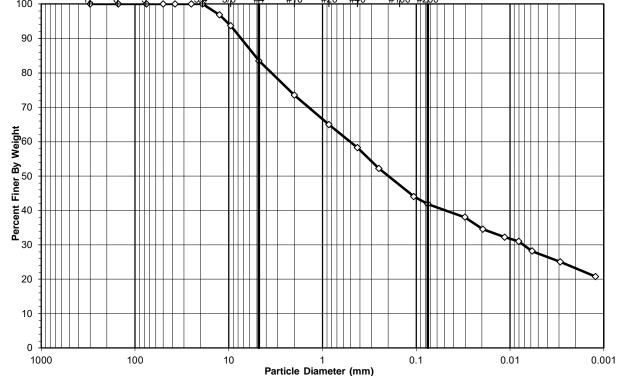
#### SIEVE AND HYDROMETER ANALYSIS

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW11-2
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 18.5-20
Project No.: N2022-051-002 Sample No.: 5

Lab ID: N2022-051-002-014 Soil Color: Orangish Brown

		SIEVE ANALYSIS								
	cobbles	gravel	sand	silt and clay fraction						
AASHTO	cobbles	gravel	sand	silt and clay fraction						
100	12" 6"	3,4,3,8,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,	#10 #20 #40 #100 #2	200						



Sieve	Percent		USCS		AASHTO		ASTM
Size (mm)	Finer		(%)		(%)		(%)
				Gravel	26.44		
100	100.00	Gravel	16.50	Sand	31.70	Gravel	16.50
2	73.56	Sand	41.65	Coarse Sand	15.31	Sand	41.65
0.075	41.86	Silt&Clay	41.86	Fine Sand	16.39	Silt	14.36
0.05	40.15			Silt & Clay	41.86	Clay	27.50
0.005	27.50			Silt	18.64		
0.002	23.22			Clay	23.22		
AASHTO (	GI):		JSCS Symbo	ol:	•	D50 =	0.20

AASHTO (GI): USCS Symbol: A - 7 - 6 (4) SC, TESTED

USCS Classification
CLAYEY SAND WITH GRAVEL

page 1 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8



#### **WASH SIEVE ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW11-2
Client Reference: 24647-009-00 I-24/I-75 Interchange Depth (ft): 18.5-20

Project No.: N2022-051-002 Sample No.: 5

Lab ID: N2022-051-002-014 Soil Color: Orangish Brown

Moisture Content of Passing 3/4" M	laterial	Moisture Content of Retained 3/4" Material	
Tana Na	07	Tana Na .	NIA
Tare No.:	27	Tare No.:	NA
Wt. of Tare & Wet Sample (g):	591.39	Weight of Tare & Wet Sample (g):	NA
Wt. of Tare & Dry Sample (g):	591.39	Weight of Tare & Dry Sample (g):	NA
Weight of Tare (g):	202.80	Weight of Tare (g):	NA
Weight of Water (g):	0.00	Weight of Water (g):	NA
Weight of Dry Soil (g):	388.59	Weight of Dry Soil (g):	NA
Moisture Content (%):	0.0	Moisture Content (%):	0.0

Wet Weight of -3/4" Sample (g):	NA	Weight of the Dry Sample (g):	388.59
Dry Weight of - 3/4" Sample (g):	388.59	Weight of minus #200 Material (g):	162.66
Wet Weight of +3/4" Sample (g):	0.00	Weight of plus #200 Material (g):	225.93
Dry Weight of +3/4" Sample (g):	0.00		
Total Dry Weight of Sample (g):	388.59		

Sieve	Sieve	Weight of Soil		Percent	Accumulated	Percent	Accumulated
Size	Opening	Retained		Retained	Percent	Finer	Percent
					Retained		Finer
	(mm)	(g)		(%)	(%)	(%)	(%)
12"	300	0.00		0.00	0.00	100.00	100.00
6"	150	0.00		0.00	0.00	100.00	100.00
3"	75	0.00		0.00	0.00	100.00	100.00
2"	50	0.00	( * )	0.00	0.00	100.00	100.00
1 1/2"	37.5	0.00		0.00	0.00	100.00	100.00
1"	25.0	0.00		0.00	0.00	100.00	100.00
3/4"	19.0	0.00		0.00	0.00	100.00	100.00
1/2"	12.5	12.29		3.16	3.16	96.84	96.84
3/8"	9.50	12.29		3.16	6.33	93.67	93.67
#4	4.75	39.52		10.17	16.50	83.50	83.50
#10	2.00	38.66		9.95	26.44	73.56	73.56
#20	0.85	33.57	( ** )	8.64	35.08	64.92	64.92
#40	0.425	25.91		6.67	41.75	58.25	58.25
#60	0.250	23.38		6.02	47.77	52.23	52.23
#140	0.106	31.96		8.22	55.99	44.01	44.01
#200	0.075	8.35		2.15	58.14	41.86	41.86
Pan	-	162.66		41.86	100.00	-	-

**NOTES:** (\*) The + 3/4" sieve analysis is based on the Total Dry Weight of the Sample

( \*\* ) The - 3/4" sieve analysis is based on the Weight of the Dry Sample

Tested By JV Date 4/19/22 Checked By NC Date 4/20/22

page 2 of 3 DCN: CT-S3TW DATE: 8/19/19 REVISION: 0



#### **HYDROMETER ANALYSIS**

ASTM D 422-63 (2007), AASHTO T88

Client: GeoEngineers, Inc. Boring No.: RW11-2 24647-009-00 I-24/I-75 Interchange Depth (ft): Client Reference: 18.5-20 Project No.: N2022-051-002 Sample No.: 5

Lab ID: N2022-051-002-014 Soil Color: Orangish Brown

Elapsed	R	Temp.	Composite	R	N	K	Diameter	N'
Time	Measured		Correction (	Corrected		Factor		
(min)		(°C)			(%)		(mm)	(%)
0	NA	NA	NA	NA	NA	NA	NA	NA
2	30.00	24.7	5.6	24.4	90.9	0.01272	0.0303	38.0
5	27.75	24.7	5.6	22.1	82.5	0.01272	0.0195	34.5
15	26.25	24.7	5.6	20.6	76.9	0.01272	0.0114	32.2
30	25.50	24.6	5.6	19.9	74.0	0.01273	0.0081	31.0
60	23.75	24.4	5.7	18.1	67.3	0.01276	0.0058	28.2
250	22.00	23.6	5.9	16.1	59.9	0.01288	0.0029	25.1
1440	19.00	24.4	5.7	13.3	49.6	0.01276	0.0012	20.8

Soil Specimen Data		Other Corrections					
Tare No.	17						
Wt. of Tare & Dry Material (g):	330.97	a - Factor	0.993				
Weight of Tare (g):	299.31						
Weight of Deflocculant (g):	5.0	Percent Finer than # 200	41.86				
Weight of Dry Material (g):	26.66						
		Specific Gravity	2.70 Assumed				

Note: Hydrometer test is performed on - # 200 sieve material.

#### **Atterberg Limits Test Results:**

42

PL24

Ы 18

> 4/19/22 Checked By Tested By NC 4/21/22 JV Date Date

page 3 of 3 DCN: CT-S3X DATE: 4/30/18 REVISION: 8

APPENDIX C
CBR Estimates Based on DCP



#### PROJECT I-24/I-75 Interchange Improvements Phase II

**FILE NO.** 24647-009-00 CBR Estimates Based on DCP PAGE 1

PREPARED BY **DATE** 4/25/2022 ECR DATE 4/27/2022 CHECKED BY

PURPOSE: Estimate California Bearing Ratio (CBR) based on dynamic cone penetrometer (DCP) readings taken in the field.

REFERENCES: Steve L. Webster, et al. (1992) Description and Application of Dual Mass Dynamic Cone Pentrometer. Instruction Report GL-92-3, US Army Corps of Engineers, Washington, DC

**CALCUATIONS:** 

$$CBR = \frac{292}{DCP Index^{1.12}}$$

Boring ID: WB-1

Number of Blows	Cumulative Pentration (mm)	Penetration Between Readings (mm)	Penetration per Blow (mm)	Hammer Factor <sup>1</sup>	DCP Index (mm/blow)	USCS Classifcation	Estimated CBR (%)
21	50	50	2	2	5	CL	51
20	100	50	3	2	5	CL	48
25	150	50	2	2	4	CL	62
13	200	50	4	2	8	CL	30
18	250	50	3	2	6	CL	43
15	300	50	3	2	7	CL	35

Average CBR (%) =

Boring ID: WB-2

Number of Blows	Cumulative Pentration (mm)	Penetration Between Readings (mm)	Penetration per Blow (mm)	Hammer Factor <sup>1</sup>	DCP Index (mm/blow)	USCS Classifcation	Estimated CBR (%)
10	50	50	5	2	10	CL	22
26	100	50	2	2	4	CL	65
24	150	50	2	2	4	CL	59
8	200	50	6	2	13	CL	17
7	250	50	7	2	14	CL	15
12	300	50	4	2	8	CL	27
21	350	50	2	2	5	CL	51

Average CBR	(%) =	37
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<sup>&</sup>lt;sup>1</sup>Hammer factor = 1 for 17.6 pound hammer and hammer factor = 2 for 10.1 pound hammer



PROJECT I-24/I-75 Interchange Improvements Phase II

**FILE NO.** 24647-009-00 PAGE 2 CBR Estimates Based on DCP 3

PREPARED BY DATE 4/25/2022 CHECKED BY ECR DATE 4/27/2022

Boring ID: WB-3

Number of Blows	Cumulative Pentration (mm)	Penetration Between Readings (mm)	Penetration per Blow (mm)	Hammer Factor <sup>1</sup>	DCP Index (mm/blow)	USCS Classifcation	Estimated CBR (%)
3	50	50	17	2	33	CL	6
4	100	50	13	2	25	CL	8
5	150	50	10	2	20	CL	10
3	200	50	17	2	33	CL	6
3	250	50	17	2	33	CL	6
5	300	50	10	2	20	CL	10
7	350	50	7	2	14	CL	15
18	400	50	3	2	6	CL	43

Average CBR (%) = 13

Boring ID: EB-1

Number of	Cumulative Pentration	Penetration Between Readings	Penetration	Hammer	DCP Index	USCS	Estimated
Blows	(mm)	(mm)	per Blow (mm)		(mm/blow)	Classifcation	CBR (%)
9	50	50	6	2	11	CL	20
11	100	50	5	2	9	CL	25
15	150	50	3	2	7	CL	35
18	200	50	3	2	6	CL	43
10	250	50	5	2	10	CL	22
16	300	50	3	2	6	CL	37
14	350	50	4	2	7	CL	32

Average CBR (%) =

<sup>&</sup>lt;sup>1</sup>Hammer factor = 1 for 17.6 pound hammer and hammer factor = 2 for 10.1 pound hammer



PROJECT I-24/I-75 Interchange Improvements Phase II

**FILE NO.** 24647-009-00 PAGE 3 CBR Estimates Based on DCP 3

PREPARED BY DATE 4/25/2022 CHECKED BY ECR DATE 4/27/2022

Boring ID: EB-2

Number of	Cumulative Pentration	Penetration Between Readings	Penetration	Hammer	DCP Index	USCS	Estimated
Blows	(mm)	(mm)	per Blow (mm)	Factor <sup>1</sup>	(mm/blow)	Classifcation	CBR (%)
7	50	50	7	2	14	CL	15
10	100	50	5	2	10	CL	22
10	150	50	5	2	10	CL	22
9	200	50	6	2	11	CL	20
13	250	50	4	2	8	CL	30
7	300	50	7	2	14	CL	15
6	350	50	8	2	17	CL	13
12	400	50	4	2	8	CL	27
11	450	50	5	2	9	CL	25
20	500	50	3	2	5	CL	48

24 Average CBR (%) =

Boring ID: EB-3

Number of Blows	Cumulative Pentration (mm)	Penetration Between Readings (mm)	Penetration per Blow (mm)	Hammer Factor <sup>1</sup>	DCP Index (mm/blow)	USCS Classifcation	Estimated CBR (%)
10	50	50	5	2	10	CL	22
6	100	50	8	2	17	CL	13
4	150	50	13	2	25	CL	8
4	200	50	13	2	25	CL	8
14	250	50	4	2	7	CL	32
10	300	50	5	2	10	CL	22
28	350	50	2	2	4	CL	70
28	400	50	2	2	4	CL	70
14	450	50	4	2	7	CL	32
14	500	50	4	2	7	CL	32

Average CBR (%) =

<sup>&</sup>lt;sup>1</sup>Hammer factor = 1 for 17.6 pound hammer and hammer factor = 2 for 10.1 pound hammer

APPENDIX D
Report Limitations and Guidelines for Use

#### APPENDIX D

#### REPORT LIMITATIONS AND GUIDELINES FOR USE<sup>1</sup>

This appendix provides information to help you manage your risks with respect to the use of this report.

#### Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

This letter has been prepared for Neel-Schaffer, Inc. (NS), and their authorized agents and regulatory agencies. The information contained herein is not applicable to other sites.

GeoEngineers structures our services to meet the specific needs of our clients. No party other than NS may rely on the product of our services unless we agree to such reliance in advance and in writing. This is to provide our firm with reasonable protection against open-ended liability claims by third parties; otherwise, there would be no contractual limits to their actions. Within the limitations of scope, schedule, and budget, our services have been executed in accordance with our Agreement with the Client and generally accepted geotechnical practices in this area at the time this report was prepared. Use of this report is not recommended for any purpose or project except the one originally contemplated.

#### A Geotechnical Engineering or Geologic Report is Based on a Unique Set of Project-Specific Factors

This report has been prepared for the I-24/I-75 Interchange Improvements Phase II project. GeoEngineers considered a number of unique, project-specific factors when establishing the scope of services for this project and report. Unless GeoEngineers specifically indicates otherwise, it is important not to rely on this report if it was:

- not prepared for you,
- not prepared for your project,
- not prepared for the specific site explored, or
- completed before important project changes were made.

For example, changes that can affect the applicability of this report include those that affect:

- the function of the proposed structure;
- elevation, configuration, location, orientation, or weight of the proposed structure;
- composition of the design team; or
- project ownership.

<sup>&</sup>lt;sup>1</sup> Developed based on material provided by ASFE, Professional Firms Practicing in the Geosciences; www.asfe.org.



If important changes are made after the date of this report, we recommend that GeoEngineers be given the opportunity to review our interpretations and recommendations. Based on that review, we can provide written modifications or confirmation, as appropriate.

#### **Subsurface Conditions Can Change**

This geotechnical or geologic report is based on conditions that existed at the time the study was performed. The findings and conclusions of this report may be affected by the passage of time, by man-made events such as construction on or adjacent to the site, or by natural events such as floods, earthquakes, slope instability, or groundwater fluctuations. If more than a few months have passed since issuance of our report or work product, or if any of the described events may have occurred, please contact GeoEngineers before applying this report for its intended purpose so that we may evaluate whether changed conditions affect the continued reliability or applicability of our conclusions and recommendations.

#### **Most Geotechnical and Geologic Findings Are Professional Opinions**

Our interpretations of subsurface conditions are based on field observations from widely spaced sampling locations at the site. Site exploration identifies the specific subsurface conditions only at those points where subsurface tests are conducted or samples are taken. GeoEngineers reviewed field and laboratory data and then applied our professional judgment to render an informed opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ, sometimes significantly, from those indicated in this report. Our report, conclusions, and interpretations should not be construed as a warranty of the subsurface conditions.

#### **Geotechnical Engineering Report Recommendations Are Not Final**

The construction recommendations included in this report are preliminary and should not be considered final. GeoEngineers' recommendations can be finalized only by observing actual subsurface conditions revealed during construction. GeoEngineers is unable to assume responsibility for the recommendations in this report without performing construction observation.

We recommend that you allow sufficient monitoring, testing, and consultation during construction by GeoEngineers to confirm that the conditions encountered are consistent with those indicated by the explorations, to provide recommendations for design changes if the conditions revealed during the work differ from those anticipated, and to evaluate whether earthwork activities are completed in accordance with our recommendations. Retaining GeoEngineers for construction observation for this project is the most effective method of managing the risks associated with unanticipated conditions.

#### A Geotechnical Engineering or Geologic Report Could Be Subject to Misinterpretation

Misinterpretation of this report by members of the design team or by contractors can result in costly problems. GeoEngineers can help reduce the risks of misinterpretation by conferring with appropriate members of the design team after submitting the report, reviewing pertinent elements of the design team's plans and specifications, participating in pre-bid and preconstruction conferences, and providing construction observation.



#### **Do Not Redraw the Exploration Logs**

Geotechnical engineers and geologists prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. The logs included in a geotechnical engineering or geologic report should never be redrawn for inclusion in architectural or other design drawings. Photographic or electronic reproduction is acceptable but separating logs from the report can create a risk of misinterpretation.

#### **Give Contractors a Complete Report and Guidance**

To help prevent costly problems associated with unanticipated subsurface conditions, we recommend giving contractors the complete geotechnical engineering or geologic report but preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report's accuracy is limited. In addition, encourage them to confer with GeoEngineers and/or to conduct additional study to obtain the specific types of information they need or prefer.

#### **Contractors Are Responsible for Site Safety on Their Own Construction Projects**

Our geotechnical recommendations are not intended to direct the contractor's procedures, methods, schedule, or management of the work site. The contractor is solely responsible for job site safety and for managing construction operations to minimize risks to on-site personnel and adjacent properties.

#### **Read These Provisions Closely**

It is important to recognize that the geoscience practices (geotechnical engineering, geology, and environmental science) are less exact than other engineering and natural science disciplines. Without this understanding, there may be expectations that could lead to disappointments, claims, and disputes. GeoEngineers includes these explanatory "limitations" provisions in our reports to help reduce such risks. Please confer with GeoEngineers if you need to know more how these "Report Limitations and Guidelines for Use" apply to your project or site.

#### **Biological Pollutants**

GeoEngineers' Scope of Work specifically excludes the investigation, detection, prevention, or assessment of the presence of Biological Pollutants. Accordingly, this report does not include any interpretations, recommendations, findings, or conclusions regarding the detecting, assessing, preventing, or abating of Biological Pollutants, and no conclusions or inferences should be drawn regarding Biological Pollutants as they may relate to this project. The term "Biological Pollutants" includes, but is not limited to, molds, fungi, spores, bacteria, and viruses, and/or any of their byproducts.



# APPENDIX C SOIL CLASSIFICATION CHARTS



### **UNIFIED SOIL CLASSIFICATION SYSTEM**

#### UNIFIED SOIL CLASSIFICATION AND SYMBOL CHART

COARSE-GRAINED SOILS

(more than 50% of material is larger than No. 200 sieve size.)

**GRAVELS** More than 50% of coarse fraction larger than No. 4 sieve size

(	Clean Gravels (Less than 5% fines)						
	GW	Well-graded gravels, gravel-sand mixtures, little or no fines					
	GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines					

Gravels with fines (More than 12% fines)

GM	Silty gravels, gravel-sand-silt mixtures
GC	Clayey gravels, gravel-sand-clay mixtures

**SANDS** 

50% or more of coarse fraction smaller than No. 4 sieve size

Clean :	Clean Sands (Less than 5% fines)									
SW	Well-graded sands, gravelly sands, little or no fines									
SP	Poorly graded sands, gravelly sands, little or no fines									

Sands with fines (More than 12% fines)

SM	Silty sands, sand-silt mixtures
sc	Clayey sands, sand-clay mixtures

#### **FINE-GRAINED SOILS**

(50% or more of material is smaller than No. 200 sieve size.)								
SILTS AND		ML	Inorganic silts and very fine sands, rock flour, silty of clayey fine sands or clayey silts with slight plasticity					
CLAYS Liquid limit less than		CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays					
50%	725700	OL	Organic silts and organic silty clays of low plasticity					
SILTS AND		МН	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts					
CLAYS Liquid limit 50%		СН	Inorganic clays of high plasticity, fat clays					
or greater		ОН	Organic clays of medium to high plasticity, organic silts					
HIGHLY ORGANIC SOILS	77. 7. 7. 7.7	PT	Peat and other highly organic soils					

#### LABORATORY CLASSIFICATION CRITERIA

GW 
$$C_u = \frac{D_{60}}{D_{10}}$$
 greater than 4;  $C_c = \frac{D_{30}}{D_{10} \times D_{60}}$  between 1 and 3

GP Not meeting all gradation requirements for GW

Atterberg limits below "A" GM line or P.I. less than 4

Atterberg limits above "A" GC line with P.I. greater than 7 Above "A" line with P.I. between 4 and 7 are borderline cases requiring use of dual symbols

SW 
$$C_u = \frac{D_{60}}{D_{10}}$$
 greater than 4;  $C_c = \frac{D_{30}}{D_{10} \times D_{60}}$  between 1 and 3

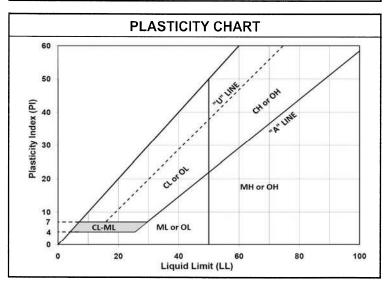
SP Not meeting all gradation requirements for GW

Atterberg limits below "A" SM line or P.I. less than 4

Atterberg limits above "A" SC line with P.I. greater than 7 Limits plotting in shaded zone with P.I. between 4 and 7 are borderline cases requiring use of dual symbols.

Determine percentages of sand and gravel from grain-size curve. Depending on percentage of fines (fraction smaller than No. 200 sieve size), coarse-grained soils are classified as follows:

Less than 5 percent ...... GW, GP, SW, SP 5 to 12 percent ...... Borderline cases requiring dual symbols



Usual types of significant constituent materials	Stone fragments, gravel and sand		Fine sand	Sand	Silty or clayey gravel and sand			Silty soils			Clayey soils				
Group Index	0				41	nax	8 max		12 max	10 max	16 max	20	max		
Plasticity index	6 max	6 max	Plastic	6 max	10 max	10 max		11 min		max		11 - 15			
Characteristics of fraction passing No. 40 Liquid limit	_	_	Non-	_	40 max	41 min	40 max	41 min	40 max 41 min						
No. 200 (75 µm)	15 max	25 max	10 max	35 max	35 max	35 max	35 max	35 max	36 min	50 min	36 min	361	min	36 min	
No. 40 (425 µm)	30 max	50 max	51 min	[2]					[3]	[4]					
No. 10 (2 mm)	50 max			4.5											
Sieve analysis, percent passing:						*				**	*			*	
Group Classification	A-1-a	A-1-b	A-3	A-3a	A-2-4	A-2-5	A-2-6	A-2-7	A-4a	A-4b		A-6a	A-6b	A-7-5	A-7-0
Group Classification	A-1		A-3 [1]		A		1-2		A-4		A-5	A-6		A-7	
General Classification	35 percent or less of total sample passing No. 20						0 (75 μm	) More than 35 percer			rcent of to	at of total sample passing No. 200 (75 μm			
General Classification	Granular Materials								Silt-Clay Materials						

#### Notes

With the test data available, the classification of a soil is found by proceeding from left to right on the chart. The first classification that the test data fits is the correct classification.

- \* A-2-5 is not allowed under 703.16.B. A-5 and A-7-5 is not allowed under 703.16.A. See "Natural Soil and Natural Granular Soils" (203.02.H) in this manual
- \*\* A-4b is not allowed in the top 3 feet (1.0 m) of the embankment under 203.03.A.
- [1] The placing of A-3 before A-2 is necessary in the "left to right" process, and does not indicate superiority of A-3 over A-2.
- [2] A-3a must contain a minimum 50 percent combined coarse and find sand sizes (passing No. 10 but retained on No. 200, between 2 mm and 75 μm).
- [3] A-4a must contain less than 50 percent silt size material (between 75 μm and 5 μm).
- [4] A-4b must contain 50 percent or more silt size material (between 75 μm and 5 μm).

JOB NO.: 300-18-0001	AASHTO CLASSIFICATION CHART	W	Ш
CLIENT: Neel-Schaffer	AASITIO CLASSII ICATION CHART	TYCHTA	즉
I-75 interchange at I-24 Chattanooga, TN	PIN 114174.00 I-75 INTERCHANGE AT I-24	KSWA	)euc
	CHATTANOOGA, TENNESSEE	K. S. Ware & Associates, L.L.C. Geotechnical • CEI • Environmental	Apk